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ANALYSIS OF THE APOLLO HEAT SHIELD PERFORMANCE

Volume II - EVAO Computer Program

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ANALYSIS OF THE APOLLO HEAT SHIELD PERFORMANCE

Volume II - CHAD Computer Program

By David W. Halstead, Richard S. Gaudette,
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PREFACE

This report was prepared by the Aerospace Systems Division, Aerospace Group of The Boeing Company, Seattle, Washington 98124. The Boeing Company program manager was Mr. Vladimir Deriugin, head of Heat Transfer and Thermal Protection in the Structures Research & Development Organization.

The program was initiated under NASA Contract NAS 9-7964, Analysis of the Apollo Heat Shield Performance, issued through the National Aeronautics and Space Administration, Manned Spacecraft Center, Houston, Texas 77058. The NASA technical monitors were Messrs. Don M. Curry and Paul Murad of the Thermal Technology Branch of the Structures and Mechanics Division.

Results obtained during this study are published in two volumes: Volume I, Analytical Methods; and Volume II, CHAD Computer Program. Boeing document numbers assigned to these volumes are D2-114433-1 and -2, respectively.

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GENERAL INFORMATION

The one-dimensional CHAD (CHarring Ablation with Diffusion) computer program described in this document was developed from the ablation analysis portion of the existing Boeing CHAP* program. This was done in support of the analytical investigation on the ablation performance of the Apollo vehicle ablation material (AVCOAT 5026-39/HC-G).

The CHAD computer program was developed to include the following areas of analysis:

- 1) Three reaction zones (virgin plastic pyrolysis, silica-carbon reactions, and carbon deposition).
- 2) Temperature, composition, and pressure variant thermal conductivity and specific heat for the char and virgin plastic.
- 3) Variable char density and variable char composition.
- 4) Gas specific heat which can be varied with time and composition.
- 5) Internal pressure profile determined and gas diffusion calculated.
- 6) Erosion rate prediction by the shear recession correlation of reference 1.

The CHAD ablation model is given the boundary layer conditions as input data. The surface heat balance includes surface sublimation and surface combustion terms. The program is written in Fortran IV. It is machine independent and, as much as possible, system independent.

* The CHAP program is a combination convective heating and ablation analysis program. The ablation analysis portion is commonly called the CHARM program. Reference 2 describes the CHAP program, and reference 3 describes the initial CHARM program.

Purpose

The purpose of the CHAD computer program is to predict the performance of charring ablators with more confidence. It provides an ablation analysis of more sophistication than previous programs by including multiple internal reactions and internal diffusion. Surface recession is determined and profiles of temperature, densities, gas flow rate, internal pressure, and gas concentrations are calculated.

Assumptions

A number of assumptions are made to simplify the program model. A brief list follows:

- 1) Virgin material is considered to be a combination of char material and decomposable material. The char material is considered to be silica and carbon.
- 2) Internal radiation may be accounted for in the thermal conductivity term.
- 3) The thermal conductivity of the ablation material is a linear combination of the thermal conductivity of the char material and of the decomposable material.
- 4) The thermal capacity of the ablation material is a linear combination of the thermal capacity of the char and of the decomposable material.
- 5) Thermal expansion or contraction is neglected.
- 6) The mass flow rate of the gas equals the amount formed or used up; that is, there is no capacity term in the gas flow equation.
- 7) The gas is in thermal equilibrium with the solid.
- 8) There is no separately-considered gas thermal conduction.

The finite-difference equations, which approximate the mathematical model, use the following assumptions:

- 1) The temperature of a nodal interface represents the temperature of the adjacent half-nodes.

- 2) Each half-node may be represented by a single density.
- 3) The thermal conductivity at the midpoint between nodal interfaces is a function of the average temperature and density of the two adjacent half-nodes.

Limitations

Limitations of the CHAD computer program are:

- 1) The maximum number of materials for one problem is 10.
- 2) The maximum number of nodes is 100 and the minimum is 2.
- 3) Char thermal properties and density are the same for all materials.
- 4) The maximum number of major nodes* in the pyrolysis reaction zone is 16. The program, as it operates, will not allow more nodes to be included in the pyrolysis reaction zone. It will wait until a node is dropped by near exhaustion (85%) of decomposable material before picking up a deeper node for the reaction zone.

There is some limitation inherent in the problems input to the program. Very high surface recession can cause the problem solution to become unstable. A rapidly oscillating heating rate to the ablation surface can result in an unstable problem solution. In each case above, the problem solutions require small time-steps for calculation resulting in excessive use of computer time and, in some cases, a computer error stop would result.

PROCEDURE

The following sections deal with the mathematical model used in the CHAD computer program. The governing equations and procedure of solution are discussed. All quantities are in consistent f.p.s. units, unless otherwise noted in the text. Most symbols are defined both in the nomenclature and in the immediate context of their use.

* Major nodes are the nodes as input. They are quartered by the program for the pyrolysis reaction zone.

Nomenclature

| | |
|------------------|---|
| A | frequency factor; area |
| B | activation temperature |
| B* | blowing parameter |
| c _p | specific heat |
| C _i | concentration of species |
| C _i | source (or sink) of species i |
| D | binary diffusivity |
| f _{dep} | weight fraction of pyrolysis gas which is deposited as solid carbon |
| g _c | gravitational constant |
| H | heat transfer coefficient |
| H _T | heat of decomposition at temperature T |
| k | thermal conductivity; specific reaction rate |
| K | diffusion reduction parameter, eq. (29) |
| K _{eq} | equilibrium constant |
| m | mass flux |
| M | molecular weight |
| n | order of reaction |
| P | pressure |
| q | heat flux |
| Q | total heat flux |
| r | radius; reaction rate |
| R | gas constant |
| s | surface recession rate |
| t | time |
| T | temperature |
| v | velocity in y-direction |
| w | mass fraction |
| x | distance |

| | |
|------------|---------------------------|
| γ | distance |
| Z | compressibility factor |
| α | absorptivity |
| Γ | permeability |
| ϵ | emissivity |
| η | γ/S |
| μ | viscosity |
| ξ | porosity |
| ρ | density |
| σ | Stefan-Boltzmann constant |
| τ | tortuosity |
| ψ | blocking efficiency |
| ω | mass fraction |
| Ω | |

Subscripts and Indexes:

| | |
|---------------|---|
| a | average quantity |
| ac | of active (decomposable) material |
| air | of air |
| char | of char formed after virgin plastic pyrolysis |
| conv | convective |
| C | carbon |
| CH_4 | methane |
| comb | combustion |
| d | decomposable |
| D | diffusion regime |
| dep | of deposition of carbon |
| eq | equilibrium |
| f | of fluid |
| g | of gases |

| | |
|----------------|-------------------------------------|
| gp | gas phase |
| H | of hydrogen |
| i | species index |
| j | time-step index |
| k | see eq. (24) |
| m | of porous matrix |
| o | initial value |
| O ₂ | of oxygen |
| p | at constant pressure |
| p,pyr | of pyrolysis gas |
| r | reactant |
| R | reaction regime |
| s | of solid; at surface |
| SiO | of silicon monoxide |
| sub | sublimation total |
| trans | transition regime |
| T | temperature |
| v | of void |
| VP | virgin plastic |
| x | in x-direction |
| l | viscous |
| 2 | inertial |
| ∞ | freestream or unsaturated condition |
| + | on positive side of interface |
| - | on negative side of interface |

Superscripts:

- .
- $\bar{}$ time derivative
- $\overline{\quad}$ average quantity
- \rightarrow vector quantity
- $*$ reference quantity
- $/$ corrected value

Mathematical Model

The mathematical model represents a simplified physical model that will be described briefly. The virgin ablation material is considered a porous char filled with decomposable material. When the decomposable material is heated, it decomposes to form a gaseous product. Eventually only the char remains. The gas flows freely toward the heated surface. Within the char, the gaseous hydrocarbons can undergo a deposition reaction which results in carbon depositing in the char and hydrogen gas being formed. The char is assumed to be a combination of carbon and silica. The carbon and silica may react to form gaseous SiO (silicon monoxide) and CO (carbon monoxide). The char at the surface may sublime, burn, and erode which results in surface recession. Thermal expansion and contraction are neglected.

Main Governing Equations

Equation of continuity for the fluid. - The simplified equation assumes that the change in mass flux of the gas equals the change in solid density; that is, there is no capacity term in the gas flow.

$$\frac{\partial \dot{m}}{\partial y} = \dot{\rho}_s \quad (1)$$

Energy equation for the solid. - The thermal conductivity of the solid includes the radiative component. Gaseous conduction is neglected.

$$\frac{\partial}{\partial t} (\rho_s i_s) + \frac{\partial}{\partial y} (\sum \dot{m}_i i_i) = \frac{\partial}{\partial y} (k_s \frac{\partial T}{\partial y}) \quad (2)$$

For use in the CHAD program, this equation is recast as follows:

$$\rho_s c_{p,s} \frac{\partial T}{\partial t} = \frac{\partial}{\partial y} (k_s \frac{\partial T}{\partial y}) - c_{p,g} \dot{m}_g \frac{\partial T}{\partial y} + \sum (H_{T,i} \frac{\partial \rho_i}{\partial t}) \quad (3)$$

where H_T = heat of reaction at temperature T ,

\dot{m}_g = gas flux,

and ρ_i = density of reactant i .

Diffusion equation. - To determine the concentrations of different gases within the ablation material, the following equation is used:

$$\frac{\partial}{\partial y} (C_i - D_i \frac{\partial C_i}{\partial y}) = \dot{C}_i \quad (4)$$

Convection - Diffusion = Source

where C_i = concentration of species i , mass per unit void volume,

\dot{C}_i = source (or sink) of species i ,

D_i = binary diffusivity, used as an approximation of diffusivity in the multicomponent mixture,

and v = velocity in y -direction

Pressure distribution. - The following modified Darcy equation is used for the pressure distribution in the porous media:

$$\frac{\partial P}{\partial y} + \frac{\mu v}{\Gamma_1} + \frac{\rho v^2}{\Gamma_2} = 0 \quad (5)$$

where Γ_1 = viscous permeability

and Γ_2 = inertial permeability.

Equations for thermal and flow properties. - The virgin plastic ablation material undergoes pyrolysis upon being sufficiently heated and eventually reduces to an irreducible char. The properties of the partially decomposed material are considered to vary between those of the virgin material and those of the char. The mathematical model used treats the virgin material as a combination of active (decomposable) material and irreducible char.

Heat capacity of the solid. - The heat capacity of the solid ($\rho_s c_{p,s}$ term) is solved in terms of the virgin plastic and char properties for the pyrolysis reaction zone and beyond. The specific heats are considered to be a function of temperature and are determined by the following cubic equations:

$$c_{p,VP} = E_{VP} + F_{VP} T + G_{VP} T^2 + H_{VP} T^3 \quad (6a)$$

$$c_{p,char} = E_{char} + F_{char} T + G_{char} T^2 + H_{char} T^3 \quad (6b)$$

The cubic coefficients are part of the input data.

In the pyrolysis reaction zone, the char density is held constant. The following equation is used for the heat capacity:

$$\rho_s c_{p,s} = \left[(\rho_{VP} c_{p,VP}) - (\rho_{char} c_{p,char}) \right] \frac{\rho_{ac}}{\rho_{VP} - \rho_{char}} + \rho_{char} c_{p,char} \quad (7)$$

where ρ_{ac} is the density of the active material, and varies between

$$0 \leq \rho_{ac} \leq (\rho_{VP} - \rho_{char})$$

The magnitude of ρ_{ac} depends on the extent of decomposition in the region being considered. It is zero when the material is completely decomposed and is $(\rho_{VP} - \rho_{char})$ when decomposition has not yet been initiated.

Beyond the pyrolysis reaction zone in the direction of the ablation surface, the char density varies because of the char deposition and silica-carbon reactions. The heat capacity of the char in this region is determined as $\rho_{char} c_{p,char}$ using the c_p found from the cubic equation for the char.

Thermal conductivity of the solid. - The thermal conductivities of the virgin plastic and of the char are considered to be functions primarily of temperature and are determined by the following cubic equations:

$$k_{VP} = A_{VP} + B_{VP} T + C_{VP} T^2 + D_{VP} T^3 \quad (8a)$$

$$k_{char} = A_{char} + B_{char} T + C_{char} T^2 + D_{char} T^3 \quad (8b)$$

The cubic coefficients are part of the input data. The following correction is applied to the calculated virgin conductivity to take into account the effect of pressure.

$$k'_{VP} = \left[\frac{k_{VP}}{\left(.622 + 2.164 \frac{T}{P} \right)} \right] + .0001120 \quad (9)$$

In the pyrolysis reaction zone, the thermal conductivity depends on the extent of the decomposition of the virgin material.

$$k_{tot} = (k_{VP} - k_{char}) \left(\frac{\rho_{ac}}{\rho_{VP} - \rho_{char}} \right) + k_{char} \quad (10)$$

Beyond the pyrolysis reaction zone in the direction toward the ablation surface, the char conductivity may at times be considered a function of density as well as of temperature. (The present documented version of the program is not using any variation of char thermal conductivity with density.) Equation (10) is still used, if any decomposable material remains.

Specific heat of the gas. - The specific heat of the gas is considered to be a function of temperature only. It is determined by a cubic equation whose cubic coefficients are included in the input data.

$$c_{p,g} = A_g + B_g T + C_g T^2 + D_g T^3 \quad (11)$$

Viscosity of the gas. - The viscosity of the gas is determined from the following relation:

$$\mu_g = \mu^* \left[\frac{T}{T^*} \right]^{0.7} \quad (12)$$

Where μ^* is the viscosity at the reference temperature T^* .

Molecular weight of the gas. - The average molecular weight of the total gas is found by the following:

$$\bar{M} = \frac{\rho_g}{\sum \left(\frac{\rho_{g,i}}{M_i} \right)} \quad (13)$$

Porosity of the solid. - The porosity of the virgin plastic or of the material in the pyrolysis reaction zone is found by

$$\xi = 1 - \frac{\rho_s}{\rho^*} \quad (14)$$

where ξ = porosity

and ρ^* = theoretical maximum density of the virgin material.

The porosity of the char is found from

$$\xi_{char} = 1 - \frac{\rho_{SiO_2}}{\rho_{SiO_2}^*} - \frac{\rho_C}{\rho_C^*} \quad (15)$$

where $\rho_{SiO_2}^*$ = theoretical maximum density of silica

and ρ_C^* = theoretical maximum density of carbon.

Permeabilities of the solid. - The viscous and inertial permeabilities are given by the following relationships

$$\Gamma_1 = \Gamma_1^* \left(\frac{\xi}{\xi^*} \right)^3 \left(\frac{1 - \xi^*}{1 - \xi} \right)^2 \left(1 + .016 \frac{T}{P}^{1.4} \right) \quad (16)$$

where Γ_1 = viscous permeability,

Γ_1^* = viscous permeability at the reference porosity,

and ξ^* = reference porosity.

$$\Gamma_2 = \Gamma_2^* \left(\frac{\xi}{\xi^*} \right)^2 \left(\frac{1 - \xi^*}{1 - \xi} \right) \quad (17)$$

where Γ_2 = inertial permeability,

Γ_2^* = inertial permeability at the reference porosity,

and ξ^* = reference porosity.

Diffusivities of the gases. - The diffusivity for hydrogen through the other gases in ft^2/sec is found by

$$D_{H_2} = \frac{.0551 T^{3/2}}{(30.48)^2 P \Omega} \quad (18)$$

where

$$\Omega = 0.877 e^{-0.0181 \left(\frac{T}{98} \right)} \left[1 - .007 \left(\frac{T}{98} \right) \right] \quad (19)$$

The diffusivity for each of the other gases through the remaining gas is found by

$$D_{O_2} = \frac{.0308 T^{3/2}}{(30.48)^2 P \Omega} \quad (20)$$

where

$$\Omega = 0.877 e^{-0.0181 \left(\frac{T}{144} \right)} \left[1 - .007 \left(\frac{T}{144} \right) \right] \quad (21)$$

Velocity of the gas. - The velocity of the gas is determined by

$$\overrightarrow{v} = \frac{\overrightarrow{m}_v}{\rho_{g,v}} \quad (22)$$

with the gas density, based on void volume, defined as $\rho_{g,v} = \frac{P \bar{M}}{R T}$ (23)

where $\frac{\dot{m}_v}{M}$ = gas mass flux per void area,
 M = average molecular weight of the gas,
 P = pressure,
 R = gas constant,
 T = temperature,
and $\rho_{g,v}$ = gas density based on void volume

Reaction equations. - There are three different types of in-depth reactions in the ablating material which are provided for in the CHAD program. They are the virgin material decomposition reaction, the carbon deposition reaction, and the silica-carbon reaction.

Virgin material decomposition reaction. - The ablation rate of the virgin plastic is assumed to follow an Arrhenius rate law. The ablation rate is

$$\frac{\partial \rho_{ac}}{\partial t} = - \sum_{k=1}^2 A_k \rho_{VP} \left[\frac{\rho_{ac}}{\rho_{VP} - \rho_{char}} \right]^{n_k} e^{-B_k/T} \quad (24)$$

The Arrhenius equation is present in this form since it readily uses the constants available in the literature and since it behaves in a manner compatible with the ablation model. A series of two reaction terms is used to represent the decomposition of the active material.

Carbon deposition reaction. - The carbon deposition reaction uses a Langmuir-Hinshelwood model. It is

$$\dot{m}_{C,dep} = - \eta^* \times \frac{\{4P_{H_2}y + [(P_{H_2}^2/K_{eq,dep}) - P_{CH_4}]z + 4P_{CH_4}P_{H_2}yz - 4P_{CH_4}P_{H_2}^2y^2z\}}{[1 - P_{H_2}y + P_{CH_4}z - 2P_{CH_4}P_{H_2}yz]^2} \quad (25)$$

For more details on this equation, including values of the constants, see Volume 1, page 23, of this report.

Silica-carbon reaction. - An Arrhenius type equation is used for the reaction of silica and carbon.

$$\dot{m}_{SiO_2} = A_f e^{-B_f/T} \left[\frac{\rho_{SiO_2}}{\rho_{SiO_2,0}} \right]^{n_f} \quad (26)$$

where $\dot{m}_{SiO_2} = lb_m SiO_2$ reacted per $ft^3 \text{-sec}$

ρ_{SiO_2} = density of silica per total volume,

and $\rho_{SiO_2,0}$ = initial density of silica

The reaction constants are part of the input data.

Surface recession equations. - Surface recession results from surface sublimation and combustion and from surface erosion. The combination of these processes gives the total surface recession.

Surface combustion. - The combustion is either reaction-controlled, diffusion-controlled, or a combination of these.

Reaction regime. - For the reaction regime (low surface temperatures), the combustion rate is determined using an Arrhenius type relationship which is

$$\dot{m}_{comb,R} = A \left[\frac{0.21 \cdot P}{2116.2} \right]^n e^{-B/T} \quad (27)$$

For carbon, the constants in this equation are shown in reference 4 to be

$$4.473 \times 10^4 < A < 6.729 \times 10^8$$

$$3.8315 \times 10^4 < B < 3.9855 \times 10^4$$

$$0 < n < 1$$

Generally the reaction order n is taken to be $1/2$.

Diffusion regime. - For moderate surface temperatures, the diffusion regime is the controlling regime. The diffusion controlled combustion rate is (reference 5)

$$\dot{m}_{comb,D} = B^* \psi H \quad (28)$$

The constant B^* , called the blowing parameter, is shown in reference 5 for carbon to be

$$B^* = 0.1737$$

The blowing parameter B^* is usually determined for a reaction between oxygen and a single surface material. Reference 6, however, performs a simplified analysis showing the effects of the ablation gases competing with the surface material for the oxygen in the boundary layer. After a slight modification, the results of the analysis are

$$\dot{m}_{\text{comb}, D} = B^* \psi H - K \dot{m}_g \quad (29)$$

where K is a material property herein called the diffusion reduction parameter. This equation indicates that the combustion rate is reduced due to the oxygen in the boundary layer reacting in part with the ablation gases rather than entirely with the surface.

Transition regime. - The transition regime consists of the gradual transition from the reaction regime to the diffusion regime. The ablation rate is shown in reference 7 to be

$$\left(\frac{1}{\dot{m}_{\text{char, comb}}} \right)^{1/n} = \left(\frac{1}{\dot{m}_{\text{comb}, R}} \right)^{1/n} + \left(\frac{1}{\dot{m}_{\text{comb}, D}} \right)^{1/n} \quad (30)$$

where n is the reaction order. The above equation is used to define the surface combustion rate for all regimes. The heat flux to the surface is increased by the amount of surface combustion, which is assumed to be

$$q_{\text{char, comb}} = \dot{m}_{\text{char, comb}} H_{\text{char, comb}} \quad (31)$$

Surface char sublimation. - At high temperatures the char begins subliming. Reference 7, which analyzes carbon, shows the sublimation rate to be

$$\dot{m}_{\text{char, sub}} = A \dot{m}_{\text{comb}, D} \left[\frac{P_s}{2116.2} \right]^C e^{-B/T} \quad (32)$$

where, for the sublimation of carbon, the constants are

$$A = 1.6 \times 10^7$$

$$B = 1.11 \times 10^5 \text{°R}$$

$$C = 0.67$$

As the char surface sublimes, the heat flux to the surface is reduced by the heat absorbed in char sublimation which is assumed to be

$$\dot{q}_{\text{char, sub}} = \dot{m}_{\text{char, sub}} H_{\text{char, sub}} \quad (33)$$

Surface erosion. - A shear removal correlation for the surface recession of the Apollo ablation material was developed in a previous NASA contract. For ease of analytical input this correlation is divided into three straight lines for use in the CHAD program (see Volume 1, page 35), and the amount of material lost by shear removal is included in the surface recession calculated.

Ablation surface heating. - The heat flux to the surface is the sum of a number of individual fluxes

$$\dot{q}_{\text{tot}} = \dot{q}_{\text{misc}} - \dot{q}_{\text{rad}} + \dot{q}_{\text{comb, g}} - \dot{q}_{C, \text{sub}} + \dot{q}_{\text{comb, s}} - \psi \dot{q}_{\text{conv}} \quad (34)$$

| | | |
|-------|----------------------------|--|
| where | \dot{q}_{tot} | = total flux, |
| | \dot{q}_{misc} | = unblocked heating to surface, |
| | \dot{q}_{rad} | = heat reradiated by ablation surface, |
| | $\dot{q}_{\text{comb, g}}$ | = gas phase combustion, |
| | $\dot{q}_{C, \text{sub}}$ | = carbon sublimation, |
| | $\dot{q}_{\text{comb, s}}$ | = surface combustion, |
| | ψ | = blocking factor, |
| and | \dot{q}_{conv} | = unblocked convective heating. |

Procedure of Solution

The calculation of temperatures is the backbone of the solution. The size of the time step and the decision on whether or not to reiterate at a given time step is controlled by the amount of deviation between estimated and calculated temperatures.

The one-dimensional heat equation is solved by the implicit Crank-Nicolson finite difference method (reference 8). The material properties which are functions of a number of variables, particularly temperature, are determined at a temperature which is an average of the old-calculated and the new-estimated temperatures. The variables other than temperature are largely decoupled from each other.

In the Crank-Nicolson finite difference procedure, a matrix equation of the form $A \bar{T} = d$ results where A is a tridiagonal matrix. The set of simultaneous equations is reduced by Gauss elimination.

The order of solution is briefly:

- (1) Internal gas pressures are calculated from the modified form of Darcy's equation.
- (2) The gas component concentrations are separately determined by an implicit finite-difference solution of the diffusion equation.
- (3) Temperatures and decomposable densities are estimated for the end of the time step ($j + 1$).
- (4) Surface recession is determined. This establishes the position of moving nodes at times $(j + 1/2)$ and $(j + 1)$.
- (5) Decomposable densities are calculated via an Arrhenius type equation. Pyrolysis gas rate and pyrolysis reaction heat are found for each node.
- (6) Similarly, the silica-carbon and the carbon deposition reactions are calculated to determine the silica and carbon densities, the sources of silicon monoxide and carbon monoxide, and the sink for pyrolysis gas.
- (7) Thermal conductivity and thermal capacity are determined.
- (8) The elements of the tridiagonal matrix for the temperature determinations are calculated and are reduced by Gauss elimination.
- (9) The front ablation surface heat balance is calculated.
- (10) Temperatures are calculated from the front to the back.
- (11) If the temperatures estimated agree (within the error criterion) with those calculated, the time step is complete. Otherwise, the process from step 3 through step 10 is repeated. If the process does not succeed in 3 attempts, the time step is reduced in size.

RESULTS AND DISCUSSION

The accuracy of the program is difficult to verify when it is run with all-possible complexities, such as reactions, surface recession, and variable thermal and flow properties.

The basic one-dimensional solid thermal conductivity model within the program has been verified to give excellent agreement with analytical results determined independently for the following cases:

1. Finite slab, constant properties, uniform initial temperature, insulated at the rear surface, constant heat flux at the front surface.
2. Finite slab, constant properties, uniform initial temperature, insulated at the rear surface, constant temperature at the front surface.
3. Semi-infinite slab, constant properties, variable initial temperature, constant temperatures at both surfaces, one surface which is moving with a constant velocity.

The other parts of the program - those sections where surface recession rates, gas component concentrations, internal and surface reaction rates, and internal gas pressures and velocities are determined - were checked separately by comparing their results with expected results.

CONCLUSIONS AND RECOMMENDATIONS

The CHAD program is based upon the CHAP program which has been used successfully for nearly three years. The CHAD program which has been developed from it through modification is a very versatile tool for the examination of new parameters not previously open to examination, such as the effect of permeability, diffusivity, char-density changes, char-deposition reaction, and the silica-carbon reaction. It will find its greatest initial use in the investigation of these parameters.

Because the contract for which CHAD was developed was a study of the Apollo heat shield performance, the program is rather specific to this material. In addition, because it is a modification of a more general program [and was kept compatible with that program (CHAP), so that it might be used as a part of it] it contains many parts from CHAP which are not needed in the present CHAD program.

In its present form, CHAD can be considered as a good basis for a more generalized ablation performance prediction program.

INPUT-OUTPUT

Input

All user supplied input is via punched cards. There are two types of data cards provided to the program. One type is the standard data cards; the other type is a set of block data subroutine cards. The standard data cards are in the order: TITLE, TABLES, MATERIALS, and INITIAL TEMPERATURE.

Standard data card input, TITLE. - The first data card is the title card, and all information in columns 1-72 on this card is printed out on the run output.

Standard data card input, TABLES. - There must be four tables provided. Either table 3-1 or table 3-2 is input, not both. The independent variable in all cases is time. The tables must be in the order of increasing time except for the last card. The last card, which is not actually a point of the table, has time equal to zero to signal the end of the table. From the four tables, the lowest maximum time is picked for the end problem time. Each of the tables can have a maximum of 99 data points. The tables are listed below:

| Table | Card no. | Card type | Format | Columns | Value |
|---------------------------------------|----------|--------------|--------|---------|---|
| 1. Max. calculation time-step control | 1 | Table no. | 110 | 1-10 | 1 |
| | 2 to n-1 | Table points | 2F10.0 | 1-10 | Time, sec |
| | | | | 11-20 | Max. calcula- tion time-step, sec |
| | n | End | F10.0 | 1-10 | 0 |
| 2. Print time-step control | 1 | Table no. | 110 | 1-10 | 2 |
| | 2 to n-1 | Table points | 2F10.0 | 1-10 | Time, sec |
| | | | | 11-20 | Print time-step, sec |
| | n | End | F10.0 | 1-10 | 0 |
| 3-1 Surface heat flux | 1 | Table no. | 2110 | 1-10 | 3 |
| | | | | 11-20 | 1 |

| <u>Table</u> | <u>Card no.</u> | <u>Card type</u> | <u>Format</u> | <u>Columns</u> | <u>Value</u> |
|---|-----------------|------------------|---------------|----------------|---|
| 3-1 Surface heat flux (Concluded) | 2 to n-1 | Table points | 4F10.0 | 1-10 | Time, sec |
| | | | | 11-20 | Recovery enthalpy Btu/lb _m |
| | | | | 21-30 | Heat transfer parameter, lb _m ² /ft ² -sec |
| | | | | 31-40 | Heat flux unaffected by blocking, Btu/ft ² -sec |
| | n | End | F10.0 | 1-10 | 0 |
| 3-2 Surface temperature | 1 | Table no. | 2110 | 1-10 | 3 |
| | | | | 11-20 | 2 |
| | 2 to n-1 | Table points | 2F10.0 | 1-10 | Time, sec |
| | | | | 11-20 | Temperature, °R |
| | n | End | F10.0 | 1-10 | 0 |
| 4. Local static pressure and flow condition | 1 | Table no. | 110 | 1-10 | 4 |
| | 2 to n-1 | Table points | 4F10.0 | 1-10 | Time, sec |
| | | | | 11-20 | Local static pressure, lb _f /ft ² |
| | | | | 21-30 | 1. for laminar or 2. for turbulent |
| | | | | 31-40 | Local shear stress, lb _f /in ² |
| | n | End | F10.0 | 1-10 | 0 |

The maximum calculation time-step control table is used to set the maximum time-step that the program may use in the calculation. The print time-step control table sets the times for print. The following table will illustrate.

| <u>Time</u> | <u>Print Time Step</u> |
|-------------|------------------------|
| 0. | 3. |
| 10. | 50. |
| 100. | 300. |
| 1000. | 300. |

The times that would be printed are 0., 3., 6., 9., 10., 60., 100., 400., 1000. Table 3-1, the surface heat flux table, provides the data for a heat flux drive to the ablation surface while Table 3-2, the surface temperature table, provides a temperature drive for the ablation surface. Table 4, the local static pressure and flow condition table needs no added explanation.

Standard data card input, MATERIALS and INITIAL TEMPERATURE. - The material widths and noding are input by cards in the format shown below. They are ended by a final card with a zero for the material number.

| <u>Card no.</u> | <u>Card type</u> | <u>Format</u> | <u>Columns</u> | <u>Value</u> |
|-----------------|------------------|---------------|----------------|---------------------|
| 1 to n-1 | Material | I10 | 1-10 | Material number |
| | | 2A6 | 11-22 | Material name |
| | | F10.4 | 31-40 | Material width, in. |
| | | I10 | 41-50 | Number of nodes |
| n | End | F10.0 | 1-10 | 0 |

Materials are numbered from 1 to 10. The material number must correspond to the proper material data in the block data subroutine. In the supplied block data subroutine Material 1 is AVCOAT 5026-39/HC-G and Material 2 is aluminum (2024T3). The order of the material cards must be from back surface to front ablation surface.

The final data card is the initial temperature card:

| <u>Card type</u> | <u>Format</u> | <u>Columns</u> | <u>Value</u> |
|---------------------|---------------|----------------|--------------------------------------|
| Initial temperature | F10.4 | 1-10 | Initial temperature for all nodes |

Block data input. - Material properties, reaction constants, erosion constants, nodal spacing, and initial temperatures are introduced as data via a block data subroutine, BLKD/D2. See page 99 for a listing of the block data program from the sample cases. All cards above the second DATA statement card are always required

without change as is the final END card. Data is introduced by the DATA statement cards which have the following format:

DATA list/d₁, d₂, ..., d_n/, list/d₁, d₂, k*d₃, ..., d_m/, ...

where

1. list contains the names of the variables being defined,
2. d's are the values corresponding to the variables in list,
- and 3. k is an integer constant which indicates the number of times the value is repeated.

(Block data subroutines and DATA statements are a standard part of FORTRAN IV)

The required DATA statements fall into the following groups:

Material 1 data

Material 2 data

Material J data (J = 1 to 10)

Char data

Gas data

Internal flow and diffusion constants

Miscellaneous data

Each group will be separately considered and described. A sign ▲ is used to mark the required data values.

Material J Data

- ▲ ACTENV (I, J), I = 1, n n = 1 to 2 Activation temperature (^oR)
- ▲ EFCOLV (I, J), I = 1, Collision frequency (1/sec)
- ▲ REORDV (I, J), I = 1, Reaction order

The above reaction constants are for the pyrolysis reaction of the decomposable material. Up to 2 simultaneous reactions may be used to describe the pyrolysis reaction, in which case n = 2, see equation (24).

- ▲ HOFM (J) Heat of pyrolysis at 536.67 ^oR (Btu/lb_m)
- ▲ COEFT (I, J), I = 1, 4 Cubic coefficients for virgin specific heat equation
- ▲ CONST (I, J), I = 1, 4 Cubic coefficients for virgin conductivity equation

The conductivity and specific heat of the virgin material are inserted as a function of temperature in the form of cubic equations. The equations are represented as

$$k = A + BT + CT^2 + DT^3$$
$$c_p = E + FT + GT^2 + HT^3$$

where

COEFT (1, J) = A = Constant term ($\text{Btu-in}/\text{ft}^2 \text{-sec}^{-2} \text{R}$)

COEFT (2, J) = B = Linear term

COEFT (3, J) = C = Square term

COEFT (4, J) = D = Cubic term

and

CONST (1, J) = E = Constant term ($\text{Btu}/\text{lb}_m \text{-}^{\circ}\text{R}$)

CONST (2, J) = F = Linear term

CONST (3, J) = G = Square term

CONST (4, J) = H = Cubic term

- ▲ EMIS (J) Virgin emissivity
- ▲ ABSORP (J) Virgin absorptivity
- ▲ RHOV (J) Virgin density (lb_m/ft^3)
- ▲ SLOPE (J) Transpiration factor for ablation gases. This value is the value for laminar flow

Material data is listed for each separate material.

Char Data

- ▲ ACTENC Activation temperature ($^{\circ}\text{R}$)
- ▲ EFCOLC Collision frequency (1/sec)
- ▲ REORDC Reaction order
- ▲ HCOM Heat of combustion (Btu/lb_m)
These reaction constants are for the surface combustion reaction
- ▲ ACTENS Activation temperature ($^{\circ}\text{R}$)
- ▲ EFCOLS Collision frequency (1/sec)

| | |
|---------------------|---|
| ▲ REORDS | Reaction order |
| ▲ HSUB | Heat of sublimation (Btu/lb _m) |
| | These reaction constants are for surface sublimation. |
| ▲ CCPC (I), I = 1,4 | Cubic coefficients for char specific heat equation |
| ▲ CKC (I), I = 1,4 | Cubic coefficients for char conductivity equation |
| ▲ EMISC | Char emissivity |
| ▲ ABSC | Char absorptivity |
| ▲ RHOC | Char density after pyrolysis and before char deposition or silica-carbon reaction (lb _m /ft ³) |
| ▲ TRCHAR | Transpiration factor for the char combustion and char sublimation gases |
| ▲ CHARRO | The carbon density in the char formed by pyrolysis (lb _m /ft ³) |

Gas Data

| | |
|---------------------|--|
| ▲ CCPG (I), I = 1,4 | Cubic coefficients for gas heat capacity (Btu/lb _m -°R for the constant term) |
| ▲ HCOMG | Heat of combustion for the gas phase at the surface (Btu/lb _m) |

Internal Flow and Diffusion Constants

| | |
|----------|--|
| ▲ CARTS | Theoretical maximum density of carbon (lb _m /ft ³) |
| ▲ RHOTS | Theoretical maximum density of the char formed by pyrolysis and before char deposition of silica-carbon reaction (lb _m /ft ³) |
| ▲ SILTS | Theoretical maximum density of silica (lb _m /ft ³) |
| ▲ PORT | Reference porosity for permeability calculation -- equations (16) and (17) |
| ▲ PERT1 | Reference viscous permeability for viscous permeability calculation -- equation (16) (ft) |
| ▲ PERT2 | Reference inertial permeability for inertial permeability calculation -- equation (17) (ft) |
| ▲ VISCO | Reference viscosity in viscosity calculation -- equation (12) (lb _m /ft-sec) |
| ▲ VISCON | Reference temperature for reference viscosity (°R) |

| | |
|---------|--|
| ▲ DCOCM | Carbon monoxide |
| ▲ DCODP | Gases other hydrogen produced in deposition reaction |
| ▲ DCOH | Hydrogen |
| ▲ DCON | Nitrogen |
| ▲ DCOO | Oxygen |
| ▲ DCOPY | Methane |
| ▲ DCOSI | Silicon monoxide |
| ▲ ANMW | Molecular weight of nitrogen |
| ▲ AOMW | Molecular weight of oxygen |
| ▲ BMW | Molecular weight of carbon monoxide |
| ▲ DMW | Molecular weight of deposition gas |
| ▲ HMW | Molecular weight of hydrogen |
| ▲ PMW | Molecular weight of methane |
| ▲ SMW | Molecular weight of silicon monoxide |

These are the constants D_C for the ablating surface diffusion where
 $D = D_C \psi H$

Miscellaneous Constants

| | |
|--------------------|--|
| ▲ BSTAR | Blowing parameter |
| ▲ DIFC(1), 1 = 1,4 | Cubic coefficients for diffusion reduction parameter calculation -- equation (29) |
| ▲ QSI | Heat of reaction for the silica-carbon reaction (Btu/lb _m of reactants) |
| ▲ QDEP | Heat of reaction for the carbon deposition reaction (Btu/lb of carbon deposited) |
| ▲ QBRN | (Not in use) |
| ▲ AF | Collision frequency for silica-carbon reaction (1/sec) |
| ▲ BF | Activation temperature for silica-carbon reaction (°R) |
| ▲ SILICA | Initial density of silica before the silica-carbon reaction begins |
| ▲ REO | Reaction order of the silica-carbon reaction |

▲ CX(I), I = 1, 6 Values for the carbon deposition reaction (see equation (25) on page 12). The relationship is as follows:

$$\begin{array}{ll} CX(1) &= X \\ CX(2) &= Y \\ CX(3) &= Z \end{array} \left. \begin{array}{l} \\ \\ \end{array} \right\} \text{for } P_{H_2} \leq .02834 \text{ atm}$$
$$\begin{array}{ll} CX(4) &= X \\ CX(5) &= Y \\ CX(6) &= Z \end{array} \left. \begin{array}{l} \\ \\ \end{array} \right\} \text{for } P_{H_2} > .02834 \text{ atm}$$

Listing of Input

The listing of data card input is included with each sample case. The block data input used with these sample cases may be found as the first subroutine listing in the Program Listing section of this report.

Output

The two sample cases may be referred to as examples of output listing.

OPERATING INSTRUCTIONS

Deck Setup

The deck setup for a run requires, in addition to the usual control cards and data cards, the inclusion of the block data subroutine. For the SRU 1108 computer with the program tape, the deck setup will be as follows:

[Initial Control Cards]

ASG A = (Program Tape No.)

XQT CUR

TRW A

IN A

TRI A

[Block Data Subroutine]

XQT MAIN

[Data Cards]

Run Time and Amount of Output

A typical run time for an Apollo heating rate input is six minutes on the SRU 1108 computer. Two or three pages of output are printed for each time point requested in the data input.

PROGRAMMING INFORMATION

Program Design

The original CHARM program was completely rewritten to make it a part of the CHAP program. This gave a combined program with both a complex ablation program and a sophisticated convective heating routine. The CHAD computer program described herein was developed from the ablation analysis part of CHAP by deleting the convective heating routines and adding input and output routines, two more internal reaction calculations, an internal pressure determination, and the calculations of gas concentrations by the diffusion equation.

Noding. - The materials are divided into major nodes which are numbered consecutively from 1 to n, n being the total number of major nodes. At the ablation surface and in the region where the virgin decomposition reaction is occurring, a higher number of nodes is needed than elsewhere. The major nodes are subdivided in these regions into more nodes which are called minor nodes. The subdivided regions are called zones - the front zone and the reaction zone. The ratio of minor nodes to major nodes is called the "nodal density".

Temperatures are estimated and calculated at nodal interfaces. When one node is of one material type and the next node is of another material type, the temperature at the nodal interface in-between is applied only to the adjacent half-nodes for reaction calculations and decomposable density calculations.

Movable node. - Only the front major node is a movable node. It is divided into equal-size minor nodes. As the ablation surface recedes, these minor nodes decrease equally in size. Corrections for this nodal shift are made for values involved.

Subscripting and storage. - The major nodes are stored according to their nodal numbers. The minor nodes are stored starting at 119 in the storage array for zone 1 and at 187 for zone 2. The decomposable densities for the upper half-nodes which are next to major nodal interfaces are the only ones necessary to calculate or store. They are stored starting at 205 in the storage arrays for densities.

Grouping. - The procedure of calculation has been set up on the basis of groups of nodes. The nodes are divided by the calculation control section into groups of nodes which satisfy the following:

1. All the nodes of a group are either in no zone or the same zone.
2. All the nodes of a group are either non-moving nodes or moving nodes.
3. No more than 40 minor or major nodes are allowed in a group.

Problem types. - The original setup of CHAP provided for three problem types: 1) nodes changing at the surfaces but not in the center; 2) nodes changing only at the ablation surface, and 3) all nodes changing. The present CHAD program is fixed at problem type 3.

Temperature calculation. - Temperatures are calculated by reducing the matrix elements of nodal groups from the back surface to the ablation surface. The front group temperatures are then found. If they deviate by more than set limits from predicted temperatures, the front group temperatures are again predicted and calculated. All temperatures of other groups are calculated. If any calculated temperature deviates by more than the set limits from predicted temperatures, all temperatures are again predicted, and temperatures of all groups are again calculated. If the third iteration has not resulted in calculated and predicted temperatures that are within the limits, the size of the time step is reduced. By this procedure, problem stability is obtained while the time step is kept as large as possible.

Node shifting and combining. - The front major node is movable; that is, it changes in size. If the major node next to it is of the same material type, the two are combined whenever the front major node reaches one-half the size of the original node that was added to the front node. If the two front nodes are of different materials, the front node is allowed to decrease in size to zero. The time step is controlled so that the front node goes to zero just at the end of the time step.

Main Routine and Subroutine Description.

Purpose of each subroutine. - MAIN is the main routine. It is a short routine which handles the input of the initial required data and the output of this initial data, the control of the calculation time step, the control of the output of calculated information, and the control of the ending time for the problem calculation. Other than system or utility routines there are only three subroutines which are called from MAIN: WRITE and CHARM.

WRITE is the output routine for calculated data.

CHARM does the calculation of the ablation analysis with the help of a large number of subroutines that it calls upon.

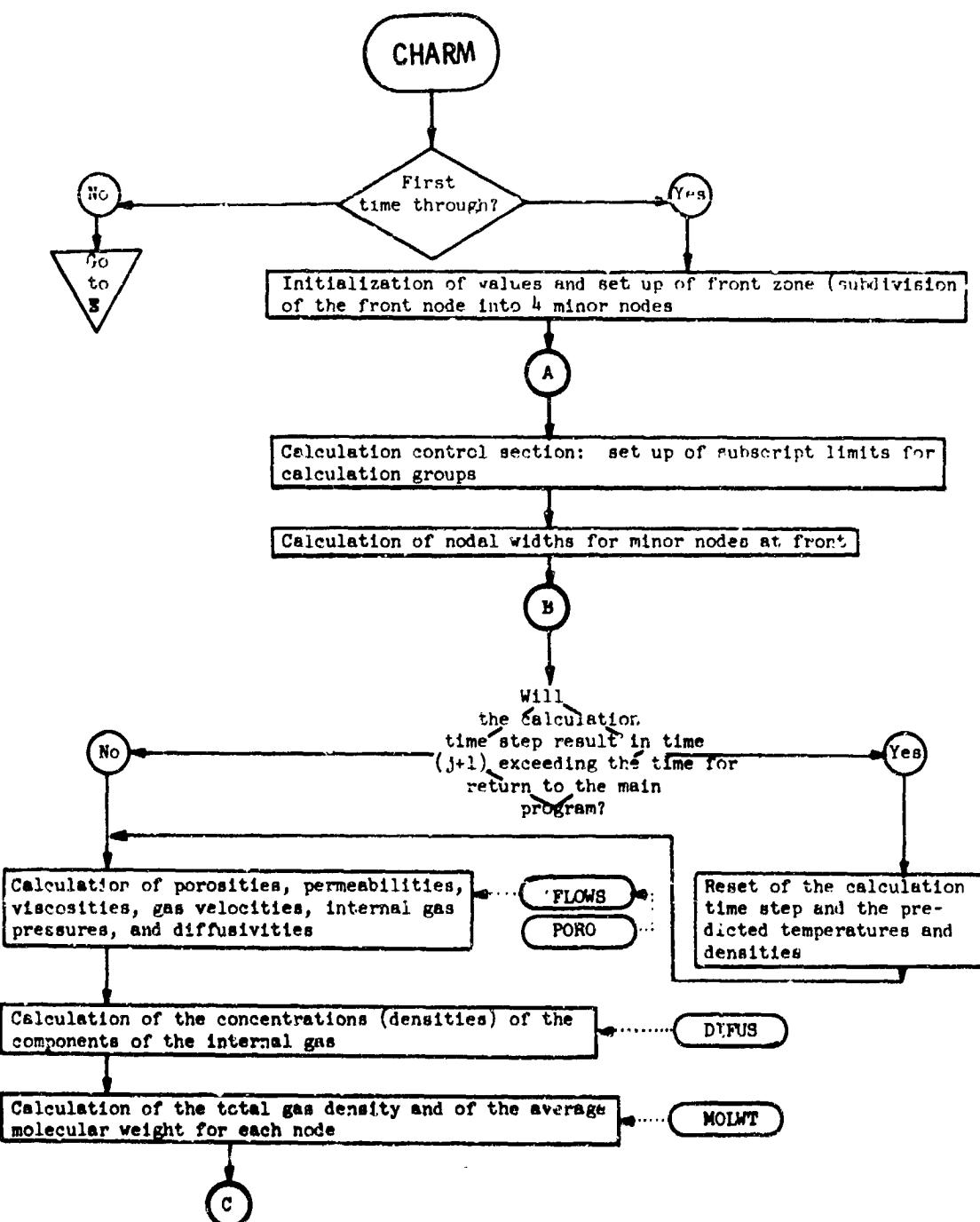
All subroutines are now listed in alphabetical order. They are classified as CHARM, CHARM-Name, WRIT or Utility subroutines. Subroutines called from CHARM are classified as CHARM, subroutines reached from a subroutine called from CHARM are classified as CHARM-Name, and subroutines used by a number of subroutines are classified as Utility.

| Subroutine | Classification | Function |
|------------|----------------|---|
| BLKD/D2 | Utility | Provides input data to the program. It is a Block Data subroutine |
| BLOCK | CHARM | Calculates the blocking function |
| CHARM/S4 | | Calculates ablation analysis with help of many subroutines |
| COMBIN | CHARM-FRONT | Combines 2 front major nodes into 1 major node. |
| CONDIF | CHARM | Calculates thermal conductivity |
| CPBA | CHARM | Calculates internal gas specific heat |
| DEPO | CHARM | Calculates the rate of carbon deposition and the change in solid carbon density |
| DIFUS | CHARM | Calculates the concentrations of the gaseous components |

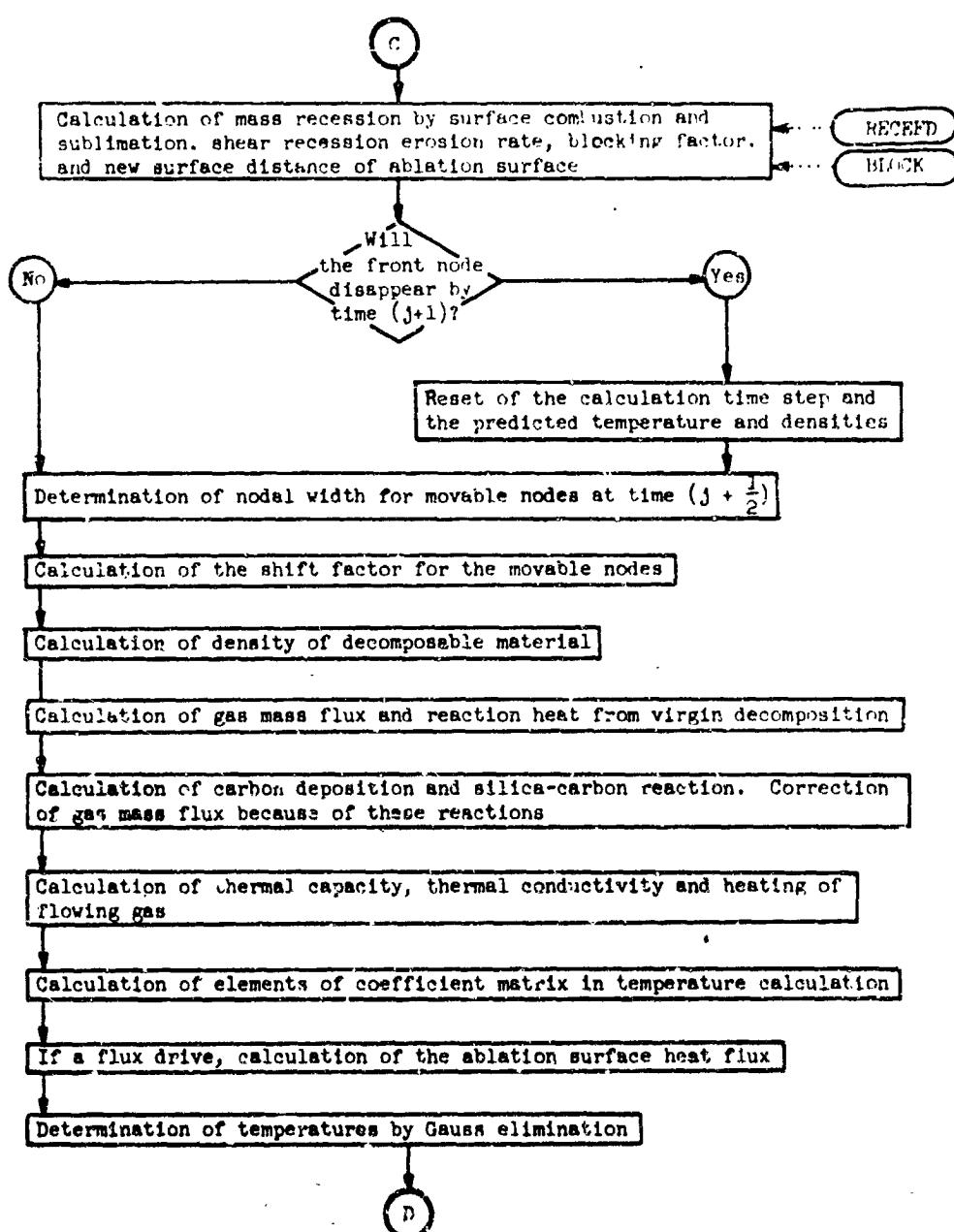
| <u>Subroutine</u> | <u>Classification</u> | <u>Function</u> |
|-------------------|-----------------------|---|
| FLOWS | CHARM | Calculates the internal pressures, internal gas velocities and the diffusion coefficients for hydrogen and other gases |
| FONEV | Utility | Linearly interpolates the value of $f(x)$ from a table given the independent variable x |
| FREC | CHARM-RECEED | Calculates a simple arithmetic function for RECEED |
| FRONT | CHARM | Determines whether to drop the front major node, to combine it with the one next to it, or to divide the major node next to the front |
| GPCOM | CHARM | Calculates the heat to the ablating surface from exterior gas phase combustion |
| GRIN | Utility | Provides the subscripting from arrays needed for calculation |
| ITER8 | CHARM-RECEED | Finds a solution for x in the equation $x = f(x)$ |
| IWR | CHARM | Calculates enthalpy given the temperature and the compressibility factor |
| LLD | Utility | Determines the major node number given a minor node number |
| MOLWT | CHARM | Calculates the molecular weight of the internal gas from the gas component concentrations |
| PCAPF | CHARM | Calculates the thermal capacity of a node (or half-node) |
| PORO | CHARM-FLows | Calculates the porosities and permeabilities of the solid and the viscosities of the internal gas |

| <u>Subroutine</u> | <u>Classification</u> | <u>Function</u> |
|-------------------|-----------------------|--|
| RECEED | CHARM | Determines the material lost by carbon combustion and carbon sublimation |
| RHOSB | CHARM | Determines the rate of virgin decomposition and required accessory values |
| SHIFT1 | CHARM CHARM-FRONT | Shifts storage of minor nodes and adds values to zone storage when a major node is subdivided |
| SHIFT 2 | CHARM | Shifts location of minor nodes in zone storage |
| SIC | CHARM | Calculates the rate of the silica-carbon reaction and the changes in silica and carbon densities |
| SUBZ | CHARM | Calculates the compressibility factor given the temperature and pressure |
| TBSTEP | Utility | Finds the value of the step function $f(x)$ given the independent variable x |
| WRITE | | Outputs all desired calculated information |

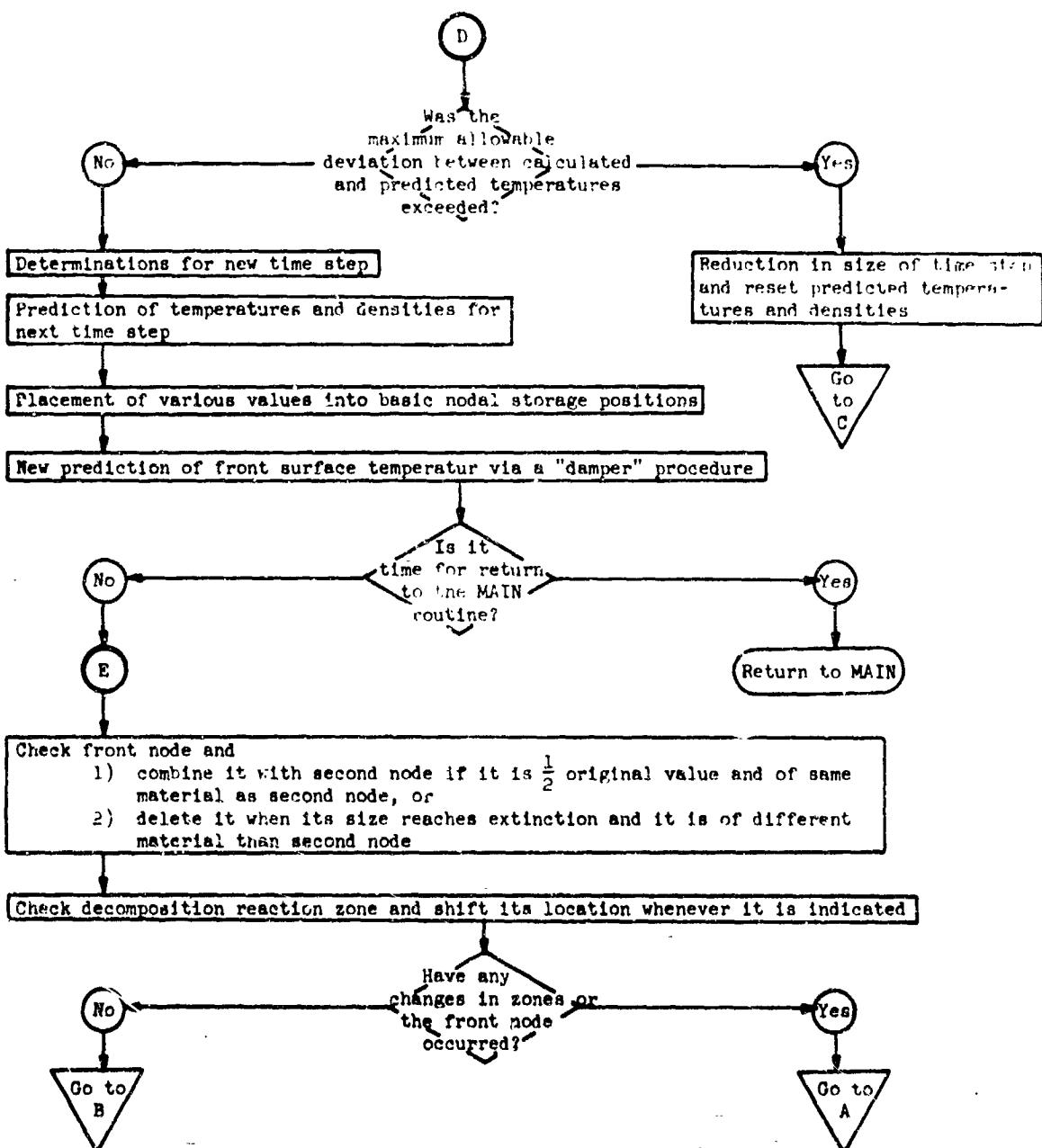
Flow charts. - Most of the subroutines are relatively simple and have been described in the previous section. A few subroutines are of sufficient complexity to warrant flow charts for the program user. They are CHARM, COMBIN, DIFUS, FRONT, and SHIFT1 and are presented here in that order.

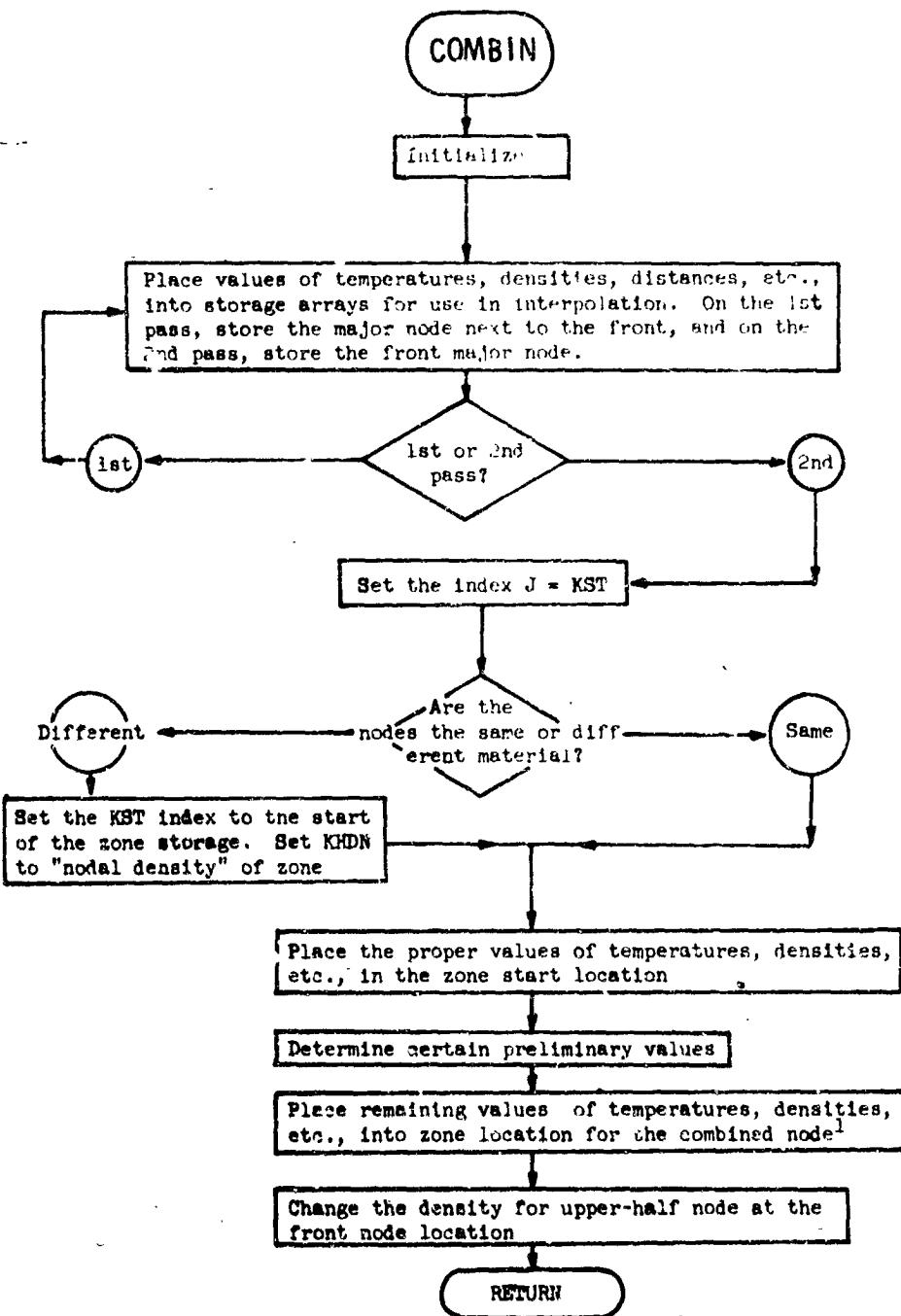


CHARM (Continued)

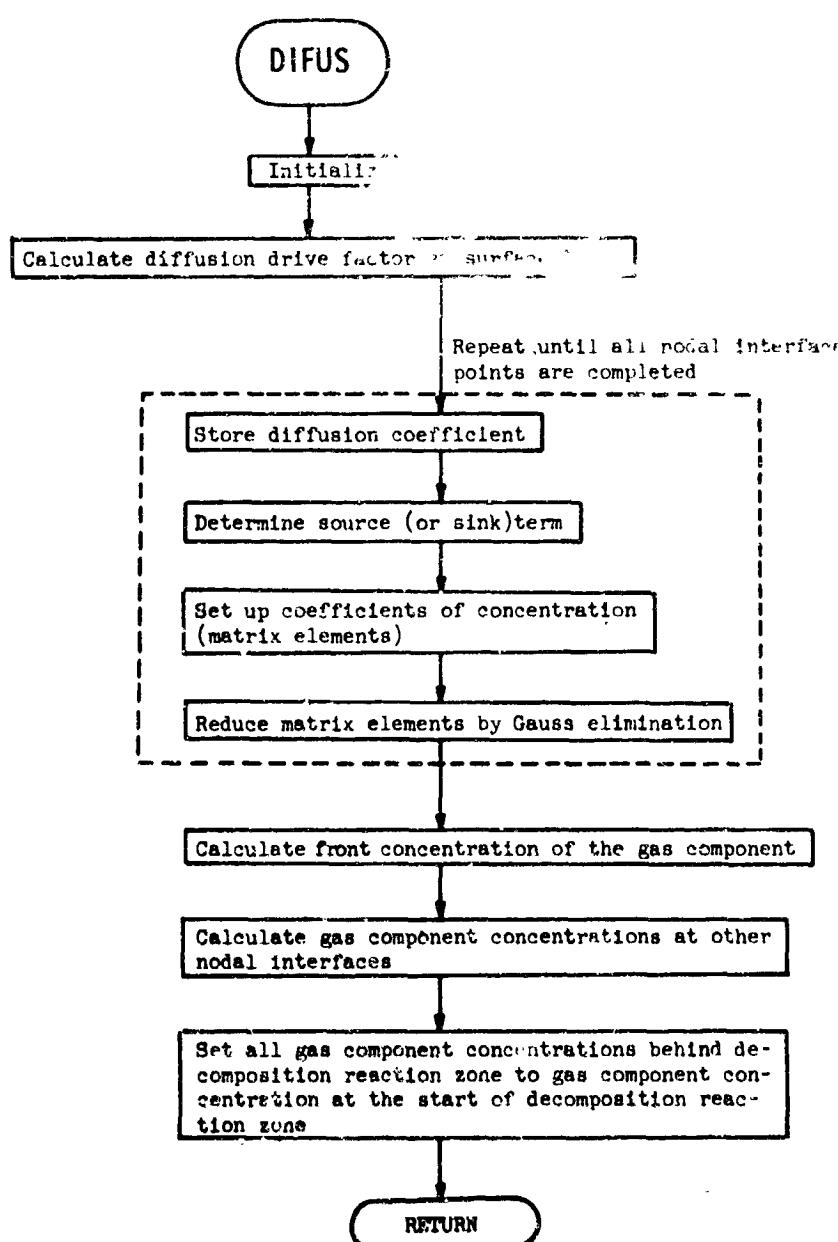


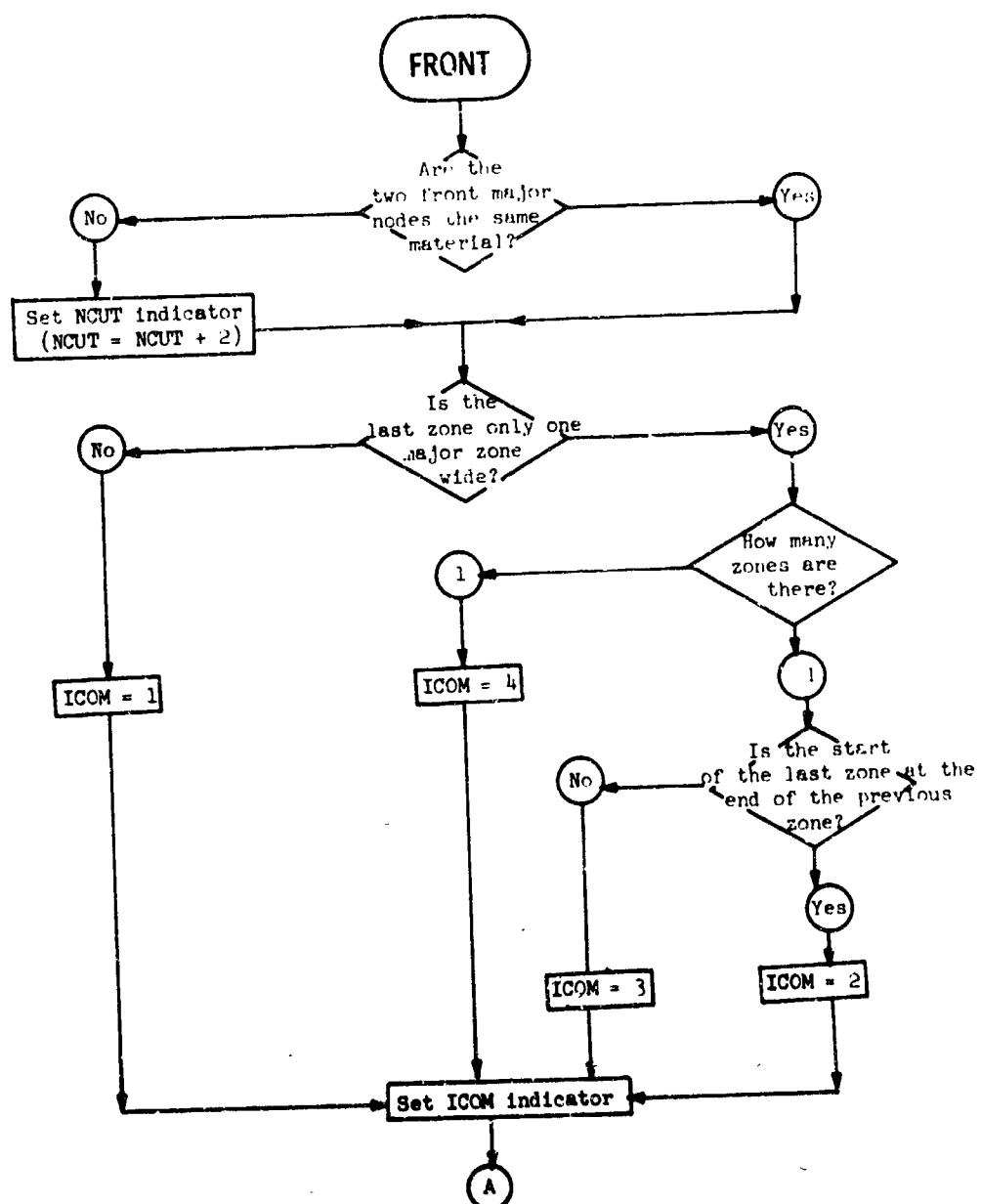
CHARM (Continued)

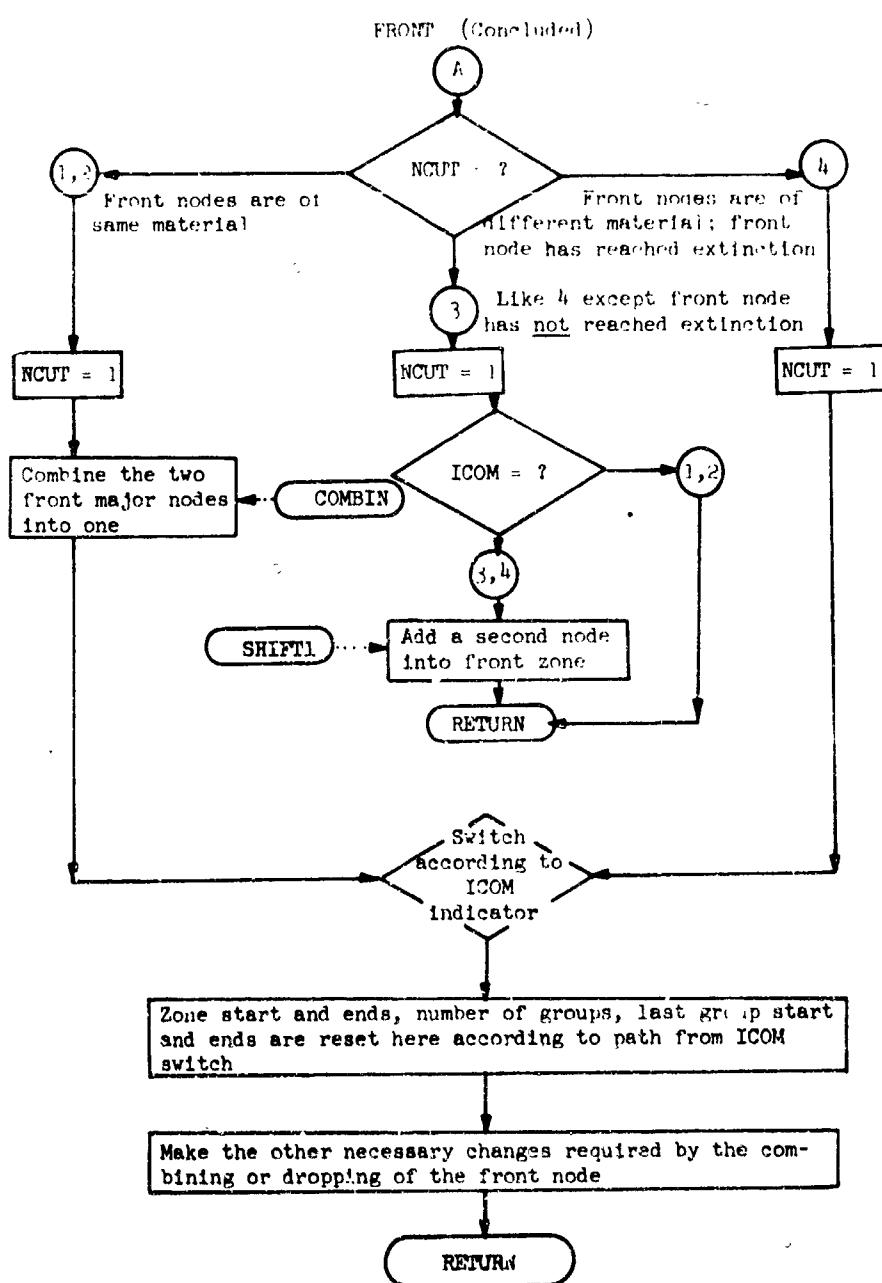


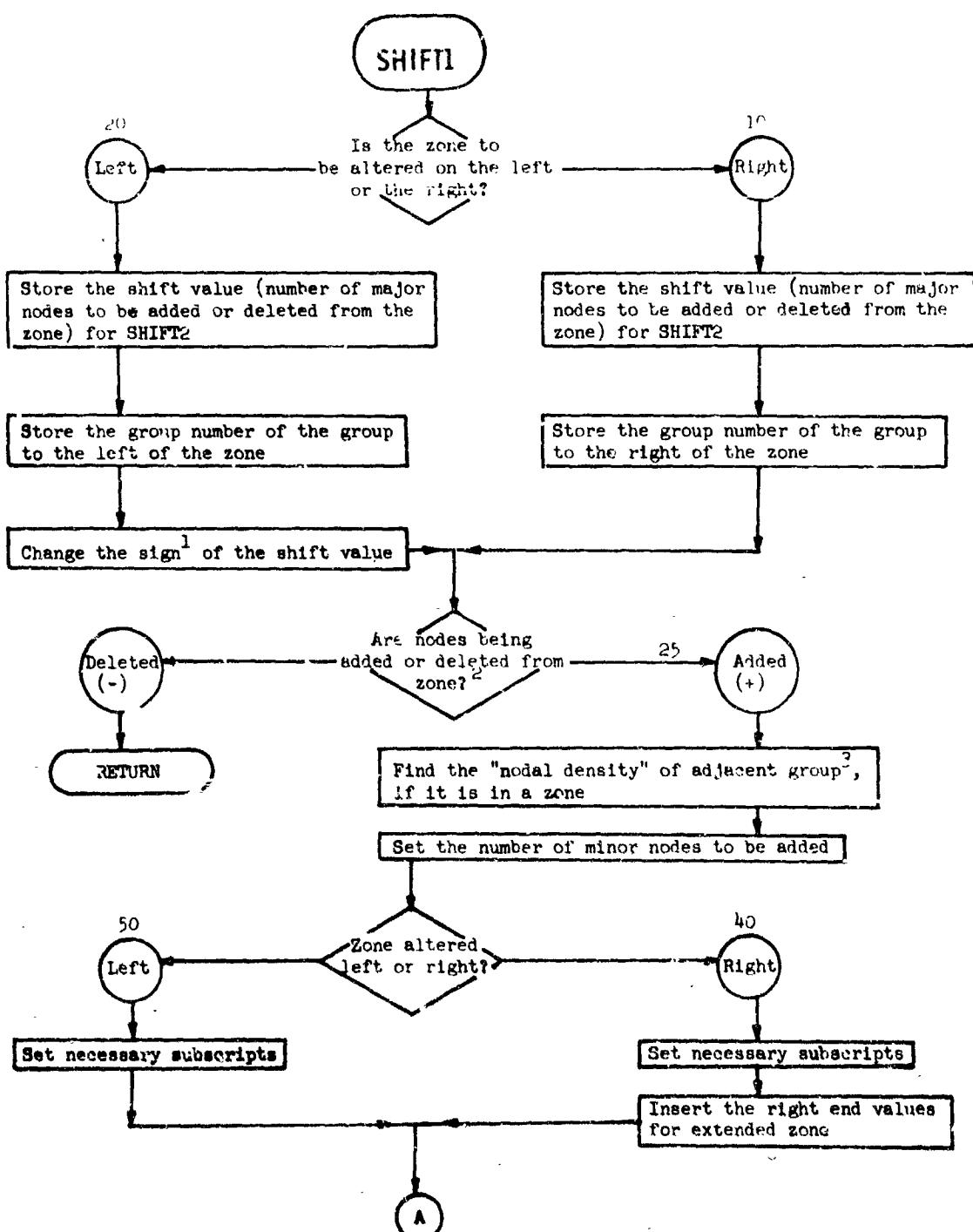


¹ In the case of different materials for the two front nodes, the front node is dropped because it is at extinction and the second node is placed in the zone storage position.

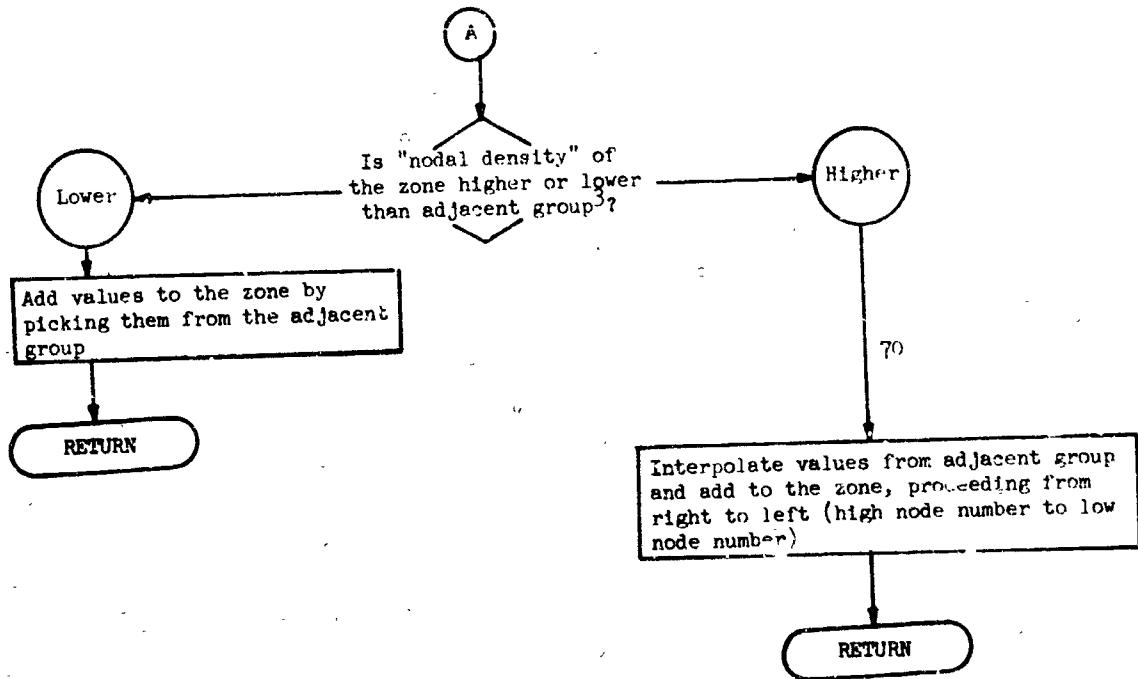








SHIFT1 (Concluded)



- 1 The sign of the shift value is minus for zone boundary movement to the left and positive for zone boundary movement to the right..
- 2 The sign of the shift value at this point indicates whether nodes are being added (+) or deleted (-).
- 3 The adjacent group is the group next to the zone side which is being added to.

Program nomenclature. - The nomenclature of all CHAD routines is included in the following section. The listing indicates a subroutine only when the quantity is specific to that subroutine.

| <u>Program Symbol</u> | <u>Math. Symbol</u> | <u>Dim. Units</u> | <u>Subroutine</u> | <u>Description</u> |
|-----------------------|---------------------------|-------------------------|-------------------|--|
| A | A_i | BTU/sec- $^{\circ}$ R | CHARM | Coefficient of temperature $(T_{i+1} - T_{i-1})$ |
| A | $\frac{n^A}{A}$ | None | BLOCK | Term in equation for blocking function. |
| A | A_g | ft/sec. | DIFUS | Coefficient of gas component concentration $(C_{I,i+1} - C_{I,i-1})$ |
| | | | ITER8 | Temporary value calculated in this subroutine |
| ABSC | α_c | None | | Char absorptivity for thermal radiation |
| ABSORP | α_v | None | | Virgin absorptivity for thermal radiation |
| ABVAL | ϵ | None | | Relative absolute error of calculated temperature: $\epsilon_{\text{calc}} = \frac{T_{\text{calc}} - T_{\text{pred}}}{T_{\text{pred}}}$ |
| ABVALM | $\epsilon_{s,\text{max}}$ | None | | Maximum relative absolute error for front group |
| ABVALS | ϵ_{max} | None | | Maximum relative absolute error for all groups except the front group |
| ACTENC | A_c | $^{\circ}$ R | RECEED | Activation temperature for char combustion |
| ACTENS | A_s | $^{\circ}$ R | RECEED | Activation temperature for char sublimation |
| ACTENV | A_v | $^{\circ}$ R | RHOSE | Activation temperature for virgin decomposition |
| AERN | C_N | lbm/ ft^3 void | | Concentration of nitrogen in gas phase |
| AERO | C_O | lbm/ ft^3 void | | Concentration of oxygen in gas phase |

| Program Symbol | Math. Symbol | Dim. Units | Subroutine | Description |
|----------------|--------------|--|------------|--|
| AF | β_{si} | 1/sec | SIC | Collision frequency for silica-carbon reaction |
| AIRM | M_{air} | lb _m /mole | | Molecular weight of air (28.96) |
| ALLGAS | C_T | lb _m ³ /ft ³ void | | Concentration of total gas in the gas phase |
| ALP | v_i^j | ft/sec | DIFUS | Gas velocity of node i at time j |
| ALPH | v_{i-1}^j | ft/sec | DIFUS | Gas velocity of node i-1 at time j |
| AI.PHA | v_{i+1}^j | ft/sec | DIFUS | Gas velocity of node i+1 at time j |
| ALPHA | v_i^j | ft/sec | FLows | Temporary storage for gas velocity |
| ANMW | M_N | lb _m /mole | | Molecular weight of nitrogen |
| AOMW | M_{O_2} | lb _m /mole | | Molecular weight of oxygen |
| AREA | A_K | ft ² | | Area for thermal conduction (It is set equal to 1 for this program) |
| AREAC | | | | Value calculated in the determination of decomposable density |
| AREAV | A_v | ft ² | | Area for heat capacity. (This area multiplied by nodal thickness gives a volume. It is set equal to 1, for this program) |
| AR A | A_{dep} | meter ² /gm | DEPO | Effective surface area for the carbon deposition reaction |
| AST | | lb _f /in ² | | Aerodynamic shear force |
| ASTORE | | | COMBIN | Storage array for TEMPA1 values needed for interpolation later in the routine |

| Program Symbol | Math. Symbol | Dim. Units | Subroutine | Description |
|----------------|--------------|---------------------------------------|------------|--|
| B | B_i | BTU/sec -°R | CHARM | Coefficient of temperature (T_{i+1}^{1+1}) |
| B | λ | None | BLOCK | The power λ in the blocking function $\psi = e^{-\lambda x}$ |
| B | B_i | ft/sec | DIFUS | Coefficient of gas component concentration ($C_{I,i+1}^{1+1}$) |
| B | | | IWR | Temporary value calculated in this subroutine |
| BDUM | | | RECEED | Temporary value calculated in this subroutine |
| BF | A_{si} | °R | SIC | Activation Temperature for silica-carbon reaction |
| BLDEN | $\rho_{g,s}$ | lb _m /ft ³ | | Local density at surface |
| BLPRES | P_s | lb _f /ft ² | | Local pressure at surface |
| BMW | M_{burn} | lb _m /mole | | Molecular weight of carbon monoxide gas |
| BSTAR | | | | Blowing parameter associated with the diffusion of the ablation gases into the boundary layer |
| BSTORE | | | COMBIN | Storage array for TEMPA2 values for interpolation later in the routine |
| BURN | C_{burn} | lb _m /ft ³ void | | Concentration of carbon monoxide gas phase |
| C | C_i | BTU/sec -°R | CHARM | Coefficient of temperature (T_{i+1}^{1+1}) |
| C | C_i | | CHARM | Coefficient of densities (ρ_{i-1}^{1+1} and ρ_{i+1}^{1+1}) in density equations where nodes are "movable". |
| C | C_i | ft/sec | DIFUS | Coefficient of gas component concentration ($C_{I,i+1}^{1+1}$) |

| Program Symbol | Math. Symbol | Dim. Units | Subroutine | Description |
|----------------|--------------|--|------------|--|
| CAJA | | | SHIFT1 | Rate of change of molecular weight |
| CAR | | 1/ft | DEPO | Effective surface area per unit volume for the silica-carbon reaction |
| CARBNI | | lb _m /ft ³ | | Density of carbon in the char at time i |
| CARBNS | | lb _m /ft ³ | | Density of carbon in the char at time of i + 1 |
| CARTS | | lb _m /ft ³ | | Theoretical maximum density of carbon |
| CC | | | CHARM | The coefficient of the temperature (T_{i+1}) after reduction of the original coefficients |
| CC | | | DIFUS | The coefficient of the gas component concentration ($C_{i,i+1}$) after reduction of the original coefficient |
| CCPC | | BTU/lb _m °R (fo. first term) | | Coefficients of the cubic equation used to calculate char specific heat |
| CCFG | | BTU/lb _m °R (for first term) | | Coefficients of the cubic equation used to calculate gas specific heat |
| CFIX | $C_{s,i}$ | lb _m /ft ³ | DIFUS | Surface concentration of gas component i |
| CFXCM | $C_{s,CO}$ | lb _m /ft ³ | | Surface concentration of carbon monoxide |
| CFXDP | $C_{s,dep}$ | lb _m /ft ³ | | Surface concentration of "deposition gas" (gas other than hydrogen formed in carbon deposition reaction) (Not in use) |
| CFXH | $C_{s,H}$ | lb _m /ft ³ | | Surface concentration of hydrogen |
| CFXN | $C_{s,N}$ | lb _m /ft ³ | | Surface concentration of nitrogen |

| Program Symbol | Math. Symbol | Dim. Units | Subroutine | Description |
|----------------|------------------|---|------------|--|
| CFXO | C_s, O_2 | lb_m/ft^3 | | Surface concentration of oxygen |
| CFXPY | C_s, pyr | lb_m/ft^3 | | Surface concentration of pyrolysis gas |
| CFXSI | C_s, SiO | lb_m/ft^3 | | Surface concentration of silicon monoxide |
| CHARRO | ρ_{carb} | lb_m/ft^3 | | Carbon density in the char formed by pyrolysis |
| CINE | | | SHIFT1 | Rate of change of graphite (Not in use) |
| CKC | k_c | $BTU-in/ft^2 sec^0 R$ (For first term) | | Cubic coefficients for char conductivity equation |
| COEFT | $C_{p,v}$ | $BTU-in/ft^2 sec^0 R$ (For first term) | | Cubic coefficients for virgin specific heat equation |
| COMMAM | Δt_{max} | sec. | | Maximum time step the CHARM subroutine is allowed to take |
| CONC | C_i | lb_m/ft^3 void | DIFUS | Concentration of gas component i |
| COND | K_i | $BTU/ft^2 -^0 R - sec$ | | Thermal conductance through a node |
| CONDc | K_c | $BTU/ft^2 -^0 R - sec$ | CONDf | Char thermal conductance |
| CONDf | | | | Function subroutine which calculates thermal conductance |
| CONDv | K_v | $BTU/ft^2 -^0 R - sec$ | CONDf | Virgin thermal conductance |
| CONDx | K | $BTU/ft^2 -^0 R - sec$ | | Last thermal conductance determined in a group |
| CONDxx | K | $BTU/ft^2 -^0 R - sec$ | | Last thermal conductance determined in the group prior to group under calculation |
| COND0 | K | $BTU/ft^2 -^0 R - sec$ | | Thermal conductance of node 0. This is a dummy value for use in calculations for back boundary |
| CONST | K_v | $BTU-in/ft^2 -^0 R - sec$ (For first term) | | Cubic coefficients for virgin conductivity equation |

| Program Symbol | Math. Symbol | Dim. Units | Subroutine | Description |
|----------------|----------------|-------------------------|------------|---|
| COORD | | | | Type of one-dimensional coordinate system: 1 = cartesian, 2 = cylindrical, 3 = spherical (Not in use) |
| CPBAR | $C_{p_g,i}$ | BTU/lb _m -°R | | Specific heat of gas at mode i |
| CPC | $(\rho C_p)_c$ | BTU/ft ³ -°R | PCAPF | Thermal capacity of the char |
| CPV | $(\rho C_p)_v$ | BTU/ft ³ -°R | PCAPF | Thermal capacity of the virgin |
| CRUZ | | | SHIFT1 | Rate of change of carbon monoxide source |
| CSTORE | | | COMBIN | Storage array for TEMPA5 values for interpolation later in the routine |
| CX | | | DEPO | (See description in the block data subroutine input in the INPUT-OUTPUT section of this volume) |
| D | D_i | BTU/sec -°R | CHARM | The value D_i in the temperature equation: $A_i T_{i-1}^{i+1} + B_i T_i^{i+1} + C_i T_{i+1}^{i+1} = D_i$ |
| D | D_i | ft/sec | DIFUS | The value D_i is the gas component concentration equation: $A_i C_{i-1,i-1}^{i+1} + B_i C_{i,i}^{i+1} + C_i C_{i+1,i+1}^{i+1} = D_i$ |
| DACT | | | | The net amount of methane remaining in the exiting gas |
| DCO | | | DIFUS | The diffusion parameter D for the ablating surface for gas component j |

| Program Symbol | Math. Symbol | Dim. Units | Subroutine | Description |
|----------------|--------------|------------------|------------|---|
| DCOCM | | | | |
| DCODP | | | | |
| DCOH | | | | |
| DCON | | | | |
| DCOO | | | | |
| DCOPY | | | | |
| DCOSI | | | | |
| DCU | | | DIFUS | The diffusion parameter D for the ablating surface for gas components carbon monoxide, "deposition gas" (not in use), hydrogen, nitrogen, oxygen, pyrolysis gas, and silicon monoxide, respectively |
| DD | | | CHARM | The diffusion coefficient for the ablating surface. $D_s = D\bar{\rho}H$ |
| DD | | | DIFUS | The value D after reduction (See the program symbol D for subroutine CHARM) |
| DEL | | | DIFUS | The value D after reduction (See the program symbol D for subroutine DIFUS) |
| DELA | | | | The nodal width of previous node used in calculation of deposition and silica-carbon reactions |
| DELTAX | | In. | | Temporary storage of the nodal width used in calculation of deposition and silica-carbon reactions |
| DELTX | | None | | The nodal width for all minor nodes and non-subdivided major nodes |
| DELX | ΔX | In. | | The normalized nodal width for the moving minor nodes |
| DEP | C_{dep} | lb_m/ft^3 void | | The nodal width for all major nodes |
| DEPX | | | | Concentration of "deposition gas in gas phase (Not in use) |
| DEPXX | | | | (Not in use) |
| | | | | (Not in use) |

| Program Symbol | Math. Symbol | Dim. Units | Subroutine | Description |
|----------------|---------------------------------------|------------|------------|---|
| DGAS | | | | The time rate of change of the exiting gas mass/flux |
| DIFC | | | RECEED | Cubic coefficients in the equation for calculation of the diffusion reduction parameter |
| DIFCAL | | | DIFUS | (Not in use) |
| DIFCH | ft^3/sec | | | Diffusion coefficients for hydrogen |
| DIFCO | ft^2/sec | | DIFUS | Storage locations in DIFUS subroutine for diffusion coefficients |
| DIFCOS | ft^2/sec | | DIFUS | Temporary storage of diffusion coefficient ($i = 1$) |
| DIFR | ft^2/sec | | | Diffusion coefficients for gases other than hydrogen |
| DIFREC | | | RECEED | Diffusion reduction parameter see equation (30) |
| DIS | In | | COMBIN | Distance value used for interpolation in combining front nodes |
| DISTL | In | | | Normalized distances for moving nodes |
| DMW | lb_m/mole | | | Molecular weight of the "deposition gas" (Not in use) |
| DPRINT | Sec | | MAIN | Print interval |
| DQ | $\text{BTU}/\text{lb}_m - ^0\text{R}$ | | | Rate of change of net ablation surface heating with temperature |
| DR | | | RECEED | Surface combustion rate |
| DS | | | RECEED | Surface sublimation rate |
| DSTEP | Sec | | MAIN | Storage array of max. calculation interval (An input table) |
| DSTORE | | | COMBIN | Storage array for distance values for use in Interpolation |
| DTAU | Δt | Sec | CHARM | Calculation time step |
| DTAUC | | Sec | CHARM | Maximum calculation time step determined by CHARM |

| Program Symbol | Math. Symbol | Dim. Units | Subroutine | Description |
|----------------|--------------|------------|--------------------------|---|
| DTAUS | | Sec. | CHARM | Calculation time step for previous step |
| DTAUX | | Sec. | CHARM | An average of the old and new calculation time steps |
| DTEND | | Sec | MAIN | Time until the end-of-problem time |
| DTF | | None | CHARM | Calculation time step factor used in cases where calculation time step is too large |
| DTR | | | CHARM | An array of surface temperature rate of change with time used in "damper" procedure |
| DWFDX | | | | Amount of methane formed between back surface and end node of group being calculated |
| DWFDXX | | | | DWFDX (see above) value at previous group calculation |
| DX | Δx | | COMBIN FONEV WRITE | { It is used separately in each of the subroutines COMBIN, FONEV, and WRITE for (distance) |
| EDFLUX | | | | Heat source to node i (Not in use) |
| EDFX | | | | (Not in use) |
| EDFXX | | | | (Not in use) |
| EF | | | CHARM | The normalized distance at time j multiplied by 2 |
| EFCOLC | B_c | 1/sec | | Collision frequency for the surface char combustion reaction |
| EFCOLS | B_s | 1/sec | | Collision frequency for the surface carbon sublimation process |
| EFCOLV | B_v | 1/sec | | Collision frequency for virgin plastic decomposition reaction |
| EK | | | | Factor used in interpolations of carbon and silica densities to account for moving nodal interfaces |

| Program Symbol | Math. Symbol | Dim. Units | Subroutine | Description |
|----------------|--------------|----------------------------------|------------|---|
| EMBM | | | | Value calculated for the determination of decomposable density |
| EMI | | | | Factor for shift correction of movable nodes |
| EMIS | e_v | None | | Emissivity of virgin material |
| EMISC | e_c | None | | Emissivity of char |
| EMWT | | lb _m /mole | | Average molecular weight of the total internal gas |
| EROC | | | | Constants in the surface shear removal correlation |
| ERODE | | lb _m /sec | | The mass eroded by aerodynamic shear removal |
| ETA | | | | Fixed error criterion for calculated temperature |
| ETAS | | | | The minimum of ETA (see above) and a second error criterion: 40/T |
| F | | lb _f /in ² | | Aerodynamic shear stress at the surface |
| FCT | | | ITER8 | Argument of an external function |
| FF | | | | Storage array for flow condition indication (laminar or turbulent) (An input table) |
| FHT | | | | Nodal heat input from the virgin decomposition reaction |
| FHTX | | | | The last FHT (see above) determined in a group |
| FHTXX | | | | The last FHT (see 2 items above) determined in the group prior to group under consideration |
| FIYE | | | SHIFT1 | Value used for interpolation |
| FLOW | | | | Turbulent or laminar flow indication (1 for laminar and 2 for turbulent) |

| Program Symbol | Math. Symbol | Dim. Units | Subroutine | Description |
|----------------|------------------|--|------------|---|
| FMFP | | | DEPO | Factor used in determination of partial pressures |
| FNRDIV | | | WRITE | Floating point equivalent of NRDIV |
| FONEV | | | | Function subroutine which performs a table lookup using linear interpolation |
| FOUR | | | SHIFT1 | Rate of change of decomposable density for time ($j + 1$) with respect to distance |
| GABY | | | SHIFT1 | Rate of change of pyrolysis gas source |
| GAGC | | | | Interim value found in the calculation of coefficient matrix elements for temperature determination |
| GAS | \dot{m} g,s | | | The ablation gas mass flux at the surface at time $j + 1/2$ |
| GAS1 | \dot{m} g,s | | | The ablation gas mass flux at the surface at time $j - 1/2$ |
| GCON | R | ft-lb _f /lb mole $^{\circ}$ R | | Gas constant which equals 1545 for these dimensional units |
| GK | | | | Interim value determined in finding matrix element for ablation surface node temperature equation |
| GRAF1 | | | | Graphite density at time j (Not in use) |
| GRAF5 | | | | Graphite density at time $j + 1$ (Not in use) |
| GX | | | | Interim value determined in finding ablation surface temperature |
| GY | | | | Interim value determined in finding the ablation surface temperature |

| Program Symbol | Math. Symbol | Dim. Units | Subroutine | Description |
|----------------|----------------|---------------------------------------|------------|--|
| GZ | | | | One-half the rate of change of the ablation surface heat flux with temperature |
| HCOM | $H_{c,c}$ | BTU/lb _m | | Heat of combustion of the ablation surface |
| HCOMG | $H_{g,c}$ | BTU/lb _m | | Heat of combustion of the gas phase at surface |
| HCONV | H | lb _m /ft ² -sec | | Heat transfer parameter at the surface |
| HDA | | | | Coefficients of the quartic equation for determining the heat of reaction for the decomposition reaction |
| HECT | | | SHIFT1 | Rate of change of carbon deposition source |
| HERE | | | DEPO | Interim value in determination of carbon deposition rate |
| HMW | M _H | | | Molecular weight of hydrogen |
| HOFM | | BTU/lb _m | | Heat of virgin decomposition reaction at 536.67°K (25°C) |
| HOLD | | | | Temporary storage location |
| HOW | | | | Temporary storage location |
| HSUB | | BTU/lb _m | | Heat of carbon sublimation |
| HYD | | lb _m /ft ³ void | | Concentration of hydrogen in the gas phase |
| HYDC | | atm | DEPO | Partial pressure of hydrogen |
| I | | | | Subscript for general use, but particularly for material type |
| IBE | | | | Array of the ending interfaces of the groups |
| IBS | | | | Array of the starting interfaces of the groups |
| IBSRM | | | | [Starting location in decomposable density storage arrays for upper half-node values] - 1 |
| IBSPN | | | | [IBSPM - 1] |

| Program Symbol | Subroutine | Description |
|----------------|------------|--|
| ICOM | FRONT | An indicator which determines the direction through the latter part of the subroutine |
| IERR | | Error indicator in comparison of predicted and calculated temperatures. (1 = no error, 2 = error) |
| IERROR | | Error indicator for major program errors resulting in problem being ended |
| IG | | Group number |
| IGC | | Used for certain group numbers |
| IGL | | IG - 1 |
| IGLD | CHARM | Group indicator used in calculation control section |
| IGR | | First reaction group number |
| IGRL | | Last reaction group number. (Used otherwise also) |
| IGT | | Used for certain group numbers |
| IGTYP | | The group type (0 for no zone, 1 for zone 1, 2 for zone 2) |
| IGX | | Used for certain group numbers |
| IG2 | | Lowest group number of problem type 2 |
| IHDN | | An array of the numbers of minor nodes per major node for each group type |
| IHYS | | (Not in use) |
| INCOM | SHIFT1 | Shift value |
| INEG | | IX - 1 |
| INFRST | MAIN | Indicator of the table point number (1 - first, 2 - other than first) |
| IN1 | | Major nodal interface number for decomposition reaction zone start |
| IN2 | | Major nodal interface number for decomposition reaction zone end |

| Program Symbol | Subroutine | Description |
|--|--------------------|--|
| IP | | Problem number |
| IPLUS | | IX + 1 |
| ISAVE1 ISAVE2 ISAVE3 ISAVE4 ISAVE5 ISAVE6 | | Table entry positions saved after table lookup by FONEV subroutine |
| ISPY | WRITE | Indicator of direction through routine (1 - first pass, 2 - second pass) |
| ITER | | Number of iterations for the time step |
| ITERT | | Total number of iterations |
| IJ | SHIFT1, SHIFT2, | Number of groups in the zone |
| IYS | | Major nodal interface at start of moving nodes |
| IZB | | Array of starting storage locations for the zones |
| IZG | | Array of group numbers for each zone |
| IZGT | | Total number of groups in a zone |
| JBE | | Ending interface for a group |
| JBEM | | JBE - 1 |
| JBND1 | | Starting boundary type |
| JBND2 | | Ending boundary type |
| JBS | | Starting interface for a group |
| JBSPM | | JBS - 1 |
| JBSPN | | IBSPN + JCSN |
| JBSPN | | JBSPN - 1 |
| JBX | | Last minor node number for the group |

| Program Symbol | Subroutine | Description |
|----------------|------------|---|
| JBXX | | Last minor node number for the previous group |
| JCEN | | The major nodal interface for the end of a group |
| JCENM | | JCEN - 1 |
| JCSN | | The major nodal interface for the start of a group |
| JCSNM | | JCSN - 1 |
| JE | | JE1 + 1 |
| JE1 | | The number of minor nodes in a group |
| JE2 | | JE1 - 1 |
| JHDN | | The number of minor nodes per major node for the group |
| JHDN | COMBIN | The number of minor nodes per major node for the front group |
| JHDN | SHIFT1 | The number of minor nodes per major node for the zone |
| JLSW | | Indicator for whether group has moving nodes or not (1 - not moving, 2 - moving) |
| JRSW | | Indicator for whether group is in decomposition reaction zone or not (1 - before zone, 2 - after zone, 3 - in zone) |
| JSLAB | | Number of major nodes in a group |
| JSUB | WRITE | Storage location of decomposable density for upper half node at ablation surface |
| KHDN | COMBIN | The number of minor nodes per major node for the new combined node |
| KHDN | SHIFT1 | The number of minor nodes per major node |
| KK | | Commonly used for the storage location of the decomposable density for the upper half node |

| Program Symbol | Dim. Units | Subroutine | Description |
|----------------|------------|------------|--|
| KK | | DIFUS | Major node number below major node KL |
| KL | | | Commonly used for relative storage location of the minor nodes |
| KL | | DIFUS | Major node number |
| KSUBI | | FONEV | One of the table points for use in the linear interpolation |
| KSUBJ | | FONEV | The other table point for use in the linear interpolation |
| K1 | | | K + 1 |
| L | | | Always equal to 1 in CHAD |
| LANDID | | | An indicator in the Calculation Control section of CHARM |
| LFT | | | Left (toward back) indicator for side of zone to be added to or subtracted from |
| LLD | | | Function subroutine which determines major node corresponding to a minor node |
| LRT | | | Right (toward ablation surface) indicator for the side of zone to be added to or subtracted from |
| MARK | | | Indicator of whether or not to enter calculation control (1 - No, 2 - Yes) |
| MARY | | SHIFT1 | Rate of change of silicon monoxide source with respect to distance |
| MAT | | | An array of material numbers which indicate material type for each major node |
| MCXT | | DEPO | Rate factor for the carbon deposition reaction |
| METC | atm | DEPO | Partial pressure of methane |

| Program Symbol | Subroutine | Description |
|----------------|------------|---|
| MG | | The total number of groups |
| MNOD | | The front major nodal interface number |
| N | | Always equal to 1 in CHAD |
| N | ITER8 | |
| NADD | | An array for a group of the number of major nodes of the same material and width in the group |
| NASW | | The type of boundary at the ablation surface |
| NBNDST | | Used in calculation control section of CHARM |
| NBND1 | | An array of starting boundary types for the groups |
| NBND2 | | An array of the ending boundary types for the groups |
| NBSW | | The type of boundary at the back surface |
| NCEN | | An array of the ending major interface numbers for the groups |
| NCSN | | An array of the starting major interface numbers for the groups |
| NCVT | | An indicator used by FRONT subroutine (See FRONT flow sheet) |
| ND | | Node divider array. ND(1) is used to indicate position between moving and non-moving nodes |
| NDOTS | | An array of the number of points in the input tables |
| NDOTSX | MAIN | A subscript limit used in table output section |
| NHDN | | An array of the number of minor nodes per major node for each zone |
| NLR | SHIFT1 | Left-right switch. (See LFT and LRT) |

| Program Symbol | Subroutine | Description |
|----------------|------------|---|
| NLSW | | An array of the indicators for each group of whether the nodes are moving or not-moving |
| NLZON | | The largest zone number |
| NN | | The maximum major node number |
| NNP | | The maximum major nodal interface number. Equals NN + 1 |
| NOF | | The ablation surface interface number (minor node basis) |
| NONE | SHIFT1 | The shift value |
| NOTIME | | Total number of time steps |
| NPBSW | | Switch based on problem type and is used in the calculation control section of CHARM |
| NPE1N | | Major nodal interface for the ending of problem 1 |
| NPS2N | | Major nodal interface for the start of problem 2 |
| NPTSW | | Switch for returning from CHARM back to MAIN (1 - Stay, 2 - Return) |
| NRDIV | | The number of minor nodes per major node |
| NREND | | The ending major interface of the zone |
| NRGO | | The starting major interface of the zone |
| NRID | | Indicator used in calculation control section in CHARM |
| NRSW | | An array of the indicators for each group of where or not the group is in the decomposition reaction zone |
| NRZON | | The zone number for the reaction zone |
| NSHL | | An array of the shift values to the left for each zone |

O

| Program Symbol | Dim. Units | Subroutine | Description |
|----------------|--|------------|---|
| NZSN | | | An array used for the major nodal interfaces of the start of zones |
| OMG | | RECEED | Interim value used in calculating diffusion reduction parameter |
| ONE | | | Temporary storage location |
| P | | SUBZ | Local pressure at the surface |
| PARTIN | | | Same as DELTA X |
| PC | BTU/sec | | Thermal capacity divided by time step |
| PCAPF | BTU/sec | | Function subroutine which calculates thermal capacity |
| PCX | | | Last PC calculated in a group |
| PCXX | | | Last PC determined in just prior group |
| PERM1 | $\text{lb}_m \text{ft}^3/\text{lb}_f \text{sec}^2$ | | Viscous permeability multiplied by gc |
| PERM2 | $\text{lb}_m \text{ft}^2/\text{lb}_f \text{sec}^2$ | | Inertial permeability multiplied by gc |
| PERT1 | ft^2 | | Reference viscous permeability for viscous permeability calculation |
| PERT2 | ft | | Reference inertial permeability for inertial permeability calculation |
| PHI | None | | Blocking parameter |
| PMW | $\text{lb}_m/\text{lb mole}$ | | Molecular weight of pyrolysis gas |
| POR | None | | Porosity |
| PORT | | | Reference porosity for porosity calculation |
| PP | | | Storage array for local surface pressure (An input table) |
| PRFRNT | | FLOWS | Local surface pressure |
| PRG | | | Internal gas pressure |
| PSI | | | Parameter calculated for use in aerodynamic shear erosion determination |

| Program Symbol | Subroutine | Description |
|----------------|------------|---|
| NSHR | | An array of the shift values to the right for each zone |
| NSLAB | | An array of the number of major nodes in each group |
| NSLABH | | An array of the number of minor nodes in each group |
| NSOUR | DIFUS | Switch in DIFUS set in CHARM according to the gas component being determined |
| NST | CHARM | Switch used in CHARM which is set to 1 for first pass into CHARM and to 2 thereafter |
| NSTILL | CHARM | Switch which is set to 1 for decomposition reaction and 0 for decomposition reaction occurring within the group |
| NSW | CHARM | Switch in calculation control section of CHARM |
| NTAB | MAIN | Table number |
| NTABT | MAIN | The total of tables what have been input |
| NTYP | MAIN | The type of table 3 temperature or heat flux |
| NXSW | CHARM | Switch in iteration control section which allows recalculation of front group of error found there on first iteration |
| NZEN | | An array of the ending major nodal interfaces for the zones |
| NZON | | Subscript used for zone numbers |
| NZONC | | Initializing value for calculation control section. It equals 1 normally and 2 when there is no decomposition reaction zone |
| NZONX | SHIFT1 | Zone type for group adjacent to zone being changed |

| Program Symbol | Dim. Units | Subroutine | Description |
|----------------|------------------------------------|------------|---|
| PSQ | | FLOWS | The square of the internal gas pressure |
| PSTORE | | COMBIN | Storage array for SILCA1 values needed for interpolation later in the routine |
| PSTEP | | | Storage array for print intervals (An input table) |
| PYRO | lb _m ³ /void | | Concentration of methane in the gas phase |
| QBACK | BTU/ft ² -sec | | Heat flux to the back surface (Not in use) |
| QBRN | BTU/lb _m | | Heat of reaction for internal combustion (Not in use) |
| QBYRAD | BTU/ft ² -sec | | Heat radiated from the ablation surface |
| QCOMB | BTU/lb _m | | Heat of surface combustion |
| QCOND | BTU/ft ² -sec | | Conducted heat flux |
| QCONV | | | Unblocked convective heat flux to the ablation surface |
| QDEP | BTU/lb _m | | Heat of reaction for carbon deposition |
| QGAS | BTU/ft ² -sec | | Heat radiated by hot gas toward ablation surface |
| QGPCOM | BTU/ft ² -sec | | Heat flux of gas phase combustion to ablation surface |
| QMISC | BTU/ft ² -sec | | Heat to ablation surface that is not blocked |
| QMU | BTU/ft ² -sec | | Storage array for unblocked heat flux (An input table) |
| QSAVE | BTU/ft ² -sec | | Total heat flux to ablation surface |
| QSI | BTU/lb _m | | Heat of reaction for silica-carbon reaction |
| QSTORE | | COMBIN | Storage array for CARBN1 values needed for interpolation later in the routine |
| QSUBL | BTU/lb _m | | Heat of sublimation |

| Program Symbol | Math. Symbol | Dim. Units | Subroutine | Description |
|----------------|----------------------------------|----------------------------------|------------|---|
| QTOT | | BTU/ft ² -sec | | Partial total of heat fluxes to the ablation surface |
| QTOTAL | | BTU/ft ² -sec | | Total heat flux to the ablation surface |
| RATE | | | | Virgin material decomposition rate |
| REO | n | None | | Reaction order of the silica-carbon reaction |
| REORDC | | None | | Reaction order of the surface combustion reaction |
| REORDS | | None | | Reaction order of the surface sublimation |
| REORDV | | None | | Reaction order of the virgin decomposition reaction |
| REQ | | None | | Same as REO |
| RH | | | | Storage array for heat transfer parameters (An input table) |
| RHO | | lb _m /ft ³ | WRITE | Density value for print-out |
| RHOC | ρ_c | lb _m /ft ³ | | Char density after pyrolysis and before char deposition or silica-carbon reaction |
| RHODE | ρ_d | lb _m /ft ³ | WRITE | Density of decomposable material |
| RHOTS | | | | Theoretical maximum density of virgin material |
| RHOV | ρ_v | lb _m /ft ³ | | Density of the virgin material |
| RHO1 | $(\rho_d)_i$ | lb _m /ft ³ | | Density of decomposable material at time i |
| RHO2 | $(\rho_d)_i^{i+1}$ (est) | lb _m /ft ³ | | Estimated density of decomposable material at time i + 1 |
| RHO3 | $(\rho_d)_i^{i+1/2}$ (est) | lb _m /ft ³ | | Estimated density of decomposable material at time of i + 1/2 |
| RHO4 | $(\rho_d)_{i+1/2}^{i+1/2}$ (est) | lb _m /ft ³ | | Average of RHO3 for two adjacent half-nodes |

| Program Symbol | Math. Symbol | Dim. Units | Subroutine | Description |
|----------------|---------------------------|---------------------------------------|------------|---|
| RHO5 | $(\rho_a)_i^{j+1}$ (calc) | lb _m /ft ³ | | Calculated density of decomposable material at time $j+1$ |
| RSTORE | | | COMBIN | Storage array for RHO1 values needed for interpolation later in the routine |
| SAVE | | | | Temporary storage |
| SCHECK | | In | | Front nodal thickness at which the front node is combined with the next one if materials are the same |
| SDN | | In | | Amount of surface recession for half a time step |
| SDOTN | | in/sec | | Surface recession rate at time $j + 1/2$ |
| SET | | | MAIN | Minimum COMMAX allowed |
| SILICA1 | $(\rho_{SiO_2})_i^j$ | lb _m /ft ³ | | Density of silica in the char at time j |
| SILICA5 | $(\rho_{SiO_2})_i^{j+1}$ | lb _m /ft ³ | | Density of silica in the char at time $j+1$ |
| SILICA | | lb _m /ft ³ | | Initial density of silica before the silica-carbon reaction begins |
| SILTS | | lb _m /ft ³ | | Theoretical maximum density of silica |
| SLOPE | | | | Transpiration factor for ablation gases |
| SMW | M _{SiO} | lb _m /lb mole | | Molecular weight of silicon monoxide |
| SN | | In | | Thickness of movable nodes at time $j + 1/2$ |
| SN1 | | In | | Thickness of movable nodes at time j |
| SOURCE | | lb _m /sec | DIFUS | Source of gas component i |
| SOX | | lb _m /ft ³ void | | Concentration of oxygen in the gas phase |
| SPEED | | ft/sec | | Velocity of the gas internally |

| Program Symbol | Math. Symbol | Dim. Units | Subroutine | Description |
|----------------|-----------------------|-------------|------------|---|
| TAR | | | | Area of back surface (Not in use) |
| TAUOUT | | | | Time for return from CHARM to the MAIN routine |
| TAUST | | | | An array of times corresponding to TEMPST and DTR for use in "damper" procedure |
| TAU1 | | | | Time j start of the time step |
| TAU2 | | | | Time $j + 1$ the end of the time step |
| TAU2S | | | | Time $j + 1$ for the previous iteration |
| TBSTEP | | | | Function subroutine which does a table lookup on a step function |
| TEMPA | | | | Temperature for use in an im- pending calculation |
| TEMPA1 | T_i^j | $^{\circ}R$ | | Temperature at a nodal inter- face at time j |
| TEMPA2 | $(T_i^{j+1})_{est}$ | $^{\circ}R$ | | Estimated temperature at a nodal interface at time $j + 1$ |
| TEMPA3 | $(T_i^{j+1/2})_{est}$ | $^{\circ}R$ | | Estimated temperature at a nodal interface at time $j + 1/2$ |
| TEMPA4 | $(T_i^{j+1/2})_{est}$ | $^{\circ}R$ | | Average of TEMP A3 for two adjacent nodal interfaces |
| TEMPA5 | $(T_i^{j+1})_{calc.}$ | $^{\circ}R$ | | Calculated temperature at a nodal interface at time $j + 1$ |
| TEMPST | | | | An array of temperatures corre- sponding to TAUST for use in "damper" procedure |
| TEND | | | MAIN | End compute time |
| TEST | | | DEPO | A limit imposed on carbon deposition based on amount of methane produced |
| TIENDA | | | SHIFT1 | Rate of change of internal gas mass flux |
| TIME | Sec | | MAIN | Same as TAU1 |

| Program Symbol | Math. Symbol | Dim. Units | Subroutine | Description |
|----------------|--------------|--------------------|------------|---|
| TIME1 | | | | |
| TIME2 | | Sec. | | Time arrays for the input tables |
| TIME3 | | | | |
| TIME4 | | | | |
| TPRINT | τ | Sec | | Time for output of calculated data |
| TRCHAR | ζ | None | | Transpiration factor for gases resulting from surface combustion and surface sublimation |
| TS | T_i | $^{\circ}R$ | | Same as TEMP1 |
| TT | | | | Storage array for ablation surface temperature (An input table) |
| TWALL | | | | Ablation surface temperature |
| UHOLD | | | COMBIN | Storage array for WFD values needed for interpolation later in the routine |
| USTORE | | | COMBIN | Storage array for EMWT values needed for interpolation later in the routine |
| VHOLD | | | COMBIN | Storage array for carbon deposition sources needed for interpolation later in the routine |
| VISC | μ | $lb_m/ft\cdot sec$ | | Viscosity of the internal gas |
| VISCO | μ^* | $lb_m/ft\cdot sec$ | | Reference viscosity for viscosity calculation |
| VISCON | T^* | $^{\circ}R$ | | Temperature corresponding to the reference viscosity |
| VSTORE | | | COMBIN | Storage array for internal gas mass flux needed for interpolation later in the routine |
| WBRN | | lb_m/sec | | Source of carbon monoxide |
| WBRNX | | lb_m/sec | | The last WBRN value determined in the group |
| WBRNXX | | lb_m/sec | | The last WBRN value determined in the group prior to the group under consideration |

| Program Symbol | Dim. Units | Subroutine | Description |
|----------------|--------------------------------------|------------|---|
| WDEP | lb _m /sec | | Source of deposited carbon |
| WDEPX | lb _m /sec | | WDEP value determined in the group prior to the group under consideration |
| WDEP | lb _m /sec | | Source of deposited carbon |
| WDEPX | lb _m /sec | | The last WDEP value determined in a group |
| WDEPXX | lb _m /sec | | The last WDEP value determined in the group prior to the group under consideration |
| WF | lb _m /ft ² sec | | Internal gas mass flux |
| WFD | | | Source of pyrolysis gas |
| WFDX | | | Last WFD value determined in the group |
| WFDXX | | | Last WFD value determined in the group prior to the last group under consideration |
| WFP | | | Interim value in the calculation of WF |
| WFX | | | Last WF value determined in a group |
| WFXX | | | Last WF value determined in a group prior to the last group under consideration |
| WHOLD | | COMBIN | Storage array for silicon monoxide source needed for interpolation later in the routine |
| WSI | | | Silicon monoxide source |
| WSIO2 | | SIC | |
| WSIX | | | The last WSI value determined in the group |
| WSIXX | | | The last WSI value determined in the group prior to the group under consideration |
| WSTORE | | COMBIN | Storage array for GRAF1 values needed for interpolation later in the routine |

| Program Symbol | Math. Symbol | Dim. Units | Subroutine | Description |
|----------------|--------------|----------------------|------------|--|
| XHOLD | | | COMBIN | Storage array for WBRN values needed for interpolation later in the routine |
| XIR | I_r | BTU/lb _m | | Recovery enthalpy |
| XIWALL | I_w | | | Enthalpy at the wall |
| XLEFT | | In | | Distance to major nodal interfaces from the back surface |
| XMDOTC | | lb _m /sec | | Mass recession at the ablation surface from combustion and sublimation |
| XMDOTD | | lb _m /sec | | Diffusion-limited surface combustion rate |
| XMDOTG | | | | Same as GAS |
| XMDOTL | | lb _m /sec | | Surface combustion rate |
| XMDOTR | | lb _m /sec | | Reaction rate limited surface combustion rate |
| XMDOTS | | lb _m /sec | | Surface sublimation rate |
| XRI | | | | Storage array for recovery enthalpies (An input table) |
| XSAVE | | | | Test value for determining whether to end the problem or not because of complete loss of ablating material |
| ZWALL | z | None | | Compressibility factor at the ablation surface |

SAMPLE CASES

The two sample cases presented have used the same basic data. The first case (I) is a temperature drive input and the second case (II) is a heat flux drive input. The calculated data output at a limited number of time points is shown for each case.

SAMPLE CASE I

Temperature drive - DATA INPUT CARDS

- XOT MAIN
TEMPERATURE DRIVE SAMPLE CASE

| | |
|-------|-----|
| 1 | |
| 0. | 1.0 |
| 40. | 0.2 |
| 100. | 1.0 |
| 600. | 2.0 |
| 1078. | 2.0 |
| 0. | 0. |
| 2 | |

TIME STEP CONTROL TABLE

| | | |
|-------|-------|--------|
| 0. | 10. | |
| 100. | 20. | |
| 600. | 100. | |
| 1078. | 100. | |
| 0. | 0. | |
| 3 | 2 | |
| 0. | 560. | .00004 |
| 20. | 1708. | .00010 |
| 40. | 1849. | .00061 |
| 60. | 3262. | .00391 |
| 80. | 5625. | .01086 |
| 100. | 4911. | .01341 |
| 120. | 4193. | .00932 |
| 140. | 3905. | .00786 |
| 160. | 3655. | .00660 |
| 180. | 3374. | .00503 |
| 200. | 3145. | .00395 |
| 220. | 2994. | .00335 |
| 240. | 2924. | .00308 |
| 260. | 2881. | .00295 |
| 280. | 2842. | .00282 |
| 300. | 2802. | .00268 |
| 320. | 2831. | .00285 |
| 340. | 2866. | .00302 |
| 360. | 2904. | .00326 |
| 380. | 2997. | .00381 |
| 400. | 3142. | .00475 |
| 420. | 3293. | .00607 |
| 440. | 3401. | .00755 |
| 460. | 3194. | .00865 |
| 480. | 3009. | .00930 |
| 500. | 2708. | .00861 |
| 540. | 2113. | .00685 |
| 600. | 1628. | .00650 |
| 700. | 990. | .01030 |
| 800. | 703. | .01360 |
| 900. | 641. | .01460 |
| 1000. | 612. | .01550 |
| 1078. | 599. | .01603 |
| 0. | 0. | |

PRINT STEP CONTROL TABLE

| | | |
|-----|-------|-------------|
| 4 | | |
| 0. | .0360 | 1. .0000403 |
| 40. | 1.756 | 1. .000639 |
| 50. | 10.5 | 1. .001944 |
| 60. | 66.08 | 1. .004779 |

LOCAL STATIC PRESSURE AND FLOW

| | | | |
|------------|--------|-------|---------|
| 70. | 393.0 | 1. | .008396 |
| 80. | 512.8 | 1. | .012207 |
| 85. | 767.0 | 1. | .01308 |
| 90. | 1030.0 | 1. | .013202 |
| 95. | 920.0 | 1. | .012724 |
| 100. | 818.1 | 1. | .012542 |
| 105. | 755.0 | 1. | .011384 |
| 110. | 651.0 | 1. | .009522 |
| 115. | 549.0 | 1. | .008698 |
| 120. | 410.9 | 1. | .007690 |
| 130. | 349.0 | 1. | .006707 |
| 140. | 298.0 | 1. | .006108 |
| 150. | 258.0 | 1. | .005552 |
| 160. | 213.4 | 1. | .004909 |
| 170. | 156.0 | 1. | .004192 |
| 180. | 125.1 | 1. | .003612 |
| 190. | 96.9 | 1. | .003218 |
| 200. | 77.7 | 1. | .00277 |
| 210. | 66.2 | 1. | .002416 |
| 240. | 47.5 | 1. | .002095 |
| 300. | 36.3 | 1. | .001795 |
| 350. | 49.8 | 1. | .002051 |
| 370. | 61.5 | 1. | .002261 |
| 390. | 90.6 | 1. | .002634 |
| 410. | 147.0 | 1. | .003475 |
| 430. | 236.0 | 1. | .004399 |
| 450. | 366. | 1. | .005078 |
| 470. | 459. | 1. | .005091 |
| 480. | 496. | 1. | .004893 |
| 490. | 480. | 1. | .004296 |
| 510. | 411. | 1. | .003504 |
| 530. | 318. | 1. | .002628 |
| 550. | 287. | 1. | .002214 |
| 570. | 307. | 1. | .001667 |
| 706. | 734. | 1. | .00118 |
| 756. | 1115. | 1. | .001561 |
| 1078. | 2117. | 1. | .001972 |
| 0. | 0. | | |
| 2 ALUMINUM | | .015 | 1 |
| 1 AVCOAT | | 1.976 | 35 |
| 0 | | | |

560.

SAMPLE CASE I

Temperature drive - OUTPUT OF INITIAL INPUT TABLES

TITLE---- TEMPERATURE DRIVE SAMPLE CASE

CALCULATION TIME STEP CONTROL TABLE

| TIME (SEC) | TIME STEP (SEC) |
|---------------|--------------------|
| 0.00 | 1.000 |
| 40.00 | .200 |
| 100.00 | 1.000 |
| 600.00 | 2.000 |
| 1078.00 | 2.0000 |

POINT TIME STEP CONTROL TABLE

| TIME (SEC) | TIME STEP (SEC) |
|---------------|--------------------|
| 0.00 | 10.000 |
| 100.00 | 20.000 |
| 600.00 | 100.000 |
| 1078.00 | 100.000 |

SURFACE TEMPERATURE TABLE

| TIME (SEC) | TEMPERATURE (DEG R) | HEAT TRANSFER PARAMETER (LBH/FT ² -SEC) |
|---------------|------------------------|--|
| 0.00 | 560.00 | 0.0004 |
| 20.00 | 1708.00 | 0.00030 |
| 40.00 | 1849.00 | 0.0001 |
| 60.00 | 3262.00 | 0.00361 |
| 80.00 | 5625.00 | 0.01084 |
| 100.00 | 9911.00 | 0.01341 |
| 120.00 | 4193.00 | 0.00932 |
| 140.00 | 3905.00 | 0.00784 |
| 160.00 | 3655.00 | 0.00640 |
| 180.00 | 3374.00 | 0.00503 |
| 200.00 | 3145.00 | 0.00395 |
| 220.00 | 2994.00 | 0.00335 |
| 240.00 | 2924.00 | 0.00308 |
| 260.00 | 2861.00 | 0.00295 |
| 280.00 | 2842.00 | 0.00282 |
| 300.00 | 2802.00 | 0.00268 |
| 320.00 | 2831.00 | 0.00265 |
| 340.00 | 2866.00 | 0.00302 |
| 360.00 | 2904.00 | 0.00324 |
| 380.00 | 2997.00 | 0.00381 |
| 400.00 | 3142.00 | 0.00475 |
| 420.00 | 3293.00 | 0.00607 |
| 440.00 | 3401.00 | 0.00755 |
| 460.00 | 3194.00 | 0.00655 |
| 480.00 | 3009.00 | 0.00939 |
| 500.00 | 2708.00 | 0.0081 |
| 520.00 | 2113.00 | 0.00685 |
| 540.00 | 1628.00 | 0.00650 |
| 560.00 | 990.00 | 0.01030 |
| 580.00 | 703.00 | 0.01360 |
| 600.00 | 641.00 | 0.01460 |
| 620.00 | 512.00 | 0.01550 |
| 640.00 | 599.00 | 0.01603 |

| LOCAL STATIC PRESSURE AND FLOW CONTROL TABLE | | | |
|--|-------------------------------------|---------------|--|
| TIME (SEC) | LOC. PRESS (LB/FT ²) | FLOW (sec) | LOCAL STRESS (LBF/IN ²) |
| 0.00 | *0.0360 | 1.0 | *0.000 |
| 40.00 | 1.7560 | 1.0 | *0.006 |
| 50.00 | 10.5000 | 1.0 | *0.019 |
| 60.00 | 66.0800 | 1.0 | *0.048 |
| 70.00 | 293.0000 | 1.0 | *0.084 |
| 80.00 | 512.8000 | 1.0 | *0.122 |
| 85.00 | 767.0000 | 1.0 | *0.131 |
| 90.00 | 1030.0000 | 1.0 | *0.132 |
| 95.00 | 1202.0000 | 1.0 | *0.127 |
| 100.00 | 1316.0000 | 1.0 | *0.125 |
| 105.00 | 1552.0000 | 1.0 | *0.114 |
| 110.00 | 1811.0000 | 1.0 | *0.095 |
| 115.00 | 2099.0000 | 1.0 | *0.087 |
| 120.00 | 2406.0000 | 1.0 | *0.077 |
| 130.00 | 3494.0000 | 1.0 | *0.067 |
| 140.00 | 2964.0000 | 1.0 | *0.061 |
| 150.00 | 258.0000 | 1.0 | *0.054 |
| 160.00 | 213.4000 | 1.0 | *0.049 |
| 170.00 | 156.0000 | 1.0 | *0.042 |
| 180.00 | 125.1000 | 1.0 | *0.034 |
| 190.00 | 96.9000 | 1.0 | *0.032 |
| 200.00 | 77.7000 | 1.0 | *0.028 |
| 210.00 | 66.2000 | 1.0 | *0.024 |
| 240.00 | 47.5000 | 1.0 | *0.021 |
| 300.00 | 36.3000 | 1.0 | *0.016 |
| 350.00 | 49.8000 | 1.0 | *0.021 |
| 370.00 | 41.5000 | 1.0 | *0.023 |
| 390.00 | 30.4000 | 1.0 | *0.028 |
| 410.00 | 147.0000 | 1.0 | *0.035 |
| 430.00 | 236.0000 | 1.0 | *0.044 |
| 450.00 | 364.0000 | 1.0 | *0.051 |
| 470.00 | 459.0000 | 1.0 | *0.051 |
| 480.00 | 496.0000 | 1.0 | *0.054 |
| 490.00 | 497.0000 | 1.0 | *0.043 |
| 510.00 | 431.0000 | 1.0 | *0.035 |
| 530.00 | 318.0000 | 1.0 | *0.026 |
| 550.00 | 287.0000 | 1.0 | *0.022 |
| 570.00 | 307.0000 | 1.0 | *0.017 |
| 704.00 | 234.0000 | 1.0 | *0.012 |
| 754.00 | 1114.9999 | 1.0 | *0.016 |
| 1078.00 | 2117.0000 | 1.0 | *0.020 |

MATERIALS

| MATERIAL NAME | THICKNESS (IN) | NUMBER OF NODES |
|---------------|-------------------|--------------------|
| (2) ALUMINUM | .0150 | 1 |
| (1) AVOCA | 1.9760 | 35 |

MATERIAL PROPERTIES OF VIRGIN MATERIALS

MATERIAL (1)

| | FIRST REAC | SECOND REAC |
|-----------------------------------|--------------|--------------|
| ACTIVATION TEMPERATURE,DEG R | 23000.0 | 0 |
| COLLISION FREQUENCY,1/SEC | 112090.05 | 0 |
| REACTION ORDER | 1.0000 | 0.0000 |
| HEAT OF DECOMPOSITION,BTU/LBM | 350.00 | |
| SPECIFIC HEAT,BTU/LBM-DEG R | •4100-0011•1 | •9936-0117•1 |
| CONDUCTIVITY,BTU-IN/FT2-SEC-DEG R | •2440-0511•1 | •125-0117•1 |
| EMISSIVITY | •9000 | |
| ABSORPTIVITY | •9000 | |
| DENSITY,LBM/FT3 | 34.00 | |
| TRANSPIRATION FACTOR (ABL GASES) | 1.2000 | |

MATERIAL (2)

| | FIRST REAC | SECOND REAC |
|-----------------------------------|-------------|--------------|
| ACTIVATION TEMPERATURE,DEG R | 0 | 0 |
| COLLISION FREQUENCY,1/SEC | •00000 | •00000 |
| REACTION ORDER | 0.0000 | 0.0000 |
| HEAT OF DECOMPOSITION,BTU/LBM | 120.00 | |
| SPECIFIC HEAT,BTU/LBM-DEG R | •0000 | •1442-0411•1 |
| CONDUCTIVITY,BTU-IN/FT2-SEC-DEG R | •153-0611•1 | •9610-0511•1 |
| EMISSIVITY | •2000 | |
| ABSORPTIVITY | •4000 | |
| DENSITY,LBM/FT3 | 64.00 | |
| TRANSPIRATION FACTOR (ABL GASES) | •7000 | |

MATERIAL PROPERTIES OF THE CHAR

| | COMBUSTION REACTION | CHAR SUBLIMATION |
|------------------------------|---------------------|------------------|
| ACTIVATION TEMPERATURE,DEG R | 36855.0 | 0 |
| COLLISION FREQUENCY,1/SEC | •673000.09 | •00000 |
| REACTION ORDER | •5000 | 0 |
| HEAT OF COMBUSTION,BTU/LBM | 0.00 | |
| HEAT OF SUBLIMATION,BTU/LBM | 0.00 | |
| EMISSIVITY | •4500 | |
| ABSORPTIVITY | •0000 | |
| DENSITY,LBM/FT3 | 20.00 | |

TRANSPIRATION FACTOR (CHAR GASES) 1.0000

DENSITY OF THE CARBON IN CHAR/LBM/FT³ 10.00

ABALATION GAS PROPERTIES

SPECIFIC HEAT BTU/LB-DEG R 7000.00E+1 0.0000 1701 0.0000 1700 0.0000
HEAT OF GAS COMBUSTION, BTU/LBM 6173.00

OTHER CONSTANTS

THEORETICAL CARBON DENSITY,LBM/FT³ 1.1.00
THEORETICAL VIRGIN DENSITY,LBM/FT³ 70.00
THEORETICAL SILICA DENSITY,LBM/FT³ 137.30

REFERENCE POROSITY 0.7500
REFERENCE VISCOSITY PERMEABILITY,FT² 0.00000=09
REFERENCE INERTIAL PERMEABILITY,FT² 0.00000=02

REFERENCE VISCOSITY,LBM/FT-SEC 1000.00=04
REFERENCE TEMPERATURE FOR VISC.,R 530.00

SURFACE DIFFUSION CONSTANT,FT²/SEC.

CARBON MONOXIDE 0.01730=01
DEPOSITION GAS (EXCEPT HYDROGEN) 0.0000=01
NITROGEN 0.0000=01
OXYGEN 0.0000=01
PETROLEUM 0.0000=01
SILICON MONOXIDE 0.0000=01

BLOWING PARAMETER 4300
DIFFUSION REDUCTION PARAM 1 -0.6190+01/ETA+1 -0.2540+01/ETA+1 =0.2300+01/ETA+2+1 +0.8700+00/ETA+3
HEAT OF REACTION, SiO₂-C, J/LBM .00
HEAT OF REACTION, C DEPOSITION, BTU/LBM 0
REACTION ORDER 1.0000

SILICA-CARBON REACTION CONSTANTS

ACTIVATION TEMPERATURE,DEG R 4075.0
COLLISION FREQUENCY,1/SEC 0.09210=04
REACTION ORDER 1.0000

SILICA O SITV IN INITIAL CHAR/LBM/FT³ 0.19

CARBON DEPOSITION REACTION CONSTANTS

| | LOW HYDROGEN | HIGH HYDROGEN |
|---|--------------|---------------|
| X | 0.00000=01 | 0.00000=03 |
| Y | 0.116200+03 | 0.114000+01 |
| Z | 0.177200+04 | 0.177000+01 |

SAMPLE CASE I

Temperature drive - OUTPUT OF CALCULATED DATA AT VARIOUS TIMES

The following listing shows the CHAD program output at time = 0, 100, 200, and 500 seconds.

TIME= .00 TOTAL ITERS=

| NODE | DISTANCE FROM BACK (LIN) | TEMP (DEG F) | CONDUCTED HEAT FLUX (BTU/FT ² -SEC) |
|------|--------------------------|--------------|--|
| 37 | 1.9910 | 100.31 | .0000 |
| 26 | 1.9769 | 100.31 | .0000 |
| 26 | 1.9628 | 100.31 | .0000 |
| 36 | 1.9487 | 100.31 | .0000 |
| 36 | 1.9345 | 100.31 | .0000 |
| 25 | 1.8781 | 100.31 | .0000 |
| 34 | 1.8216 | 100.31 | .0000 |
| 33 | 1.7452 | 100.31 | .0000 |
| 32 | 1.7087 | 100.31 | .0000 |
| 31 | 1.6523 | 100.31 | .0000 |
| 30 | 1.5958 | 100.31 | .0000 |
| 29 | 1.5393 | 100.31 | .0000 |
| 28 | 1.4829 | 100.31 | .0000 |
| 27 | 1.4264 | 100.31 | .0000 |
| 26 | 1.3700 | 100.31 | .0000 |
| 25 | 1.3135 | 100.31 | .0000 |
| 24 | 1.2571 | 100.31 | .0000 |
| 23 | 1.2006 | 100.31 | .0000 |
| 22 | 1.1441 | 100.31 | .0000 |
| 21 | 1.0877 | 100.31 | .0000 |
| 20 | 1.0312 | 100.31 | .0000 |
| 19 | .9748 | 100.31 | .0000 |
| 18 | .9183 | 100.31 | .0000 |
| 17 | .8614 | 100.31 | .0000 |
| 16 | .8054 | 100.31 | .0000 |
| 15 | .7489 | 100.31 | .0000 |
| 14 | .6925 | 100.31 | .0000 |
| 13 | .6360 | 100.31 | .0000 |
| 12 | .5794 | 100.31 | .0000 |
| 11 | .5231 | 100.31 | .0000 |
| 10 | .4667 | 100.31 | .0000 |
| 9 | .4102 | 100.31 | .0000 |
| 8 | .3527 | 100.31 | .0000 |
| 7 | .2973 | 100.31 | .0000 |
| 6 | .2408 | 100.31 | .0000 |
| 5 | .1844 | 100.31 | .0000 |
| 4 | .1279 | 100.31 | .0000 |
| 3 | .0715 | 100.31 | .0000 |
| 2 | .0150 | 100.31 | .0000 |
| 1 | .0000 | 100.31 | .0000 |

-----SOURCES AND SINKS-----
NODE GAS FLOW RATE (LBM/FT²-SEC) PYRO DEPO SINK (LBM/MODE-SEC)

INTERNAL PRESSURE (LBF/FT²)

MOL %

VELOCITY (FT/SEC)

TOTAL

-----DENSITIES (LBM/FT³)-----
TOTAL DECOMP CARBON GRAPHITE SILICA

10.0000

10.0000

10.0000

10.0000

10.0000

10.0000

10.0000

10.0000

10.0000

10.0000

10.0000

10.0000

10.0000

10.0000

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-----GAS FLOW-----
NODE GAS FLOW RATE (LBM/FT²-SEC) PYRO DEPO SINK (LBM/MODE-SEC)

INTERNAL PRESSURE (LBF/FT²)

MOL %

VELOCITY (FT/SEC)

TOTAL

-----CONCENTRATIONS-----
(LBM/FT³)

OXYGEN NITROGEN HYDROGEN PYRO DEPO SINK BULKY TOTAL

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TIME= 100.00 TOTAL ITERATIONS= 369

78

TOTAL ITERATIONS = 369

| NODE | DISTANCE FROM BACK (MM) | TEMP (DEG F) | CONDUCTED HEAT FLUX (BTU/FT ² /SEC) | | DECOMP TOTAL | | | DENSITIES (LBM/FT ³) | | | INTERNAL PRESSURE (LB/FT ²) | MOL AT VOID | VELOCITY (FT/SEC) |
|------|-------------------------------|-----------------|--|-----------|-----------------|---------|---------|----------------------------------|---------|----------|---|----------------|----------------------|
| | | | TEMP | HEAT FLUX | CARBON | DECOMP | SILICA | GRAPHITE | SILICA | GRAPHITE | | | |
| 37 | 1.9653 | 4951.31 | - | 0.0000 | 13.9551 | 16.1514 | 24.5975 | 1.42639 | 0.0000 | 1.42639 | 12.6619 | 1.9464 | +2.4311+0.1 |
| 36 | 1.9574 | 4354.16 | - | 24.5975 | 16.1514 | 18.3146 | 16.6763 | *0.0000 | 15.5575 | 15.5575 | 1.6844 | 0.82218+0.3 | +2.4423+0.1 |
| 35 | 1.9499 | 4257.84 | 2.1622 | 24.5975 | 19.0571 | 16.6232 | 16.6763 | *0.0000 | 15.5575 | 15.5575 | 2.6384 | 0.82326+0.3 | +2.4275+0.1 |
| 34 | 1.9422 | 4162.34 | 2.1622 | 24.5975 | 15.2327 | 15.2327 | 16.6763 | *0.0000 | 15.5575 | 15.5575 | 3.4996 | 0.82394+0.3 | +2.3743+0.1 |
| 33 | 1.9345 | 4067.62 | 2.1622 | 24.5975 | 12.0674 | 12.0674 | 16.6763 | *0.0000 | 15.5575 | 15.5575 | 4.4134 | 0.82431+0.3 | +2.325+0.1 |
| 32 | 1.9261 | 3983.63 | 2.2221 | 24.5975 | 9.0500 | 9.0500 | 16.6763 | *0.0000 | 15.5575 | 15.5575 | 8.6902 | 0.83221+0.3 | +2.221+0.1 |
| 31 | 1.9178 | 2983.11 | 2.2221 | 24.5975 | 20.1754 | 20.1754 | 16.6763 | *0.0000 | 15.5575 | 15.5575 | 6.3901 | 0.83901+0.3 | +1.7153+0.1 |
| 30 | 1.9104 | 2983.11 | 2.2221 | 24.5975 | 20.2223 | 20.2223 | 16.6763 | *0.0000 | 15.5575 | 15.5575 | 9.0500 | 0.86982+0.3 | +1.9114+0.1 |
| 29 | 1.8752 | 2973.63 | 1.6575 | 24.5975 | 17.9489 | 20.0000 | 16.6763 | *0.0000 | 15.5575 | 15.5575 | 10.0000 | 0.86982+0.3 | +1.7808+0.1 |
| 28 | 1.8751 | 2335.91 | 1.7025 | 24.5975 | 20.0000 | 20.0000 | 16.6763 | *0.0000 | 15.5575 | 15.5575 | 10.0000 | 0.86350+0.3 | +1.6215+0.1 |
| 27 | 1.8736 | 2190.69 | 1.7025 | 24.5975 | 20.0000 | 20.0000 | 16.6763 | *0.0000 | 15.5575 | 15.5575 | 10.0000 | 0.86350+0.3 | +1.4717+0.1 |
| 26 | 1.8728 | 2035.14 | 1.6091 | 24.5975 | 20.0000 | 20.0000 | 16.6763 | *0.0000 | 15.5575 | 15.5575 | 10.0000 | 0.86946+0.3 | +1.3519+0.1 |
| 25 | 1.8726 | 1859.58 | 1.3722 | 24.5975 | 20.7054 | 20.7054 | 16.6763 | *0.0000 | 15.5575 | 15.5575 | 10.0000 | 0.89607+0.3 | +1.9588 |
| 24 | 1.8707 | 1559.49 | 0.3959 | 24.5975 | 30.4073 | 10.4073 | 16.6763 | *0.0000 | 15.5575 | 15.5575 | 10.0000 | 0.91624+0.3 | +20.030 |
| 23 | 1.8694 | 890.83 | 4.0068 | 24.5975 | 33.9922 | 13.9922 | 16.6763 | *0.0000 | 15.5575 | 15.5575 | 10.0000 | 0.91624+0.3 | +20.033 |
| 22 | 1.8685 | 479.45 | 2.0332 | 24.5975 | 34.0000 | 14.0000 | 16.6763 | *0.0000 | 15.5575 | 15.5575 | 10.0000 | 0.91624+0.3 | +20.033 |
| 21 | 1.8664 | 479.45 | 1.6523 | 24.5975 | 34.0000 | 14.0000 | 16.6763 | *0.0000 | 15.5575 | 15.5575 | 10.0000 | 0.91624+0.3 | +20.033 |
| 20 | 1.8598 | 126.32 | 0.5318 | 24.5975 | 34.0000 | 14.0000 | 16.6763 | *0.0000 | 15.5575 | 15.5575 | 10.0000 | 0.91624+0.3 | +20.033 |
| 19 | 1.8539 | 104.45 | 0.0685 | 24.5975 | 34.0000 | 14.0000 | 16.6763 | *0.0000 | 15.5575 | 15.5575 | 10.0000 | 0.91624+0.3 | +20.033 |
| 18 | 1.8482 | 101.00 | 0.014 | 24.5975 | 34.0000 | 14.0000 | 16.6763 | *0.0000 | 15.5575 | 15.5575 | 10.0000 | 0.91624+0.3 | +20.033 |
| 17 | 1.8426 | 100.43 | 0.0063 | 24.5975 | 34.0000 | 14.0000 | 16.6763 | *0.0000 | 15.5575 | 15.5575 | 10.0000 | 0.91624+0.3 | +20.033 |
| 16 | 1.8370 | 100.33 | 0.0000 | 24.5975 | 34.0000 | 14.0000 | 16.6763 | *0.0000 | 15.5575 | 15.5575 | 10.0000 | 0.91624+0.3 | +20.033 |
| 15 | 1.8315 | 100.31 | 0.0000 | 24.5975 | 34.0000 | 14.0000 | 16.6763 | *0.0000 | 15.5575 | 15.5575 | 10.0000 | 0.91624+0.3 | +20.033 |
| 14 | 1.8271 | 100.30 | 0.0000 | 24.5975 | 34.0000 | 14.0000 | 16.6763 | *0.0000 | 15.5575 | 15.5575 | 10.0000 | 0.91624+0.3 | +20.033 |
| 13 | 1.8226 | 100.30 | 0.0000 | 24.5975 | 34.0000 | 14.0000 | 16.6763 | *0.0000 | 15.5575 | 15.5575 | 10.0000 | 0.91624+0.3 | +20.033 |
| 12 | 1.8204 | 100.30 | 0.0000 | 24.5975 | 34.0000 | 14.0000 | 16.6763 | *0.0000 | 15.5575 | 15.5575 | 10.0000 | 0.91624+0.3 | +20.033 |
| 11 | 1.8141 | 100.30 | 0.0000 | 24.5975 | 34.0000 | 14.0000 | 16.6763 | *0.0000 | 15.5575 | 15.5575 | 10.0000 | 0.91624+0.3 | +20.033 |
| 10 | 1.8077 | 100.30 | 0.0000 | 24.5975 | 34.0000 | 14.0000 | 16.6763 | *0.0000 | 15.5575 | 15.5575 | 10.0000 | 0.91624+0.3 | +20.033 |
| 9 | 1.8031 | 100.30 | 0.0000 | 24.5975 | 34.0000 | 14.0000 | 16.6763 | *0.0000 | 15.5575 | 15.5575 | 10.0000 | 0.91624+0.3 | +20.033 |
| 8 | 1.7746 | 100.30 | 0.0000 | 24.5975 | 34.0000 | 14.0000 | 16.6763 | *0.0000 | 15.5575 | 15.5575 | 10.0000 | 0.91624+0.3 | +20.033 |
| 7 | 1.7183 | 100.30 | 0.0000 | 24.5975 | 34.0000 | 14.0000 | 16.6763 | *0.0000 | 15.5575 | 15.5575 | 10.0000 | 0.91624+0.3 | +20.033 |
| 6 | 1.6619 | 100.30 | 0.0000 | 24.5975 | 34.0000 | 14.0000 | 16.6763 | *0.0000 | 15.5575 | 15.5575 | 10.0000 | 0.91624+0.3 | +20.033 |
| 5 | 1.6054 | 100.30 | 0.0000 | 24.5975 | 34.0000 | 14.0000 | 16.6763 | *0.0000 | 15.5575 | 15.5575 | 10.0000 | 0.91624+0.3 | +20.033 |
| 4 | 1.4667 | 100.30 | 0.0000 | 24.5975 | 34.0000 | 14.0000 | 16.6763 | *0.0000 | 15.5575 | 15.5575 | 10.0000 | 0.91624+0.3 | +20.033 |
| 3 | 1.0102 | 100.30 | 0.0000 | 24.5975 | 34.0000 | 14.0000 | 16.6763 | *0.0000 | 15.5575 | 15.5575 | 10.0000 | 0.91624+0.3 | +20.033 |
| 2 | 0.0150 | 100.30 | 0.0000 | 24.5975 | 34.0000 | 14.0000 | 16.6763 | *0.0000 | 15.5575 | 15.5575 | 10.0000 | 0.91624+0.3 | +20.033 |
| 1 | 0.0000 | 100.30 | 0.0000 | 24.5975 | 34.0000 | 14.0000 | 16.6763 | *0.0000 | 15.5575 | 15.5575 | 10.0000 | 0.91624+0.3 | +20.033 |

GAS FLOW SOURCES AND SINKS
NOCE RATE (LBM/H) [LBIN/HODE-SEC]

— CONCENTRATIONS — 18/MAY/1910

TIME= 200.00 TOTAL ITERS= 547

| 80 NODE | DISTANCE FROM BACK (IN) | TEMP (DEG F) | CONDUCTED HEAT FLUX (BTU/FT ² -SEC) | INTERNAL PRESSURE (LB/FT ²) | | | MOL #1 | MOL #2 | MOL #3 |
|------------|-------------------------|--------------|--|---|---------|---------------------------------|---------|---------|------------|
| | | | | DECOMP | TOTAL | DENSITIES (LB/FT ³) | | | |
| 34 | 1.9315 | 2685.31 | 0.0000 | 16.7289 | 16.7289 | 13.4931 | 2.2356 | 19.3667 | +3.6848+01 |
| 35 | 1.9162 | 2664.27 | 3.5773 | 16.3584 | 16.3584 | 13.2022 | 3.1363 | 19.1470 | +370846+01 |
| 35 | 1.9049 | 2642.71 | 3.6007 | 17.2724 | 17.2724 | 13.1389 | 4.1337 | 18.9119 | +373466+01 |
| 35 | 1.8914 | 2620.44 | 3.6796 | 19.3169 | 19.3169 | 14.1264 | 5.1105 | 18.7000 | +37719+01 |
| 35 | 1.8781 | 2597.47 | 3.8884 | 21.3513 | 21.3513 | 15.0299 | 6.3214 | 18.4811 | +38438+01 |
| 34 | 1.8216 | 2491.63 | 4.1785 | 25.4263 | 25.4263 | 15.7427 | 8.6336 | 18.2880 | +38288+01 |
| 32 | 1.7452 | 2369.63 | 4.5625 | 27.4521 | 27.4521 | 16.0536 | 10.0000 | 18.025 | +37251+01 |
| 32 | 1.7087 | 2229.01 | 4.65628 | 23.1680 | 23.1680 | 13.2731 | 0.0000 | 9.8949 | +34288+01 |
| 31 | 1.6523 | 2067.94 | 4.5341 | 21.0153 | 21.0153 | 11.0375 | 0.0000 | 9.9778 | +36598+01 |
| 30 | 1.5958 | 1881.74 | 4.3926 | 20.6984 | 20.6984 | 10.0721 | 0.0000 | 9.9948 | +36168+01 |
| 29 | 1.5393 | 1658.49 | 4.2330 | 20.0002 | 20.0002 | 10.0000 | 0.0000 | 10.0000 | +32768+01 |
| 28 | 1.5252 | 1594.46 | 4.1435 | 20.0000 | 20.0000 | 10.0000 | 0.0000 | 10.0000 | +30300+01 |
| 28 | 1.5111 | 1525.06 | 3.9741 | 20.4205 | 20.4205 | 10.0000 | 0.0000 | 10.0000 | +28195+01 |
| 28 | 1.4970 | 1443.23 | 3.5105 | 22.5993 | 22.5993 | 10.0000 | 0.0000 | 10.0000 | +24969+01 |
| 28 | 1.4829 | 1322.30 | 2.6316 | 29.0091 | 29.0091 | 10.0000 | 0.0000 | 10.0000 | +16452+01 |
| 27 | 1.4688 | 1100.45 | 2.1436 | 33.4154 | 33.4154 | 12.4154 | 0.0000 | 10.0000 | +20100+00 |
| 27 | 1.4547 | 844.09 | 1.5052 | 33.9725 | 33.9725 | 10.0000 | 0.0000 | 10.0000 | +82993+02 |
| 27 | 1.4405 | 448.46 | 1.1461 | 33.9989 | 33.9989 | 10.0000 | 0.0000 | 10.0000 | +26383+03 |
| 27 | 1.3264 | 504.05 | .5354 | 34.0000 | 34.0000 | 10.0000 | 0.0000 | 10.0000 | +54289+05 |
| 26 | 1.3700 | 291.73 | .1926 | 34.0000 | 34.0000 | 10.0000 | 0.0000 | 10.0000 | +16477+03 |
| 25 | 1.3135 | 146.15 | .0646 | 34.0000 | 34.0000 | 10.0000 | 0.0000 | 10.0000 | +12638+03 |
| 24 | 1.2571 | 114.15 | .0200 | 34.0000 | 34.0000 | 10.0000 | 0.0000 | 10.0000 | +12628+03 |
| 23 | 1.2004 | 104.14 | .0057 | 34.0000 | 34.0000 | 10.0000 | 0.0000 | 10.0000 | +12637+03 |
| 22 | 1.1491 | 101.32 | .0015 | 34.0000 | 34.0000 | 10.0000 | 0.0000 | 10.0000 | +12637+03 |
| 21 | 1.0877 | 100.56 | .0004 | 34.0000 | 34.0000 | 10.0000 | 0.0000 | 10.0000 | +12637+03 |
| 20 | 1.0312 | 100.34 | .0001 | 34.0000 | 34.0000 | 10.0000 | 0.0000 | 10.0000 | +12637+03 |
| 19 | .9746 | 100.31 | .0000 | 34.0000 | 34.0000 | 10.0000 | 0.0000 | 10.0000 | +12637+03 |
| 18 | .9183 | 100.30 | .0000 | 34.0000 | 34.0000 | 10.0000 | 0.0000 | 10.0000 | +12637+03 |
| 17 | .8619 | 100.30 | .0000 | 34.0000 | 34.0000 | 10.0000 | 0.0000 | 10.0000 | +12637+03 |
| 16 | .8054 | 100.30 | .0000 | 34.0000 | 34.0000 | 10.0000 | 0.0000 | 10.0000 | +12637+03 |
| 15 | .7489 | 100.30 | .0000 | 34.0000 | 34.0000 | 10.0000 | 0.0000 | 10.0000 | +12637+03 |
| 14 | .6925 | 100.30 | .0000 | 34.0000 | 34.0000 | 10.0000 | 0.0000 | 10.0000 | +12637+03 |
| 13 | .6360 | 100.30 | .0000 | 34.0000 | 34.0000 | 10.0000 | 0.0000 | 10.0000 | +12637+03 |
| 12 | .5794 | 100.30 | .0000 | 34.0000 | 34.0000 | 10.0000 | 0.0000 | 10.0000 | +12637+03 |
| 11 | .5231 | 100.30 | .0000 | 34.0000 | 34.0000 | 10.0000 | 0.0000 | 10.0000 | +12637+03 |
| 10 | .4667 | 100.30 | .0000 | 34.0000 | 34.0000 | 10.0000 | 0.0000 | 10.0000 | +12637+03 |
| 9 | .4102 | 100.30 | .0000 | 34.0000 | 34.0000 | 10.0000 | 0.0000 | 10.0000 | +12637+03 |
| 8 | .3537 | 100.30 | .0000 | 34.0000 | 34.0000 | 10.0000 | 0.0000 | 10.0000 | +12637+03 |
| 7 | .2973 | 100.30 | .0000 | 34.0000 | 34.0000 | 10.0000 | 0.0000 | 10.0000 | +12637+03 |
| 6 | .2508 | 100.30 | .0000 | 34.0000 | 34.0000 | 10.0000 | 0.0000 | 10.0000 | +12637+03 |
| 5 | .1919 | 100.30 | .0000 | 34.0000 | 34.0000 | 10.0000 | 0.0000 | 10.0000 | +12637+03 |
| 4 | .1274 | 100.30 | .0000 | 34.0000 | 34.0000 | 10.0000 | 0.0000 | 10.0000 | +12637+03 |
| 3 | .0715 | 100.30 | .0000 | 34.0000 | 34.0000 | 10.0000 | 0.0000 | 10.0000 | +12637+03 |
| 2 | .0150 | 100.30 | .0000 | 34.0000 | 34.0000 | 10.0000 | 0.0000 | 10.0000 | +12637+03 |
| 1 | .0000 | 100.30 | .0000 | 34.0000 | 34.0000 | 10.0000 | 0.0000 | 10.0000 | +12637+03 |

GAS FLOW SOURCES AND THERMS
NODE RATE(MOL/FT²-SEC) PYRO DEPO S1-C INT. SOMP OXYGEN NITROGEN HYDROGEN PYRO DEPO S10 CONCENTRATIONS (LBM/FT³ VOID)
1013-02 .00 .91-11 .00 .645-04 .244-04 .000 .371-05 .149-03 .505-03

| | | | | | | | | | | | |
|----|-----------|-----|--------|-----|---------|---------|---------|---------|---------|---------|-----|
| 35 | *1012*-02 | *00 | *24*05 | *00 | *52-11 | *24*04 | *172-04 | *238-03 | *172-04 | *24*05 | *00 |
| 35 | *1009*-02 | *00 | *26-05 | *00 | *52-11 | *229-03 | *178-04 | *241-04 | *178-04 | *26-05 | *00 |
| 35 | *1006*-02 | *00 | *32-05 | *00 | *21-10 | *220-03 | *195-04 | *29-04 | *195-04 | *32-05 | *00 |
| 35 | *1003*-02 | *00 | *12-07 | *00 | *12-07 | *211-03 | *191-04 | *314-04 | *191-04 | *12-07 | *00 |
| 35 | *9939*-03 | *00 | *30-06 | *00 | *13-04 | *454-04 | *178-03 | *219-04 | *178-03 | *30-06 | *00 |
| 34 | *9914*-03 | *00 | *74-05 | *00 | *370-04 | *370-04 | *147-03 | *250-04 | *147-03 | *74-05 | *00 |
| 33 | *9811*-03 | *00 | *16-03 | *00 | *297-04 | *297-04 | *121-03 | *281-04 | *121-03 | *16-03 | *00 |
| 32 | *9716*-02 | *00 | *17-03 | *00 | *232-04 | *974-04 | *274-04 | *808-04 | *274-04 | *17-03 | *00 |
| 31 | *9714*-02 | *00 | *21-04 | *00 | *177-04 | *773-04 | *241-04 | *125-03 | *241-04 | *21-04 | *00 |
| 30 | *9712*-02 | *00 | *40-06 | *00 | *132-04 | *621-04 | *206-04 | *104-03 | *206-04 | *40-06 | *00 |
| 29 | *9714*-02 | *00 | *00 | *00 | *132-04 | *132-04 | *104-03 | *206-03 | *104-03 | *00 | *00 |
| 28 | *9714*-02 | *00 | *00 | *00 | *118-04 | *575-04 | *194-04 | *206-03 | *194-04 | *118-04 | *00 |
| 28 | *9714*-02 | *00 | *00 | *00 | *105-04 | *105-04 | *183-04 | *230-03 | *183-04 | *105-04 | *00 |
| 28 | *9714*-02 | *00 | *00 | *00 | *940-05 | *502-05 | *173-04 | *256-03 | *173-04 | *940-05 | *00 |
| 28 | *9714*-02 | *00 | *00 | *00 | *868-05 | *483-05 | *166-04 | *261-03 | *166-04 | *868-05 | *00 |
| 28 | *9714*-02 | *00 | *00 | *00 | *854-05 | *483-05 | *164-04 | *289-03 | *164-04 | *854-05 | *00 |
| 27 | *9714*-02 | *00 | *00 | *00 | *853-05 | *483-05 | *164-04 | *289-03 | *164-04 | *853-05 | *00 |
| 27 | *9714*-02 | *00 | *00 | *00 | *853-05 | *483-05 | *164-04 | *289-03 | *164-04 | *853-05 | *00 |
| 27 | *9714*-02 | *00 | *00 | *00 | *853-05 | *483-05 | *164-04 | *289-03 | *164-04 | *853-05 | *00 |
| 27 | *9714*-02 | *00 | *00 | *00 | *853-05 | *483-05 | *164-04 | *289-03 | *164-04 | *853-05 | *00 |
| 27 | *9714*-02 | *00 | *00 | *00 | *853-05 | *483-05 | *164-04 | *289-03 | *164-04 | *853-05 | *00 |
| 27 | *9714*-02 | *00 | *00 | *00 | *853-05 | *483-05 | *164-04 | *289-03 | *164-04 | *853-05 | *00 |
| 27 | *9714*-02 | *00 | *00 | *00 | *853-05 | *483-05 | *164-04 | *289-03 | *164-04 | *853-05 | *00 |
| 27 | *9714*-02 | *00 | *00 | *00 | *853-05 | *483-05 | *164-04 | *289-03 | *164-04 | *853-05 | *00 |
| 26 | *9714*-02 | *00 | *00 | *00 | *853-05 | *483-05 | *164-04 | *289-03 | *164-04 | *853-05 | *00 |
| 26 | *9714*-02 | *00 | *00 | *00 | *853-05 | *483-05 | *164-04 | *289-03 | *164-04 | *853-05 | *00 |
| 26 | *9714*-02 | *00 | *00 | *00 | *853-05 | *483-05 | *164-04 | *289-03 | *164-04 | *853-05 | *00 |
| 25 | *9714*-02 | *00 | *00 | *00 | *853-05 | *483-05 | *164-04 | *289-03 | *164-04 | *853-05 | *00 |
| 25 | *9714*-02 | *00 | *00 | *00 | *853-05 | *483-05 | *164-04 | *289-03 | *164-04 | *853-05 | *00 |
| 24 | *9714*-02 | *00 | *00 | *00 | *853-05 | *483-05 | *164-04 | *289-03 | *164-04 | *853-05 | *00 |
| 23 | *9714*-02 | *00 | *00 | *00 | *853-05 | *483-05 | *164-04 | *289-03 | *164-04 | *853-05 | *00 |
| 23 | *9714*-02 | *00 | *00 | *00 | *853-05 | *483-05 | *164-04 | *289-03 | *164-04 | *853-05 | *00 |
| 22 | *9714*-02 | *00 | *00 | *00 | *853-05 | *483-05 | *164-04 | *289-03 | *164-04 | *853-05 | *00 |
| 21 | *9714*-02 | *00 | *00 | *00 | *853-05 | *483-05 | *164-04 | *289-03 | *164-04 | *853-05 | *00 |
| 20 | *9714*-02 | *00 | *00 | *00 | *853-05 | *483-05 | *164-04 | *289-03 | *164-04 | *853-05 | *00 |
| 19 | *9714*-02 | *00 | *00 | *00 | *853-05 | *483-05 | *164-04 | *289-03 | *164-04 | *853-05 | *00 |
| 18 | *9714*-02 | *00 | *00 | *00 | *853-05 | *483-05 | *164-04 | *289-03 | *164-04 | *853-05 | *00 |
| 17 | *9714*-02 | *00 | *00 | *00 | *853-05 | *483-05 | *164-04 | *289-03 | *164-04 | *853-05 | *00 |
| 16 | *9714*-02 | *00 | *00 | *00 | *853-05 | *483-05 | *164-04 | *289-03 | *164-04 | *853-05 | *00 |
| 15 | *9714*-02 | *00 | *00 | *00 | *853-05 | *483-05 | *164-04 | *289-03 | *164-04 | *853-05 | *00 |
| 14 | *9714*-02 | *00 | *00 | *00 | *853-05 | *483-05 | *164-04 | *289-03 | *164-04 | *853-05 | *00 |
| 13 | *9714*-02 | *00 | *00 | *00 | *853-05 | *483-05 | *164-04 | *289-03 | *164-04 | *853-05 | *00 |
| 12 | *9714*-02 | *00 | *00 | *00 | *853-05 | *483-05 | *164-04 | *289-03 | *164-04 | *853-05 | *00 |
| 11 | *9714*-02 | *00 | *00 | *00 | *853-05 | *483-05 | *164-04 | *289-03 | *164-04 | *853-05 | *00 |
| 10 | *9714*-02 | *00 | *00 | *00 | *853-05 | *483-05 | *164-04 | *289-03 | *164-04 | *853-05 | *00 |
| 9 | *9714*-02 | *00 | *00 | *00 | *853-05 | *483-05 | *164-04 | *289-03 | *164-04 | *853-05 | *00 |
| 8 | *9714*-02 | *00 | *00 | *00 | *853-05 | *483-05 | *164-04 | *289-03 | *164-04 | *853-05 | *00 |
| 7 | *9714*-02 | *00 | *00 | *00 | *853-05 | *483-05 | *164-04 | *289-03 | *164-04 | *853-05 | *00 |
| 6 | *9714*-02 | *00 | *00 | *00 | *853-05 | *483-05 | *164-04 | *289-03 | *164-04 | *853-05 | *00 |
| 5 | *9714*-02 | *00 | *00 | *00 | *853-05 | *483-05 | *164-04 | *289-03 | *164-04 | *853-05 | *00 |
| 4 | *9714*-02 | *00 | *00 | *00 | *853-05 | *483-05 | *164-04 | *289-03 | *164-04 | *853-05 | *00 |
| 3 | *9714*-02 | *00 | *00 | *00 | *853-05 | *483-05 | *164-04 | *289-03 | *164-04 | *853-05 | *00 |
| 2 | *9714*-02 | *00 | *00 | *00 | *853-05 | *483-05 | *164-04 | *289-03 | *164-04 | *853-05 | *00 |
| 1 | *9714*-02 | *00 | *00 | *00 | *853-05 | *483-05 | *164-04 | *289-03 | *164-04 | *853-05 | *00 |

TIME= 500.00 TOTAL ITERATIONS= 853

82

| NODE | DISTANCE FROM BACK (IN) | CONDUCTED HEAT FLUX (BTU/FT ² -SEC) | | | DECOMP TOTAL DENSITIES (LBM/FT ³) | | | INTERNAL PRESSURE (LBF/FT ²) | NO. OF VELCITY (FT/SEC) |
|------|-------------------------|--|----------|--------|---|---------|-----------|--|-------------------------|
| | | CARBON | GRAPHITE | SILICA | DECOMP | TOTAL | DENSITIES | | |
| 35 | 1.00017 | 2248.31 | 0.0000 | 0.0000 | 19.0110 | 19.0110 | 0.0000 | 14.6114 | 5.1996 |
| 34 | 1.00667 | 2251.84 | 0.2102 | 0.0000 | 21.1016 | 0.0000 | 0.0000 | 15.0143 | 6.0814 |
| 34 | 1.0510 | 2253.95 | 0.0497 | 0.0000 | 22.0713 | 0.0000 | 0.0000 | 15.2461 | 6.8252 |
| 34 | 1.05266 | 2254.05 | 1.1222 | 0.0000 | 22.9149 | 0.0000 | 0.0000 | 15.4413 | 7.4736 |
| 34 | 1.09216 | 2253.94 | 0.9840 | 0.0000 | 23.7701 | 0.0000 | 0.0000 | 15.6436 | 8.4954 |
| 32 | 1.74552 | 2238.43 | 1.0740 | 0.0000 | 27.9165 | 0.0000 | 0.0000 | 16.6949 | 9.1246 |
| 32 | 1.75087 | 2203.70 | 1.5398 | 0.0000 | 26.9022 | 0.0000 | 0.0000 | 17.2087 | 9.2236 |
| 31 | 1.65223 | 2151.17 | 1.9447 | 0.0000 | 29.3131 | 0.0000 | 0.0000 | 19.4532 | 9.8559 |
| 30 | 1.65950 | 2081.10 | 2017.41 | 0.0000 | 22.3873 | 0.0000 | 0.0000 | 12.4477 | 9.2398 |
| 29 | 1.5393 | 1997.25 | 2.3213 | 0.0000 | 20.7011 | 0.0000 | 0.0000 | 10.7261 | 9.9750 |
| 28 | 1.48229 | 1899.71 | 2.4057 | 0.0000 | 20.1596 | 0.0000 | 0.0000 | 10.1690 | 9.9907 |
| 27 | 1.4264 | 1787.11 | 2.4319 | 0.0000 | 20.0287 | 0.0000 | 0.0000 | 10.0316 | 9.9971 |
| 26 | 1.3700 | 1656.42 | 2.3973 | 0.0000 | 20.0037 | 0.0000 | 0.0000 | 10.0043 | 9.9993 |
| 25 | 1.3135 | 1501.90 | 2.3371 | 0.0002 | 20.0002 | 0.0000 | 0.0000 | 10.0000 | 9.9951 |
| 24 | 1.2994 | 1458.56 | 2.3050 | 0.0000 | 20.0000 | 0.0000 | 0.0000 | 10.0000 | 9.9950 |
| 24 | 1.2853 | 1412.52 | 2.2455 | 0.0000 | 20.2273 | 0.0000 | 0.0000 | 10.0000 | 9.9950 |
| 24 | 1.2712 | 1361.99 | 2.1090 | 0.0000 | 21.3553 | 0.0000 | 0.0000 | 10.0000 | 9.9950 |
| 24 | 1.2571 | 1302.26 | 1.8642 | 0.0000 | 24.5102 | 0.0000 | 0.0000 | 10.0000 | 9.9950 |
| 23 | 1.2429 | 1223.26 | 1.5819 | 0.0000 | 28.9487 | 0.0000 | 0.0000 | 10.0000 | 9.9950 |
| 23 | 1.2288 | 1113.15 | 1.3264 | 0.0000 | 32.2779 | 0.0000 | 0.0000 | 10.0000 | 9.9950 |
| 23 | 1.2147 | 984.71 | 1.1148 | 0.0000 | 33.5453 | 0.0000 | 0.0000 | 10.0000 | 9.9950 |
| 23 | 1.2004 | 865.61 | 942.11 | 0.0000 | 33.9439 | 0.0000 | 0.0000 | 10.0000 | 9.9950 |
| 22 | 1.1865 | 763.39 | 797.2 | 0.0000 | 33.9809 | 0.0000 | 0.0000 | 10.0000 | 9.9950 |
| 22 | 1.1724 | 676.62 | 647.70 | 0.0000 | 33.9954 | 0.0000 | 0.0000 | 10.0000 | 9.9950 |
| 22 | 1.1583 | 603.05 | 574.5 | 0.0000 | 33.9989 | 0.0000 | 0.0000 | 10.0000 | 9.9950 |
| 22 | 1.1441 | 540.46 | 414.60 | 0.0000 | 34.0070 | 0.0000 | 0.0000 | 10.0000 | 9.9950 |
| 21 | 1.0877 | 360.48 | 254.3 | 0.0000 | 34.0000 | 0.0000 | 0.0000 | 10.0000 | 9.9950 |
| 20 | 1.0312 | 250.24 | 150.9 | 0.0000 | 34.0000 | 0.0000 | 0.0000 | 10.0000 | 9.9950 |
| 19 | 974.8 | 164.81 | .0677 | 0.0000 | 14.0000 | 0.0000 | 0.0000 | 10.0000 | 9.9950 |
| 18 | 918.3 | 146.73 | .0498 | 0.0000 | 14.0000 | 0.0000 | 0.0000 | 10.0000 | 9.9950 |
| 17 | 861.9 | 125.07 | .0275 | 0.0000 | 14.0000 | 0.0000 | 0.0000 | 10.0000 | 9.9950 |
| 16 | 805.4 | 113.12 | .0147 | 0.0000 | 14.0000 | 0.0000 | 0.0000 | 10.0000 | 9.9950 |
| 15 | 748.9 | 106.72 | .0074 | 0.0000 | 14.0000 | 0.0000 | 0.0000 | 10.0000 | 9.9950 |
| 14 | 692.5 | 103.42 | .0038 | 0.0000 | 14.0000 | 0.0000 | 0.0000 | 10.0000 | 9.9950 |
| 13 | 643.6 | 101.76 | .0018 | 0.0000 | 14.0000 | 0.0000 | 0.0000 | 10.0000 | 9.9950 |
| 12 | 579.6 | 100.98 | .0009 | 0.0000 | 14.0000 | 0.0000 | 0.0000 | 10.0000 | 9.9950 |
| 11 | 523.1 | 100.59 | .0004 | 0.0000 | 14.0000 | 0.0000 | 0.0000 | 10.0000 | 9.9950 |
| 10 | 566.7 | 100.42 | .0002 | 0.0000 | 14.0000 | 0.0000 | 0.0000 | 10.0000 | 9.9950 |
| 9 | 410.2 | 100.35 | .0001 | 0.0000 | 14.0000 | 0.0000 | 0.0000 | 10.0000 | 9.9950 |
| 8 | 353.7 | 100.32 | .0000 | 0.0000 | 14.0000 | 0.0000 | 0.0000 | 10.0000 | 9.9950 |
| 7 | 297.9 | 100.30 | .0000 | 0.0000 | 14.0000 | 0.0000 | 0.0000 | 10.0000 | 9.9950 |
| 6 | 240.6 | 100.30 | .0000 | 0.0000 | 14.0000 | 0.0000 | 0.0000 | 10.0000 | 9.9950 |
| 5 | 184.4 | 100.30 | .0000 | 0.0000 | 14.0000 | 0.0000 | 0.0000 | 10.0000 | 9.9950 |
| 4 | 127.9 | 100.30 | .0000 | 0.0000 | 14.0000 | 0.0000 | 0.0000 | 10.0000 | 9.9950 |
| 3 | 70.15 | 100.30 | .0000 | 0.0000 | 14.0000 | 0.0000 | 0.0000 | 10.0000 | 9.9950 |
| 2 | 0.150 | 100.30 | .0000 | 0.0000 | 14.0000 | 0.0000 | 0.0000 | 10.0000 | 9.9950 |
| 1 | .0000 | 100.30 | .0000 | 0.0000 | 14.0000 | 0.0000 | 0.0000 | 10.0000 | 9.9950 |

----- CONCENTRATIONS -----
 SAI FLOW
 MODE RATE (LBM/SEC)
 PYRO DEPO SI-C INT COMB OXYGEN NITROGEN HYDROGEN PYRO DEPO SIO BURN TOTAL
 (LBM/SEC) (LBM/SEC) (LBM/SEC)

| | | | | | | | | | | | | | | |
|----|----------|------|----------|--------|--------|---------|---------|---------|---------|---------|---------|---------|---------|---------|
| 35 | .6834-03 | .900 | .26-11 | .30-06 | .00 | .507-03 | .194-04 | .000 | .222-02 | .504-04 | .000 | .507-05 | .324-02 | |
| 34 | .6821-03 | .000 | .16-10 | .72-06 | .00 | .57-03 | .216-02 | .000 | .593-03 | .210-02 | .000 | .639-05 | .429-03 | |
| 34 | .6823-03 | .000 | .14-09 | .81-04 | .00 | .593-03 | .210-02 | .000 | .503-04 | .770-04 | .000 | .763-05 | .517-03 | |
| 34 | .6815-03 | .000 | .84-08 | .89-04 | .00 | .536-03 | .204-02 | .000 | .536-04 | .900-04 | .000 | .876-05 | .604-03 | |
| 34 | .6806-03 | .000 | .54-05 | .23-05 | .00 | .520-03 | .197-02 | .000 | .610-04 | .103-03 | .000 | .690-03 | .333-02 | |
| 33 | .6838-03 | .000 | .13-03 | .38-05 | .00 | .457-03 | .175-02 | .000 | .451-04 | .150-03 | .000 | .127-04 | .981-03 | |
| 32 | .6810-03 | .000 | .00 | .32-05 | .00 | .369-03 | .150-02 | .000 | .607-04 | .281-03 | .000 | .136-04 | .122-02 | |
| 31 | .6807-03 | .000 | .00 | .65-04 | .24-05 | .00 | .329-03 | .128-02 | .000 | .692-04 | .398-03 | .000 | .134-04 | .142-02 |
| 30 | .6803-03 | .000 | .38-04 | .16-05 | .00 | .276-03 | .09-02 | .000 | .672-04 | .535-03 | .000 | .122-04 | .159-02 | |
| 29 | .6806-03 | .000 | .16-04 | .91-04 | .00 | .232-03 | .024-03 | .000 | .618-04 | .672-02 | .000 | .108-04 | .172-02 | |
| 28 | .6821-03 | .000 | .56-05 | .46-04 | .00 | .195-03 | .786-03 | .000 | .687-03 | .807-03 | .000 | .92-05 | .184-02 | |
| 27 | .6826-03 | .000 | .16-05 | .19-04 | .00 | .162-03 | .470-03 | .000 | .687-04 | .940-03 | .000 | .763-05 | .197-02 | |
| 26 | .6822-03 | .000 | .35-06 | .62-07 | .00 | .135-03 | .571-03 | .000 | .623-04 | .101-02 | .000 | .453-05 | .353-02 | |
| 25 | .6827-03 | .000 | .00 | .00 | .00 | .109-03 | .477-03 | .000 | .555-04 | .124-02 | .000 | .526-05 | .229-02 | |
| 24 | .6827-03 | .000 | .14-03 | .14-03 | .00 | .101-03 | .449-03 | .000 | .53-04 | .12-02 | .000 | .488-05 | .426-02 | |
| 24 | .6827-03 | .000 | .34-04 | .00 | .00 | .933-04 | .423-03 | .000 | .512-04 | .135-02 | .000 | .451-05 | .242-02 | |
| 24 | .6838-03 | .000 | .14-03 | .00 | .00 | .683-04 | .499-03 | .000 | .49-04 | .140-02 | .000 | .418-05 | .444-02 | |
| 24 | .6826-03 | .000 | .26-03 | .00 | .00 | .003-04 | .378-03 | .000 | .913-04 | .154-02 | .000 | .389-05 | .257-02 | |
| 23 | .6819-03 | .000 | .7579-03 | .26-03 | .00 | .740-04 | .365-03 | .000 | .46-04 | .152-02 | .000 | .368-05 | .210-02 | |
| 23 | .6819-03 | .000 | .14-03 | .14-03 | .00 | .700-04 | .359-03 | .000 | .554-04 | .155-02 | .000 | .356-05 | .270-02 | |
| 23 | .6820-03 | .000 | .5426-04 | .41-04 | .00 | .733-04 | .357-03 | .000 | .492-04 | .152-02 | .000 | .355-05 | .277-02 | |
| 23 | .6827-04 | .000 | .1287-04 | .99-05 | .00 | .712-04 | .356-03 | .000 | .451-04 | .157-02 | .000 | .354-05 | .273-02 | |
| 23 | .6829-05 | .000 | .2969-05 | .23-05 | .00 | .731-04 | .355-03 | .000 | .451-04 | .157-02 | .000 | .354-05 | .273-02 | |
| 22 | .6814-04 | .000 | .6814-04 | .54-04 | .00 | .731-04 | .354-03 | .000 | .451-04 | .157-02 | .000 | .354-05 | .273-02 | |
| 22 | .6814-04 | .000 | .1460-04 | .13-04 | .00 | .731-04 | .354-03 | .000 | .45-04 | .157-02 | .000 | .354-05 | .273-02 | |
| 22 | .6814-04 | .000 | .1460-07 | .14-07 | .00 | .731-04 | .356-03 | .000 | .45-04 | .157-02 | .000 | .354-05 | .273-02 | |
| 21 | .0000 | .000 | .0000 | .0000 | .00 | .731-04 | .356-03 | .000 | .451-04 | .157-02 | .000 | .354-05 | .273-02 | |
| 20 | .0000 | .000 | .0000 | .0000 | .00 | .731-04 | .356-03 | .000 | .451-04 | .157-02 | .000 | .354-05 | .273-02 | |
| 19 | .0000 | .000 | .0000 | .0000 | .00 | .731-04 | .356-03 | .000 | .451-04 | .157-02 | .000 | .354-05 | .273-02 | |
| 18 | .0000 | .000 | .0000 | .0000 | .00 | .731-04 | .356-03 | .000 | .451-04 | .157-02 | .000 | .354-05 | .273-02 | |
| 17 | .0000 | .000 | .0000 | .0000 | .00 | .731-04 | .356-03 | .000 | .451-04 | .157-02 | .000 | .354-05 | .273-02 | |
| 16 | .0000 | .000 | .0000 | .0000 | .00 | .731-04 | .356-03 | .000 | .451-04 | .157-02 | .000 | .354-05 | .273-02 | |
| 15 | .0000 | .000 | .0000 | .0000 | .00 | .731-04 | .356-03 | .000 | .451-04 | .157-02 | .000 | .354-05 | .273-02 | |
| 14 | .0000 | .000 | .0000 | .0000 | .00 | .731-04 | .356-03 | .000 | .451-04 | .157-02 | .000 | .354-05 | .273-02 | |
| 13 | .0000 | .000 | .0000 | .0000 | .00 | .731-04 | .356-03 | .000 | .451-04 | .157-02 | .000 | .354-05 | .273-02 | |
| 12 | .0000 | .000 | .0000 | .0000 | .00 | .731-04 | .356-03 | .000 | .451-04 | .157-02 | .000 | .354-05 | .273-02 | |
| 11 | .0000 | .000 | .0000 | .0000 | .00 | .731-04 | .356-03 | .000 | .451-04 | .157-02 | .000 | .354-05 | .273-02 | |
| 10 | .0000 | .000 | .0000 | .0000 | .00 | .731-04 | .356-03 | .000 | .451-04 | .157-02 | .000 | .354-05 | .273-02 | |
| 9 | .0000 | .000 | .0000 | .0000 | .00 | .731-04 | .356-03 | .000 | .451-04 | .157-02 | .000 | .354-05 | .273-02 | |
| 8 | .0000 | .000 | .0000 | .0000 | .00 | .731-04 | .356-03 | .000 | .451-04 | .157-02 | .000 | .354-05 | .273-02 | |
| 7 | .0000 | .000 | .0000 | .0000 | .00 | .731-04 | .356-03 | .000 | .451-04 | .157-02 | .000 | .354-05 | .273-02 | |
| 6 | .0000 | .000 | .0000 | .0000 | .00 | .731-04 | .356-03 | .000 | .451-04 | .157-02 | .000 | .354-05 | .273-02 | |
| 5 | .0000 | .000 | .0000 | .0000 | .00 | .731-04 | .356-03 | .000 | .451-04 | .157-02 | .000 | .354-05 | .273-02 | |
| 4 | .0000 | .000 | .0000 | .0000 | .00 | .731-04 | .356-03 | .000 | .451-04 | .157-02 | .000 | .354-05 | .273-02 | |
| 3 | .0000 | .000 | .0000 | .0000 | .00 | .731-04 | .356-03 | .000 | .451-04 | .157-02 | .000 | .354-05 | .273-02 | |
| 2 | .0000 | .000 | .0000 | .0000 | .00 | .731-04 | .356-03 | .000 | .451-04 | .157-02 | .000 | .354-05 | .273-02 | |
| 1 | .0000 | .000 | .0000 | .0000 | .00 | .731-04 | .356-03 | .000 | .451-04 | .157-02 | .000 | .354-05 | .273-02 | |

SAMPLE CASE 11

Heat flux drive - DATA INPUT CARDS

```

- XQT MAIN
  FLUX DRIVE SAMPLE CASE
    1
    0.      1.0
    40.     0.2
   100.     1.0
   600.     2.0
 1078.     2.0
    0.      0.
    2
    0.      10.
   100.     20.
   600.     100.
 1078.     100.
    0.      0.
    3
    1
    0.  24751.  .00004
   20.  24843.  .00030  .067
   40.  24935.  .00061  12.33
   60.  24854.  .00391  33.88
   80.  22965.  .01086  192.31
 100.  18058.  .01341  30.31
 120.  14524.  .00932  7.25
 140.  12713.  .00786  3.91
 160.  11419.  .00660  2.43
 180.  10614.  .00503  1.75
 200.  10133.  .00395  1.47
 220.  9810.   .00335  1.36
 240.  9572.   .00308  1.26
 260.  9408.   .00295  1.22
 280.  9240.   .00282  1.19
 300.  9076.   .00268  1.15
 320.  8902.   .00285  1.10
 340.  8727.   .00302  1.05
 360.  8530.   .00326  0.985
 380.  8275.   .00381  0.925
 400.  7880.   .00475  0.905
 420.  7280.   .00607  0.97
 440.  6420.   .00755  1.115
 460.  5245.   .00865  1.22
 480.  3858.   .00939  1.14
 500.  2720.   .00861  0.785
 540.  1245.   .00685  0.245
 600.  560.    .00650
 700.  110.    .01030
 800.  114.    .01360
 900.  117.    .01460
1000. 123.    .01550
1078. 124.    .01603
    0.
    4
    0.  .0360    1.  .0006403
   40.  1.756   1.  .000639
   50.  10.5   1.  .001944
   60.  66.08   1.  .004779

```

| | | | |
|-------|----------|-------|---------|
| 70. | 393.0 | 1. | .008396 |
| 80. | 512.8 | 1. | .012207 |
| 85. | 767.0 | 1. | .01308 |
| 90. | 1030.0 | 1. | .013202 |
| 95. | 920.0 | 1. | .012724 |
| 100. | 818.1 | 1. | .012542 |
| 105. | 755.0 | 1. | .011384 |
| 110. | 651.0 | 1. | .009522 |
| 115. | 549.0 | 1. | .008698 |
| 120. | 410.9 | 1. | .007690 |
| 130. | 349.0 | 1. | .006707 |
| 140. | 298.0 | 1. | .006108 |
| 150. | 258.0 | 1. | .005552 |
| 160. | 213.4 | 1. | .004909 |
| 170. | 156.0 | 1. | .004192 |
| 180. | 125.1 | 1. | .003612 |
| 190. | 96.9 | 1. | .003218 |
| 200. | 77.7 | 1. | .00277 |
| 210. | 66.2 | 1. | .002416 |
| 240. | 47.5 | 1. | .002095 |
| 300. | 36.3 | 1. | .001795 |
| 350. | 49.8 | 1. | .002061 |
| 370. | 61.5 | 1. | .002261 |
| 390.. | 90.6 | 1. | .002834 |
| 410. | 147.0 | 1. | .003475 |
| 430. | 236.0 | 1. | .004399 |
| 450. | 366.0 | 1. | .005078 |
| 470. | 459.0 | 1. | .005091 |
| 480. | 496.0 | 1. | .004893 |
| 490. | 480.0 | 1. | .004296 |
| 510. | 411.0 | 1. | .003504 |
| 530. | 318.0 | 1. | .002628 |
| 550. | 287.0 | 1. | .002214 |
| 570. | 307.0 | 1. | .001667 |
| 706. | 734.0 | 1. | .001118 |
| 756. | 1115.0 | 1. | .001561 |
| 1078. | 2117.0 | 1. | .001972 |
| 0. | 0. | | |
| 2 | ALUMINUM | .015 | 1 |
| 1 | AVCOAT | 1.976 | 35 |
| 0 | | | |

560.

001882

0036

CALCULATION TIME STEP CONTROL TABLE

| TIME (SEC) | TIME STEP (SEC) |
|---------------|--------------------|
| *0.0 | 1.0000 |
| 40.00 | .2000 |
| 100.00 | 1.0000 |
| 400.00 | 2.0000 |
| 1078.00 | 2.0000 |

PRINT TIME STEP CONTROL TABLE

| TIME (SEC) | TIME STEP (SEC) |
|---------------|--------------------|
| *0.0 | 24751.00 |
| 20.00 | 24643.00 |
| 40.00 | 24355.00 |
| 60.00 | 24054.00 |
| 80.00 | 22965.00 |
| 100.00 | 16058.00 |
| 120.00 | 14524.00 |
| 140.00 | 12713.00 |
| 160.00 | 11419.00 |
| 180.00 | 10414.00 |
| 200.00 | 10335.00 |
| 220.00 | 9810.00 |
| 240.00 | 9572.00 |
| 260.00 | 9408.00 |
| 280.00 | 9240.00 |
| 300.00 | 9076.00 |
| 320.00 | 8902.00 |
| 340.00 | 8727.00 |
| 360.00 | 8550.00 |
| 380.00 | 8275.00 |
| 400.00 | 7880.00 |
| 420.00 | 7260.00 |
| 440.00 | 6920.00 |
| 460.00 | 5245.00 |
| 480.00 | 480.00 |
| 500.00 | 2720.00 |
| 540.00 | 1245.00 |
| 560.00 | 540.00 |
| 700.00 | 110.00 |
| 800.00 | 114.00 |
| 900.00 | 117.00 |
| 1000.00 | 123.00 |
| 1078.00 | 125.00 |

SURFACE HEAT FLUX TABLE

| TIME | RECOVERY ENTHALPY (BTU/LBM) | HEAT TRANSFER PARAMETER (BTU/FT ² SEC) (BTU/SEC) | MISC HEAT TO SURFACE (BTU/SEC) |
|---------|-----------------------------------|--|--------------------------------------|
| *0.0 | 0.0000 | 0.0000 | 0.000 |
| 20.00 | 24643.00 | 0.00030 | 0.07 |
| 40.00 | 24355.00 | 0.00061 | 1.2330 |
| 60.00 | 24054.00 | 0.00121 | 23.880 |
| 80.00 | 22965.00 | 0.00161 | 192.310 |
| 100.00 | 16058.00 | 0.01341 | 30.310 |
| 120.00 | 14524.00 | 0.00332 | 7.250 |
| 140.00 | 12713.00 | 0.00716 | 3.910 |
| 160.00 | 11419.00 | 0.00460 | 2.440 |
| 180.00 | 10414.00 | 0.00503 | 1.750 |
| 200.00 | 10335.00 | 0.00495 | 1.470 |
| 220.00 | 9810.00 | 0.00335 | 1.340 |
| 240.00 | 9572.00 | 0.00036 | 1.260 |
| 260.00 | 9408.00 | 0.00215 | 1.220 |
| 280.00 | 9240.00 | 0.00282 | 1.190 |
| 300.00 | 9076.00 | 0.00268 | 1.150 |
| 320.00 | 8902.00 | 0.00245 | 1.100 |
| 340.00 | 8727.00 | 0.00302 | 1.050 |
| 360.00 | 8550.00 | 0.00326 | 1.000 |
| 380.00 | 8275.00 | 0.00381 | 9.95 |
| 400.00 | 7880.00 | 0.00478 | 9.05 |
| 420.00 | 7260.00 | 0.00607 | 9.70 |
| 440.00 | 6920.00 | 0.00558 | 11.15 |
| 460.00 | 5245.00 | 0.00665 | 11.20 |
| 480.00 | 480.00 | 0.00639 | 11.40 |
| 500.00 | 2720.00 | 0.00661 | 7.85 |
| 540.00 | 1245.00 | 0.00666 | 2.45 |
| 560.00 | 540.00 | 0.00680 | 0.05 |
| 700.00 | 110.00 | 0.01030 | 0.000 |
| 800.00 | 114.00 | 0.01460 | 0.000 |
| 900.00 | 117.00 | 0.01460 | 0.000 |
| 1000.00 | 123.00 | 0.01630 | 0.000 |
| 1078.00 | 125.00 | 0.01603 | 0.000 |

SAMPLE CASE 11

Heat flux drive - OUTPUT OF INITIAL INPUT TABLES

LOCAL STATIC PRESSURE AND FLOW CONTROL TABLE

| TIME (SEC) | LOC PRESS (LBF/FT ²) | FLOW (LBF/MIN) | LOCAL STRESS | |
|---------------|-------------------------------------|-------------------|-----------------------|-----------------------|
| | | | (LBF/M ²) | (LBF/M ²) |
| 0.00 | 0.0360 | 1.0 | 0.0000 | 0.0000 |
| 40.00 | 1.7560 | 1.0 | 0.0006 | 0.0019 |
| 50.00 | 10.5000 | 1.0 | 0.0019 | 0.0048 |
| 60.00 | 66.0800 | 1.0 | 0.0048 | 0.0084 |
| 70.00 | 393.0000 | 1.0 | 0.0122 | 0.0122 |
| 80.00 | 512.8000 | 1.0 | 0.0131 | 0.0132 |
| 85.00 | 747.0000 | 1.0 | 0.0132 | 0.0127 |
| 90.03 | 1030.0000 | 1.0 | 0.0127 | 0.0125 |
| 95.00 | 920.0000 | 1.0 | 0.0125 | 0.0114 |
| 100.00 | 818.1000 | 1.0 | 0.0114 | 0.0095 |
| 105.00 | 755.0000 | 1.0 | 0.0095 | 0.0087 |
| 110.00 | 651.0000 | 1.0 | 0.0087 | 0.0077 |
| 115.00 | 549.0000 | 1.0 | 0.0077 | 0.0067 |
| 120.00 | 410.0000 | 1.0 | 0.0067 | 0.0056 |
| 130.00 | 349.0000 | 1.0 | 0.0056 | 0.0049 |
| 140.00 | 298.0000 | 1.0 | 0.0049 | 0.0042 |
| 150.00 | 259.0000 | 1.0 | 0.0042 | 0.0036 |
| 160.00 | 213.4000 | 1.0 | 0.0036 | 0.0032 |
| 170.00 | 156.0000 | 1.0 | 0.0032 | 0.0028 |
| 180.00 | 125.1000 | 1.0 | 0.0028 | 0.0024 |
| 190.00 | 96.8000 | 1.0 | 0.0024 | 0.0021 |
| 200.00 | 77.7000 | 1.0 | 0.0021 | 0.0018 |
| 210.00 | 64.2000 | 1.0 | 0.0018 | 0.0016 |
| 240.00 | 47.5000 | 1.0 | 0.0016 | 0.0014 |
| 300.00 | 36.3000 | 1.0 | 0.0014 | 0.0012 |
| 350.00 | 49.8000 | 1.0 | 0.0012 | 0.0010 |
| 370.00 | 61.5000 | 1.0 | 0.0010 | 0.0009 |
| 390.00 | 90.6000 | 1.0 | 0.0009 | 0.0008 |
| 410.00 | 147.0000 | 1.0 | 0.0008 | 0.0007 |
| 430.00 | 234.0000 | 1.0 | 0.0007 | 0.0006 |
| 450.00 | 364.0000 | 1.0 | 0.0006 | 0.0005 |
| 470.00 | 459.0000 | 1.0 | 0.0005 | 0.0004 |
| 480.00 | 496.0000 | 1.0 | 0.0004 | 0.0003 |
| 490.00 | 490.0000 | 1.0 | 0.0003 | 0.0002 |
| 510.00 | 411.0000 | 1.0 | 0.0002 | 0.0002 |
| 530.00 | 318.0000 | 1.0 | 0.0002 | 0.0001 |
| 550.00 | 247.0000 | 1.0 | 0.0001 | 0.0001 |
| 570.00 | 307.0000 | 1.0 | 0.0001 | 0.0001 |
| 706.00 | 734.0000 | 1.0 | 0.0012 | 0.0014 |
| 756.00 | 1114.9999 | 1.0 | 0.0014 | 0.0020 |
| 1076.00 | 2117.0000 | 1.0 | 0.0020 | 0.0020 |

MATERIALS

| MATERIAL NAME | THICKNESS (IN) | NUMBER OF NODES |
|---------------|-------------------|--------------------|
| (2) ALUMINUM | .0150 | 1 |
| (11) AVOCAI | 1.9760 | 35 |

MATERIAL PROPERTIES OF VIRGIN MATERIALS

MATERIAL (1)

| | FIRST REAC | SECOND REAC |
|------------------------------------|------------|-------------|
| ACTIVATION TEMPERATURE, DEG R | 23300.0 | 0 |
| COLLISION FREQUENCY, 1/SEC | .112090*05 | .000000 |
| REACTION ORDER | 1.0000 | 0 |
| HEAT OF DECOMPOSITION, BTU/LBM | 350.00 | |
| SPECIFIC HEAT, BTU/LBM-DEG R | .4100*0001 | .9936*0111* |
| CONDUCTIVITY, BTU-IN/FT2-SEC-DEG R | .4446*0514 | .4125*0117* |
| EMISSIVITY | .9000 | |
| ABSORPTIVITY | .9000 | |
| DENSITY, LBM/FT3 | .34*00 | |
| TRANSPERSION FACTOR (ABL GASES) | 1.2000 | |

MATERIAL (2)

| | FIRST REAC | SECOND REAC |
|------------------------------------|-------------|--------------|
| ACTIVATION TEMPERATURE, DEG R | 0 | 0 |
| COLLISION FREQUENCY, 1/SEC | .000000 | .000000 |
| REACTION ORDER | .0000 | 0 |
| HEAT OF DECOMPOSITION, BTU/LBM | 420.00 | |
| SPECIFIC HEAT, BTU/LBM-DEG R | .0000 | .51642*0411* |
| CONDUCTIVITY, BTU-IN/FT2-SEC-DEG R | .0153*0017* | .9610*0517* |
| EMISSIVITY | .2000 | |
| ABSORPTIVITY | .6000 | |
| DENSITY, LBM/FT3 | .48*00 | |
| TRANSPERSION FACTOR (ABL GASES) | .7000 | |

MATERIAL PROPERTIES OF THE CHAR

| | COMBUSTION REACTION | CHAR SUBLIMATION |
|-------------------------------|---------------------|------------------|
| ACTIVATION TEMPERATURE, DEG R | 3785.0 | 0 |
| COLLISION FREQUENCY, 1/SEC | .671000*09 | .000000 |
| REACTION ORDER | .5000 | 0 |
| HEAT OF COMBUSTION, BTU/LBM | | |
| HEAT OF SUBLIMATION, BTU/LBM | .00 | |
| EMISSIVITY | .6500 | |
| ABSORPTIVITY | .6000 | |
| DENSITY, LBM/FT3 | .00 | |

| | |
|---|-----------|
| TRANSPERSION FACTOR (CHAR GASES) | 1.0000 |
| DENSITY OF THE CARBON IN CHAR, LB/M/FT ³ | 12.00 |
| ABALATION GAS PROPERTIES | |
| SPECIFIC HEAT, BTU/LB-DEG R | .7660-001 |
| HEAT OF GAS COMBUSTION, BTU/LBM | 6173.00 |

OTHER CONSTANTS

| | |
|---|------------|
| THEORETICAL CARBON DENSITY, LB/M/FT ³ | 131.00 |
| THEORETICAL VIRGIN DENSITY, LB/M/FT ³ | 70.00 |
| THEORETICAL SILICA DENSITY, LB/M/FT ³ | 137.30 |
| REFERENCE VISCOSITY PENMEABILITY, FT ² | .7500 |
| REFERENCE INERTIAL PERMEABILITY, FT ² | .100000-09 |
| REFERENCE VISCOSITY, LB/FT-SEC | .100000-04 |
| REFERENCE TEMPERATURE FOR VISC., R | 630.00 |
| SURFACE DIFFUSION CONSTANT, FT ² /SEC | .100000-01 |
| CARBON MONOXIDE DEPOSITION GAS (EXCEPT HYDROGEN) | .100000-01 |
| NITROGEN | .100000-01 |
| OXYGEN | .100000-01 |
| METHANE | .100000-01 |
| SILICON MONOXIDE | .100000-01 |

BLODING PARAMETER
 DIFFUSION REDUCTION PARAMETER
 HEAT OF REACTION, SIO₂-C, BTU/LBM
 HEAT OF REACTION, C DEPOSITION, BTU/LBM

$\alpha = -0.6490-001 + (-0.2540-001)ETA + (-0.2300-001)ETA^2 + (-0.8750-001)ETA^3$

SILICA-CARBON REACTION CONSTANTS
 ACTIVATION TEMPERATURE, DEG R
 COLLISION FREQUENCY, 1/SEC
 REACTION ORDER

CARBON DEPOSITION REACTION CONSTANTS

| | |
|--------------|---------------|
| LOW HYDROGEN | HIGH HYDROGEN |
| .345000-01 | .600000-03 |
| .116200-03 | .114000-01 |
| .577700-04 | .422000-01 |

SAMPLE CASE 11

Heat flux drive - OUTPUT OF CALCULATED DATA AT VARIOUS TIMES

The following listing shows the CHAD program output at time = 0, 100, 200, and 500 seconds.

TIME = .00 TOTAL ILLUSTRATIONS

| NODE | DISTANCE FROM BACK (IN) | TEMP (DEG F) | CONDUCTED HEAT FLUX (BTU/FT2-SEC) | | | TOTAL DECOMP CARBON | | | DENSITIES (LBH/FT3) | | | INTERNAL PRESSURE (LBF/FT2) | | | MUL AT VELCITY (FT/SEC) | | |
|------|-------------------------|--------------|-----------------------------------|---------|-----------|---------------------|---------|----------|---------------------|-----------|--------|-----------------------------|-------|-------|-------------------------|--|--|
| | | | INT COHE | SINC | PYRO DEPO | INT COHE | OXYGEN | NITROGEN | HYDROGEN | PYRO DEPO | SIC | BURN | TOTAL | | | | |
| 37 | 1.9910 | 100.31 | - | - | .0000 | 34.0000 | 14.0000 | 10.0000 | .0000 | 10.0000 | .0000 | 20.000 | .0000 | .0000 | .0000 | | |
| 36 | 1.9769 | 100.31 | 0.000 | 34.0000 | 14.0000 | 10.0000 | 0.000 | 0.000 | 10.0000 | 0.000 | 20.000 | .0000 | .0000 | .0000 | | | |
| 36 | 1.9628 | 100.31 | 0.000 | 34.0000 | 14.0000 | 10.0000 | 0.000 | 0.000 | 10.0000 | 0.000 | 20.000 | .0000 | .0000 | .0000 | | | |
| 36 | 1.9487 | 100.31 | 0.000 | 34.0000 | 14.0000 | 10.0000 | 0.000 | 0.000 | 10.0000 | 0.000 | 20.000 | .0000 | .0000 | .0000 | | | |
| 36 | 1.9345 | 100.31 | 0.000 | 34.0000 | 14.0000 | 10.0000 | 0.000 | 0.000 | 10.0000 | 0.000 | 20.000 | .0000 | .0000 | .0000 | | | |
| 35 | 1.9201 | 100.31 | .0000 | 34.0000 | 14.0000 | 10.0000 | 0.000 | 0.000 | 10.0000 | 0.000 | 20.000 | .0000 | .0000 | .0000 | | | |
| 34 | 1.8216 | 100.31 | .0000 | 34.0000 | 14.0000 | 10.0000 | 0.000 | 0.000 | 10.0000 | 0.000 | 20.000 | .0000 | .0000 | .0000 | | | |
| 33 | 1.7652 | 100.31 | .0000 | 34.0000 | 14.0000 | 10.0000 | 0.000 | 0.000 | 10.0000 | 0.000 | 20.000 | .0000 | .0000 | .0000 | | | |
| 32 | 1.7087 | 100.31 | .0000 | 34.0000 | 14.0000 | 10.0000 | 0.000 | 0.000 | 10.0000 | 0.000 | 20.000 | .0000 | .0000 | .0000 | | | |
| 31 | 1.6523 | 100.31 | .0000 | 34.0000 | 14.0000 | 10.0000 | 0.000 | 0.000 | 10.0000 | 0.000 | 20.000 | .0000 | .0000 | .0000 | | | |
| 30 | 1.5958 | 100.31 | .0000 | 34.0000 | 14.0000 | 10.0000 | 0.000 | 0.000 | 10.0000 | 0.000 | 20.000 | .0000 | .0000 | .0000 | | | |
| 29 | 1.5393 | 100.31 | .0000 | 34.0000 | 14.0000 | 10.0000 | 0.000 | 0.000 | 10.0000 | 0.000 | 20.000 | .0000 | .0000 | .0000 | | | |
| 28 | 1.4829 | 100.31 | .0000 | 34.0000 | 14.0000 | 10.0000 | 0.000 | 0.000 | 10.0000 | 0.000 | 20.000 | .0000 | .0000 | .0000 | | | |
| 27 | 1.4264 | 100.31 | .0000 | 34.0000 | 14.0000 | 10.0000 | 0.000 | 0.000 | 10.0000 | 0.000 | 20.000 | .0000 | .0000 | .0000 | | | |
| 26 | 1.3700 | 100.31 | .0000 | 34.0000 | 14.0000 | 10.0000 | 0.000 | 0.000 | 10.0000 | 0.000 | 20.000 | .0000 | .0000 | .0000 | | | |
| 25 | 1.3135 | 100.31 | .0000 | 34.0000 | 14.0000 | 10.0000 | 0.000 | 0.000 | 10.0000 | 0.000 | 20.000 | .0000 | .0000 | .0000 | | | |
| 24 | 1.2571 | 100.31 | .0000 | 34.0000 | 14.0000 | 10.0000 | 0.000 | 0.000 | 10.0000 | 0.000 | 20.000 | .0000 | .0000 | .0000 | | | |
| 23 | 1.2006 | 100.31 | .0000 | 34.0000 | 14.0000 | 10.0000 | 0.000 | 0.000 | 10.0000 | 0.000 | 20.000 | .0000 | .0000 | .0000 | | | |
| 22 | 1.1441 | 100.31 | .0000 | 34.0000 | 14.0000 | 10.0000 | 0.000 | 0.000 | 10.0000 | 0.000 | 20.000 | .0000 | .0000 | .0000 | | | |
| 21 | 1.0877 | 100.31 | .0000 | 34.0000 | 14.0000 | 10.0000 | 0.000 | 0.000 | 10.0000 | 0.000 | 20.000 | .0000 | .0000 | .0000 | | | |
| 20 | 1.0312 | 100.31 | .0000 | 34.0000 | 14.0000 | 10.0000 | 0.000 | 0.000 | 10.0000 | 0.000 | 20.000 | .0000 | .0000 | .0000 | | | |
| 19 | .9748 | 100.31 | .0000 | 34.0000 | 14.0000 | 10.0000 | 0.000 | 0.000 | 10.0000 | 0.000 | 20.000 | .0000 | .0000 | .0000 | | | |
| 18 | .9183 | 100.31 | .0000 | 34.0000 | 14.0000 | 10.0000 | 0.000 | 0.000 | 10.0000 | 0.000 | 20.000 | .0000 | .0000 | .0000 | | | |
| 17 | .8619 | 100.31 | .0000 | 34.0000 | 14.0000 | 10.0000 | 0.000 | 0.000 | 10.0000 | 0.000 | 20.000 | .0000 | .0000 | .0000 | | | |
| 16 | .8054 | 100.31 | .0000 | 34.0000 | 14.0000 | 10.0000 | 0.000 | 0.000 | 10.0000 | 0.000 | 20.000 | .0000 | .0000 | .0000 | | | |
| 15 | .7489 | 100.31 | .0000 | 34.0000 | 14.0000 | 10.0000 | 0.000 | 0.000 | 10.0000 | 0.000 | 20.000 | .0000 | .0000 | .0000 | | | |
| 14 | .6925 | 100.31 | .0000 | 34.0000 | 14.0000 | 10.0000 | 0.000 | 0.000 | 10.0000 | 0.000 | 20.000 | .0000 | .0000 | .0000 | | | |
| 13 | .6360 | 100.31 | .0000 | 34.0000 | 14.0000 | 10.0000 | 0.000 | 0.000 | 10.0000 | 0.000 | 20.000 | .0000 | .0000 | .0000 | | | |
| 12 | .5795 | 100.31 | .0000 | 34.0000 | 14.0000 | 10.0000 | 0.000 | 0.000 | 10.0000 | 0.000 | 20.000 | .0000 | .0000 | .0000 | | | |
| 11 | .5231 | 100.31 | .0000 | 34.0000 | 14.0000 | 10.0000 | 0.000 | 0.000 | 10.0000 | 0.000 | 20.000 | .0000 | .0000 | .0000 | | | |
| 10 | .4667 | 100.31 | .0000 | 34.0000 | 14.0000 | 10.0000 | 0.000 | 0.000 | 10.0000 | 0.000 | 20.000 | .0000 | .0000 | .0000 | | | |
| 9 | .4102 | 100.31 | .0000 | 34.0000 | 14.0000 | 10.0000 | 0.000 | 0.000 | 10.0000 | 0.000 | 20.000 | .0000 | .0000 | .0000 | | | |
| 8 | .3537 | 100.31 | .0000 | 34.0000 | 14.0000 | 10.0000 | 0.000 | 0.000 | 10.0000 | 0.000 | 20.000 | .0000 | .0000 | .0000 | | | |
| 7 | .2973 | 100.31 | .0000 | 34.0000 | 14.0000 | 10.0000 | 0.000 | 0.000 | 10.0000 | 0.000 | 20.000 | .0000 | .0000 | .0000 | | | |
| 6 | .2408 | 100.31 | .0000 | 34.0000 | 14.0000 | 10.0000 | 0.000 | 0.000 | 10.0000 | 0.000 | 20.000 | .0000 | .0000 | .0000 | | | |
| 5 | .1844 | 100.31 | .0000 | 34.0000 | 14.0000 | 10.0000 | 0.000 | 0.000 | 10.0000 | 0.000 | 20.000 | .0000 | .0000 | .0000 | | | |
| 4 | .1279 | 100.31 | .0000 | 34.0000 | 14.0000 | 10.0000 | 0.000 | 0.000 | 10.0000 | 0.000 | 20.000 | .0000 | .0000 | .0000 | | | |
| 3 | .0715 | 100.31 | .0000 | 34.0000 | 14.0000 | 10.0000 | 0.000 | 0.000 | 10.0000 | 0.000 | 20.000 | .0000 | .0000 | .0000 | | | |
| 2 | .0150 | 100.31 | .0000 | 34.0000 | 14.0000 | 10.0000 | 0.000 | 0.000 | 10.0000 | 0.000 | 20.000 | .0000 | .0000 | .0000 | | | |
| 1 | .0000 | 100.31 | .0000 | 34.0000 | 14.0000 | 10.0000 | 0.000 | 0.000 | 10.0000 | 0.000 | 20.000 | .0000 | .0000 | .0000 | | | |

GAS FLOW RATE(F1/F2-SEC) SOURCES AND SINKS (LB/NODE-SEC)

| | | | | | | | | | | | | | | | |
|----|----------|--------|-----|-----|-----|-----|-----|-----|-----|-----|-----|------|------|------|------|
| 37 | .1527-1 | .19-15 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .000 | .000 | .000 | .000 |
| 36 | .1336-14 | .38-15 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .000 | .000 | .000 | .000 |
| 36 | .9544-15 | .38-15 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .000 | .000 | .000 | .000 |
| 36 | .5726-15 | .38-15 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .000 | .000 | .000 | .000 |
| 36 | .1909-15 | .19-15 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .000 | .000 | .000 | .000 |
| 35 | .0000 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .000 | .000 | .000 | .000 |

INTERNAL PRESSURE (LBF/FT2) CONCENTRATIONS (LBM/FT3 VOID)

| | | | | | | | | | | | | | | | |
|----|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 37 | .16000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 |
| 36 | .16000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 |
| 36 | .16000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 |
| 36 | .16000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 |
| 36 | .16000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 |
| 36 | .16000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 |
| 36 | .16000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 |
| 36 | .16000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 |
| 36 | .16000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 | .36000-01 |

t = 0

113-10141-100-00

| NODE | | DISTANCE FROM BACK (IN) | | CONDUCTED HEAT FLUX (BTU/FT ² -SEC) | | DENSITIES (LBM/FT ³) | | | INTERNAL PRESSURE (LBF/FT ²) | | | CONCENTRATIONS--SOURCES AND SINKS-- | | | GAS FLOW RATE (LBM/FT ² -SEC) | | |
|------|--------------|-------------------------|--------------|--|----------|----------------------------------|---------|---------|--|------|---------|-------------------------------------|---------|--------|--|---------|--------|
| NUDE | TEMP (DEG F) | TEMP (DEG F) | TEMP (DEG F) | TOTAL DECOMP | CARBON | GRAPHITE | SILICA | | | | | | | | | | |
| 37 | 1996.3 | 4336.85 | 23.7554 | 14.6032 | *0.0066 | 12.7420 | *0.0000 | 1.8432 | *0.2216 | 0.3 | 20.011 | *2.1511 | *0.0000 | 1.9732 | *2.1625 | *0.0000 | 1.9445 |
| 36 | 1958.4 | 4245.00 | 21.3168 | 17.0705 | *0.0000 | 14.4805 | *0.0000 | 2.0900 | *0.2226 | *0.1 | 19.732 | *2.1625 | *0.0000 | 1.9445 | *2.0559 | *0.0000 | 1.9153 |
| 35 | 1950.4 | 4149.42 | 23.3274 | 19.8252 | *0.0000 | 16.2775 | *0.0000 | 3.4550 | *0.2236 | 0.3 | 19.445 | *2.1625 | *0.0000 | 1.9153 | *1.9463 | *0.0000 | 1.8874 |
| 34 | 1949.6 | 4057.65 | 23.5552 | 20.9745 | *0.0000 | 16.6152 | *0.0000 | 5.2650 | *0.2245 | 0.3 | 19.153 | *2.1625 | *0.0000 | 1.8874 | *1.9463 | *0.0000 | 1.8683 |
| 33 | 1947.2 | 4057.65 | 22.7923 | 16.1255 | *0.0000 | 10.605 | *0.0000 | 6.0700 | *0.2254 | 0.3 | 18.874 | *2.1625 | *0.0000 | 1.8683 | *1.9463 | *0.0000 | 1.8503 |
| 32 | 1934.5 | 3965.63 | 22.7923 | 16.1255 | *0.0000 | 10.605 | *0.0000 | 6.0700 | *0.2263 | 0.3 | 18.593 | *2.1625 | *0.0000 | 1.8503 | *1.9463 | *0.0000 | 1.8423 |
| 31 | 1934.5 | 3965.63 | 21.5333 | 24.1026 | *0.0000 | 15.2006 | *0.0000 | 6.0700 | *0.2272 | 0.3 | 18.313 | *2.1625 | *0.0000 | 1.8423 | *1.9463 | *0.0000 | 1.8343 |
| 30 | 1878.1 | 3420.63 | 2933.56 | 1.9588 | *0.0000 | 23.5850 | *0.0000 | 9.8390 | *0.2281 | 0.3 | 17.702 | *2.1625 | *0.0000 | 1.8343 | *1.9463 | *0.0000 | 1.8263 |
| 29 | 1821.6 | 3420.63 | 2933.56 | 1.9588 | *0.0000 | 13.7459 | *0.0000 | 10.0000 | *0.2290 | 0.3 | 17.422 | *2.1625 | *0.0000 | 1.8263 | *1.9463 | *0.0000 | 1.8183 |
| 28 | 1765.2 | 2430.21 | 1.6070 | 20.1588 | *0.588 | 1.588 | *0.0000 | 10.0000 | *0.2309 | 0.3 | 17.327 | *2.1625 | *0.0000 | 1.8183 | *1.9463 | *0.0000 | 1.8103 |
| 27 | 1755.1 | 2292.84 | 1.7359 | 20.0000 | *0.0000 | 10.0000 | *0.0000 | 10.0000 | *0.2318 | 0.3 | 17.1907 | *2.1625 | *0.0000 | 1.8103 | *1.9463 | *0.0000 | 1.8023 |
| 26 | 1736.4 | 2147.04 | 1.6550 | 20.0000 | *0.0000 | 10.0000 | *0.0000 | 10.0000 | *0.2327 | 0.3 | 17.0927 | *2.1625 | *0.0000 | 1.8023 | *1.9463 | *0.0000 | 1.7943 |
| 25 | 1722.6 | 1959.87 | 1.5661 | 20.0000 | *0.0000 | 10.0000 | *0.0000 | 10.0000 | *0.2336 | 0.3 | 16.9843 | *2.1625 | *0.0000 | 1.7943 | *1.9463 | *0.0000 | 1.7863 |
| 24 | 1708.7 | 1803.71 | 1.26184 | 21.6196 | *1.6196 | 1.6196 | *0.0000 | 10.0000 | *0.2345 | 0.3 | 16.8963 | *2.1625 | *0.0000 | 1.7863 | *1.9463 | *0.0000 | 1.7783 |
| 23 | 1694.6 | 1459.86 | 7.1621 | 32.2143 | *12.2143 | 12.2143 | *0.0000 | 10.0000 | *0.2354 | 0.3 | 16.7983 | *2.1625 | *0.0000 | 1.7783 | *1.9463 | *0.0000 | 1.7703 |
| 22 | 1680.5 | 803.22 | 3.5660 | 33.9976 | *13.9976 | 13.9976 | *0.0000 | 10.0000 | *0.2363 | 0.3 | 16.6903 | *2.1625 | *0.0000 | 1.7703 | *1.9463 | *0.0000 | 1.7623 |
| 21 | 1666.4 | 4944.50 | 1.7075 | 34.0000 | *14.0000 | 14.0000 | *0.0000 | 10.0000 | *0.2372 | 0.3 | 16.5823 | *2.1625 | *0.0000 | 1.7623 | *1.9463 | *0.0000 | 1.7543 |
| 20 | 1652.3 | 264.20 | 3.412 | 34.0000 | *14.0000 | 14.0000 | *0.0000 | 10.0000 | *0.2381 | 0.3 | 16.4743 | *2.1625 | *0.0000 | 1.7543 | *1.9463 | *0.0000 | 1.7463 |
| 19 | 1595.6 | 125.98 | 0.529 | 34.0000 | *14.0000 | 14.0000 | *0.0000 | 10.0000 | *0.2390 | 0.3 | 16.3663 | *2.1625 | *0.0000 | 1.7463 | *1.9463 | *0.0000 | 1.7383 |
| 18 | 1539.3 | 104.51 | 0.084 | 34.0000 | *14.0000 | 14.0000 | *0.0000 | 10.0000 | *0.2409 | 0.3 | 16.2583 | *2.1625 | *0.0000 | 1.7383 | *1.9463 | *0.0000 | 1.7303 |
| 17 | 1482.9 | 101.02 | 0.014 | 34.0000 | *14.0000 | 14.0000 | *0.0000 | 10.0000 | *0.2418 | 0.3 | 16.1503 | *2.1625 | *0.0000 | 1.7303 | *1.9463 | *0.0000 | 1.7223 |
| 16 | 1426.4 | 100.43 | 0.003 | 34.0000 | *14.0000 | 14.0000 | *0.0000 | 10.0000 | *0.2427 | 0.3 | 16.0423 | *2.1625 | *0.0000 | 1.7223 | *1.9463 | *0.0000 | 1.7143 |
| 15 | 1370.0 | 160.33 | 0.000 | 34.0000 | *14.0000 | 14.0000 | *0.0000 | 10.0000 | *0.2436 | 0.3 | 15.9343 | *2.1625 | *0.0000 | 1.7143 | *1.9463 | *0.0000 | 1.7063 |
| 14 | 1313.5 | 100.30 | 0.000 | 34.0000 | *14.0000 | 14.0000 | *0.0000 | 10.0000 | *0.2445 | 0.3 | 15.8263 | *2.1625 | *0.0000 | 1.7063 | *1.9463 | *0.0000 | 1.6983 |
| 13 | 1257.1 | 100.30 | 0.000 | 34.0000 | *14.0000 | 14.0000 | *0.0000 | 10.0000 | *0.2454 | 0.3 | 15.7183 | *2.1625 | *0.0000 | 1.6983 | *1.9463 | *0.0000 | 1.6903 |
| 12 | 1200.6 | 100.30 | 0.000 | 34.0000 | *14.0000 | 14.0000 | *0.0000 | 10.0000 | *0.2463 | 0.3 | 15.6103 | *2.1625 | *0.0000 | 1.6903 | *1.9463 | *0.0000 | 1.6823 |
| 11 | 1144.1 | 100.30 | 0.000 | 34.0000 | *14.0000 | 14.0000 | *0.0000 | 10.0000 | *0.2472 | 0.3 | 15.5023 | *2.1625 | *0.0000 | 1.6823 | *1.9463 | *0.0000 | 1.6743 |
| 10 | 1087.7 | 100.30 | 0.000 | 34.0000 | *14.0000 | 14.0000 | *0.0000 | 10.0000 | *0.2481 | 0.3 | 15.3943 | *2.1625 | *0.0000 | 1.6743 | *1.9463 | *0.0000 | 1.6663 |
| 9 | 1031.2 | 100.30 | 0.000 | 34.0000 | *14.0000 | 14.0000 | *0.0000 | 10.0000 | *0.2490 | 0.3 | 15.2863 | *2.1625 | *0.0000 | 1.6663 | *1.9463 | *0.0000 | 1.6583 |
| 8 | 974.6 | 100.30 | 0.000 | 34.0000 | *14.0000 | 14.0000 | *0.0000 | 10.0000 | *0.2509 | 0.3 | 15.1783 | *2.1625 | *0.0000 | 1.6583 | *1.9463 | *0.0000 | 1.6503 |
| 7 | 918.3 | 100.30 | 0.000 | 34.0000 | *14.0000 | 14.0000 | *0.0000 | 10.0000 | *0.2518 | 0.3 | 15.0703 | *2.1625 | *0.0000 | 1.6503 | *1.9463 | *0.0000 | 1.6423 |
| 6 | 861.9 | 100.30 | 0.000 | 34.0000 | *14.0000 | 14.0000 | *0.0000 | 10.0000 | *0.2527 | 0.3 | 14.9623 | *2.1625 | *0.0000 | 1.6423 | *1.9463 | *0.0000 | 1.6343 |
| 5 | 805.4 | 100.30 | 0.000 | 34.0000 | *14.0000 | 14.0000 | *0.0000 | 10.0000 | *0.2536 | 0.3 | 14.8543 | *2.1625 | *0.0000 | 1.6343 | *1.9463 | *0.0000 | 1.6263 |
| 4 | 748.7 | 100.30 | 0.000 | 34.0000 | *14.0000 | 14.0000 | *0.0000 | 10.0000 | *0.2545 | 0.3 | 14.7463 | *2.1625 | *0.0000 | 1.6263 | *1.9463 | *0.0000 | 1.6183 |
| 3 | 692.5 | 100.30 | 0.000 | 34.0000 | *14.0000 | 14.0000 | *0.0000 | 10.0000 | *0.2554 | 0.3 | 14.6383 | *2.1625 | *0.0000 | 1.6183 | *1.9463 | *0.0000 | 1.6103 |
| 2 | 636.0 | 100.30 | 0.000 | 34.0000 | *14.0000 | 14.0000 | *0.0000 | 10.0000 | *0.2563 | 0.3 | 14.5303 | *2.1625 | *0.0000 | 1.6103 | *1.9463 | *0.0000 | 1.6023 |
| 1 | 580.0 | 100.30 | 0.000 | 34.0000 | *14.0000 | 14.0000 | *0.0000 | 10.0000 | *0.2572 | 0.3 | 14.4223 | *2.1625 | *0.0000 | 1.6023 | *1.9463 | *0.0000 | 1.5943 |

| | | | | | | | | | | |
|----|----------|----------|-----|--------|---------|---------|----------|----------|----------|----------|
| 37 | .9296-02 | .4258-02 | .00 | .39-04 | .104-03 | .137-03 | *.000 | *.191-03 | *.001-03 | *.334-02 |
| 36 | .4166-02 | .00 | .00 | .10-03 | .109-03 | .150-02 | *.151-02 | *.110-02 | *.110-02 | .335-02 |
| 34 | .4063-02 | .00 | .00 | .11-03 | .114-03 | .132-02 | *.132-02 | *.120-02 | *.120-02 | .336-02 |
| 34 | .3954-02 | .00 | .00 | .14-03 | .119-03 | .124-02 | *.124-02 | *.120-03 | *.120-03 | .338-02 |
| 35 | .3517-02 | .00 | .00 | .35-03 | .126-03 | .116-02 | *.116-02 | *.120-03 | *.120-03 | .340-02 |
| 34 | .3208-02 | .00 | .00 | .11-02 | .124-03 | .198-03 | *.198-03 | *.167-03 | *.167-03 | .341-02 |
| 33 | .4281-02 | .00 | .00 | .00 | .666-04 | .537-03 | *.215-03 | *.386-03 | *.386-03 | .346-02 |
| 32 | .4281-02 | .00 | .00 | .00 | .513-04 | .283-03 | *.139-03 | *.138-02 | *.138-02 | .467-02 |
| 32 | .4281-02 | .00 | .00 | .00 | .398-04 | .245-03 | *.121-03 | *.164-02 | *.164-02 | .499-02 |
| 32 | .4281-02 | .00 | .00 | .00 | .303-04 | .218-03 | *.105-03 | *.169-02 | *.169-02 | .537-02 |
| 32 | .4281-02 | .00 | .00 | .00 | .00 | .00 | *.902-04 | *.216-02 | *.216-02 | .562-02 |
| 31 | .4281-02 | .00 | .00 | .23-02 | .00 | .00 | *.201-03 | *.216-02 | *.216-02 | .639-02 |
| 31 | .1984-02 | .00 | .00 | .20-02 | .00 | .00 | *.198-04 | *.248-03 | *.248-03 | .647-02 |
| 31 | .3564-05 | .00 | .00 | .36-05 | .00 | .00 | *.197-04 | *.248-02 | *.248-02 | .649-02 |
| 31 | .2103-06 | .00 | .00 | .21-06 | .00 | .00 | *.197-04 | *.248-02 | *.248-02 | .650-02 |
| 31 | .0000 | .00 | .00 | .00 | .00 | .00 | *.197-04 | *.248-02 | *.248-02 | .650-02 |
| 30 | .0000 | .00 | .00 | .00 | .00 | .00 | *.197-04 | *.248-02 | *.248-02 | .650-02 |
| 29 | .0000 | .00 | .00 | .00 | .00 | .00 | *.197-04 | *.248-02 | *.248-02 | .650-02 |
| 28 | .0000 | .00 | .00 | .00 | .00 | .00 | *.197-04 | *.248-02 | *.248-02 | .650-02 |
| 27 | .0000 | .00 | .00 | .00 | .00 | .00 | *.197-04 | *.248-02 | *.248-02 | .650-02 |
| 26 | .0000 | .00 | .00 | .00 | .00 | .00 | *.197-04 | *.248-02 | *.248-02 | .650-02 |
| 25 | .0000 | .00 | .00 | .00 | .00 | .00 | *.197-04 | *.248-02 | *.248-02 | .650-02 |
| 24 | .0000 | .00 | .00 | .00 | .00 | .00 | *.197-04 | *.248-02 | *.248-02 | .650-02 |
| 23 | .0000 | .00 | .00 | .00 | .00 | .00 | *.197-04 | *.248-02 | *.248-02 | .650-02 |
| 22 | .0000 | .00 | .00 | .00 | .00 | .00 | *.197-04 | *.248-02 | *.248-02 | .650-02 |
| 21 | .0000 | .00 | .00 | .00 | .00 | .00 | *.197-04 | *.248-02 | *.248-02 | .650-02 |
| 20 | .0000 | .00 | .00 | .00 | .00 | .00 | *.197-04 | *.248-02 | *.248-02 | .650-02 |
| 19 | .0000 | .00 | .00 | .00 | .00 | .00 | *.197-04 | *.248-02 | *.248-02 | .650-02 |
| 18 | .0000 | .00 | .00 | .00 | .00 | .00 | *.197-04 | *.248-02 | *.248-02 | .650-02 |
| 17 | .0000 | .00 | .00 | .00 | .00 | .00 | *.197-04 | *.248-02 | *.248-02 | .650-02 |
| 16 | .0000 | .00 | .00 | .00 | .00 | .00 | *.197-04 | *.248-02 | *.248-02 | .650-02 |
| 15 | .0000 | .00 | .00 | .00 | .00 | .00 | *.197-04 | *.248-02 | *.248-02 | .650-02 |
| 14 | .0000 | .00 | .00 | .00 | .00 | .00 | *.197-04 | *.248-02 | *.248-02 | .650-02 |
| 13 | .0000 | .00 | .00 | .00 | .00 | .00 | *.197-04 | *.248-02 | *.248-02 | .650-02 |
| 12 | .0000 | .00 | .00 | .00 | .00 | .00 | *.197-04 | *.248-02 | *.248-02 | .650-02 |
| 11 | .0000 | .00 | .00 | .00 | .00 | .00 | *.197-04 | *.248-02 | *.248-02 | .650-02 |
| 10 | .0000 | .00 | .00 | .00 | .00 | .00 | *.197-04 | *.248-02 | *.248-02 | .650-02 |
| 9 | .0000 | .00 | .00 | .00 | .00 | .00 | *.197-04 | *.248-02 | *.248-02 | .650-02 |
| 8 | .0000 | .00 | .00 | .00 | .00 | .00 | *.197-04 | *.248-02 | *.248-02 | .650-02 |
| 7 | .0000 | .00 | .00 | .00 | .00 | .00 | *.197-04 | *.248-02 | *.248-02 | .650-02 |
| 6 | .0000 | .00 | .00 | .00 | .00 | .00 | *.197-04 | *.248-02 | *.248-02 | .650-02 |
| 5 | .0000 | .00 | .00 | .00 | .00 | .00 | *.197-04 | *.248-02 | *.248-02 | .650-02 |
| 4 | .0000 | .00 | .00 | .00 | .00 | .00 | *.197-04 | *.248-02 | *.248-02 | .650-02 |
| 3 | .0000 | .00 | .00 | .00 | .00 | .00 | *.197-04 | *.248-02 | *.248-02 | .650-02 |
| 2 | .0000 | .00 | .00 | .00 | .00 | .00 | *.197-04 | *.248-02 | *.248-02 | .650-02 |
| | .0000 | .00 | .00 | .00 | .00 | .00 | *.197-04 | *.248-02 | *.248-02 | .650-02 |

TIME = 200.00 TOTAL ITERATIONS = 755

| NODE | DISTANCE FROM BACK (IN) | TEMP (DEG F) | CONDUCED HEAT FLUX (BTU/FT ² -SEC) | DECOMP | | | DENSITIES (LB/FT ³) | | | INTERNAL PRESSURE (LB/FT ²) | | | MOL AT | VELOCITY (IFT/SEC) |
|------|-------------------------|--------------|---|----------|----------|----------|---------------------------------|---------|-------------|---|------------|---------|---------|--------------------|
| | | | | TOTAL | CARBON | GRAPHITE | SILICA | | | | | | | |
| 36 | 1.9354 | -2651.75 | - | 3.4510 | - | 1.65926 | - | 0.0000 | - | 13.9537 | - | 2.63309 | 1.9.400 | .34200+01 |
| 35 | 1.9210 | 2429.47 | 3.2135 | 17.1729 | *0.0000 | 13.5253 | *0.0000 | 3.6471 | *0.79857+02 | 1.9.361 | *1.4425+01 | 1.9.400 | 1.9.400 | 1.9.400 |
| 35 | 1.9067 | 2603.49 | 3.5579 | 17.4830 | *0.0000 | 12.7971 | *0.0000 | 4.6859 | *0.0105+02 | 1.9.121 | *1.4489+01 | 1.9.400 | 1.9.400 | 1.9.400 |
| 35 | 1.8924 | 2578.62 | 3.5952 | 19.6921 | *0.0000 | 13.9537 | *0.0000 | 5.7384 | *0.0447+02 | 1.8.885 | *1.5068+01 | 1.9.400 | 1.9.400 | 1.9.400 |
| 35 | 1.8781 | 2553.03 | 3.7676 | 21.7462 | *0.0000 | 14.9016 | *0.0000 | 6.3446 | *0.0898+02 | 1.8.449 | *1.5556+01 | 1.9.400 | 1.9.400 | 1.9.400 |
| 34 | 1.86216 | 2446.09 | 4.1042 | 27.6070 | *0.0000 | 18.6977 | *0.0000 | 8.9092 | *0.4585 | 1.7.778 | *1.6019+01 | 1.9.400 | 1.9.400 | 1.9.400 |
| 33 | 1.7652 | 2323.26 | 4.2993 | 23.9400 | - | 14.2817 | *0.0000 | 9.6783 | *0.6997+ | 1.7.004 | *1.3495+01 | 1.9.400 | 1.9.400 | 1.9.400 |
| 32 | 1.7087 | 2183.03 | 4.3823 | 23.6396 | *0.0000 | 13.7206 | *0.0000 | 9.9191 | *0.9336+02 | 1.6.389 | *1.3211+01 | 1.9.400 | 1.9.400 | 1.9.400 |
| 31 | 1.66523 | 2022.40 | 4.3432 | 20.6864 | *0.0000 | 10.7027 | *0.0000 | 9.9837 | *0.1250+02 | 1.6.562 | *1.3519+01 | 1.9.400 | 1.9.400 | 1.9.400 |
| 30 | 1.5754 | 1836.00 | 4.1972 | 20.0354 | *0.0000 | 10.0376 | *0.0000 | 9.9978 | *0.1026+02 | 1.7.134 | *1.3548+01 | 1.9.400 | 1.9.400 | 1.9.400 |
| 29 | 1.5393 | 1610.84 | 3.9952 | 20.0001 | *0.0001 | 10.0000 | *0.0000 | 10.0000 | *0.0569+03 | 1.7.973 | *1.3046+01 | 1.9.400 | 1.9.400 | 1.9.400 |
| 28 | 1.5252 | 1545.74 | 3.9459 | 20.0000 | *0.0000 | 10.0000 | *0.0000 | 10.0000 | *0.0854+03 | 1.6.255 | *1.2620+01 | 1.9.400 | 1.9.400 | 1.9.400 |
| 28 | 1.5111 | 1472.76 | 3.4552 | 21.1280 | - | 1.1280 | *0.0000 | 10.0000 | *0.0000 | 1.1219 | *1.5454+01 | 1.9.400 | 1.9.400 | 1.9.400 |
| 28 | 1.4970 | 1376.64 | 3.0220 | 25.9374 | 5.9376 | 10.0000 | *0.0000 | 10.0000 | *0.1895+03 | 1.6.828 | *1.2019+01 | 1.9.400 | 1.9.400 | 1.9.400 |
| 28 | 1.4829 | 1212.70 | 3.1689 | 32.0998 | 12.0998 | 10.0000 | *0.0000 | 10.0000 | *0.2406+03 | 1.6.790 | *1.6423+00 | 1.9.400 | 1.9.400 | 1.9.400 |
| 27 | 1.4688 | 957.74 | 1.7851 | 33.6726 | 13.6728 | 10.0000 | *0.0000 | 10.0000 | *0.2448+03 | 1.6.799 | *1.6155+01 | 1.9.400 | 1.9.400 | 1.9.400 |
| 27 | 1.4547 | 738.51 | 1.3251 | 33.9942 | 13.9942 | 10.0000 | *0.0000 | 10.0000 | *0.2449+03 | 1.9.001 | *1.6566+02 | 1.9.400 | 1.9.400 | 1.9.400 |
| 27 | 1.4405 | 574.92 | .9637 | 33.9997 | 13.9997 | 10.0000 | *0.0000 | 10.0000 | *0.2450+03 | 1.9.001 | *1.6334+02 | 1.9.400 | 1.9.400 | 1.9.400 |
| 27 | 1.4264 | 455.83 | .4631 | 34.0000 | 14.0000 | 10.0000 | *0.0000 | 10.0000 | *0.2450+03 | 1.9.001 | *1.4519+02 | 1.9.400 | 1.9.400 | 1.9.400 |
| 26 | 1.3700 | 226.87 | .1717 | 34.0000 | 14.0000 | 10.0000 | *0.0000 | 10.0000 | *0.2450+03 | 1.9.001 | *1.0000 | 1.9.400 | 1.9.400 | 1.9.400 |
| 25 | 1.3135 | 141.88 | .0584 | 34.0000 | 14.0000 | 10.0000 | *0.0000 | 10.0000 | *0.2450+03 | 1.9.001 | *1.0000 | 1.9.400 | 1.9.400 | 1.9.400 |
| 24 | 1.2571 | 112.89 | .0182 | 34.0000 | 14.0000 | 10.0000 | *0.0000 | 10.0000 | *0.2450+03 | 1.9.001 | *1.0000 | 1.9.400 | 1.9.400 | 1.9.400 |
| 23 | 1.2006 | 103.85 | .0052 | 34.0000 | 14.0000 | 10.0000 | *0.0000 | 10.0000 | *0.2450+03 | 1.9.001 | *1.0000 | 1.9.400 | 1.9.400 | 1.9.400 |
| 22 | 1.1441 | 101.24 | .0014 | 34.0000 | 14.0000 | 10.0000 | *0.0000 | 10.0000 | *0.2450+03 | 1.9.001 | *1.0000 | 1.9.400 | 1.9.400 | 1.9.400 |
| 21 | 1.0877 | 100.54 | .0004 | 34.0000 | 14.0000 | 10.0000 | *0.0000 | 10.0000 | *0.2450+03 | 1.9.001 | *1.0000 | 1.9.400 | 1.9.400 | 1.9.400 |
| 20 | 1.0312 | 100.34 | .0001 | 34.0000 | 14.0000 | 10.0000 | *0.0000 | 10.0000 | *0.2450+03 | 1.9.001 | *1.0000 | 1.9.400 | 1.9.400 | 1.9.400 |
| 19 | .9748 | 100.31 | .0000 | 34.0000 | 14.0000 | 10.0000 | *0.0000 | 10.0000 | *0.2450+03 | 1.9.001 | *1.0000 | 1.9.400 | 1.9.400 | 1.9.400 |
| 18 | .9163 | 100.30 | .0000 | 34.0000 | 14.0000 | 10.0000 | *0.0000 | 10.0000 | *0.2450+03 | 1.9.001 | *1.0000 | 1.9.400 | 1.9.400 | 1.9.400 |
| 17 | .8619 | 100.30 | .0000 | 34.0000 | 14.0000 | 10.0000 | *0.0000 | 10.0000 | *0.2450+03 | 1.9.001 | *1.0000 | 1.9.400 | 1.9.400 | 1.9.400 |
| 16 | .8054 | 100.30 | .0000 | 34.0000 | 14.0000 | 10.0000 | *0.0000 | 10.0000 | *0.2450+03 | 1.9.001 | *1.0000 | 1.9.400 | 1.9.400 | 1.9.400 |
| 15 | .7489 | 100.30 | .0000 | 34.0000 | 14.0000 | 10.0000 | *0.0000 | 10.0000 | *0.2450+03 | 1.9.001 | *1.0000 | 1.9.400 | 1.9.400 | 1.9.400 |
| 14 | .6925 | 100.30 | .0000 | 34.0000 | 14.0000 | 10.0000 | *0.0000 | 10.0000 | *0.2450+03 | 1.9.001 | *1.0000 | 1.9.400 | 1.9.400 | 1.9.400 |
| 13 | .6360 | 100.30 | .0000 | 34.0000 | 14.0000 | 10.0000 | *0.0000 | 10.0000 | *0.2450+03 | 1.9.001 | *1.0000 | 1.9.400 | 1.9.400 | 1.9.400 |
| 12 | .5794 | 100.30 | .0000 | 34.0000 | 14.0000 | 10.0000 | *0.0000 | 10.0000 | *0.2450+03 | 1.9.001 | *1.0000 | 1.9.400 | 1.9.400 | 1.9.400 |
| 11 | .5231 | 100.30 | .0000 | 34.0000 | 14.0000 | 10.0000 | *0.0000 | 10.0000 | *0.2450+03 | 1.9.001 | *1.0000 | 1.9.400 | 1.9.400 | 1.9.400 |
| 10 | .4667 | 100.30 | .0000 | 34.0000 | 14.0000 | 10.0000 | *0.0000 | 10.0000 | *0.2450+03 | 1.9.001 | *1.0000 | 1.9.400 | 1.9.400 | 1.9.400 |
| 9 | .4102 | 100.30 | .0000 | 34.0000 | 14.0000 | 10.0000 | *0.0000 | 10.0000 | *0.2450+03 | 1.9.001 | *1.0000 | 1.9.400 | 1.9.400 | 1.9.400 |
| 8 | .3537 | 100.30 | .0000 | 34.0000 | 14.0000 | 10.0000 | *0.0000 | 10.0000 | *0.2450+03 | 1.9.001 | *1.0000 | 1.9.400 | 1.9.400 | 1.9.400 |
| 7 | .2973 | 100.30 | .0000 | 34.0000 | 14.0000 | 10.0000 | *0.0000 | 10.0000 | *0.2450+03 | 1.9.001 | *1.0000 | 1.9.400 | 1.9.400 | 1.9.400 |
| 6 | .2408 | 100.30 | .0000 | 34.0000 | 14.0000 | 10.0000 | *0.0000 | 10.0000 | *0.2450+03 | 1.9.001 | *1.0000 | 1.9.400 | 1.9.400 | 1.9.400 |
| 5 | .1844 | 100.30 | .0000 | 34.0000 | 14.0000 | 10.0000 | *0.0000 | 10.0000 | *0.2450+03 | 1.9.001 | *1.0000 | 1.9.400 | 1.9.400 | 1.9.400 |
| 4 | .1279 | 100.30 | .0000 | 34.0000 | 14.0000 | 10.0000 | *0.0000 | 10.0000 | *0.2450+03 | 1.9.001 | *1.0000 | 1.9.400 | 1.9.400 | 1.9.400 |
| 3 | .0715 | 100.30 | .0000 | 34.0000 | 14.0000 | 10.0000 | *0.0000 | 10.0000 | *0.2450+03 | 1.9.001 | *1.0000 | 1.9.400 | 1.9.400 | 1.9.400 |
| 2 | .0150 | 100.30 | .0000 | 40.0000 | 40.0000 | 10.0000 | *0.0000 | 10.0000 | *0.2450+03 | 1.9.001 | *1.0000 | 1.9.400 | 1.9.400 | 1.9.400 |
| 1 | .0000 | 100.30 | .0000 | -20.0000 | -20.0000 | 10.0000 | *0.0000 | 10.0000 | *0.2450+03 | 1.9.001 | *1.0000 | 1.9.400 | 1.9.400 | 1.9.400 |

| NODE | GAS FLOW RATE(M3/SEC) | | | SOURCES AND SINKS | | | CONCENTRATIONS | | |
|------|-----------------------|--------|----------|-------------------|------|---------|----------------|-------|-----------------|
| | INT COMB | OXYGEN | NITROGEN | HYDROGEN | Pyro | Depo | Sink | Burn | Total |
| 36 | .9620-03 | .05 | .26-11 | .97-06 | .00 | .672-04 | .257-03 | .0000 | .145-03 .512-03 |

| | | | | | | | | | | | | | | | |
|----|----------|-----|--------|--------|-----|----------|----------|------|---------|---------|---------|------|---------|---------|---------|
| 35 | .9618-03 | .00 | .26-11 | .24-05 | .00 | .2445-04 | .2447-03 | .000 | .169-04 | .175-04 | .27-04 | .000 | .377-05 | .168-03 | .516-03 |
| 35 | .9594-03 | .00 | .26-11 | .24-05 | .00 | .619-04 | .238-03 | .000 | .169-04 | .175-04 | .27-04 | .000 | .377-05 | .168-03 | .516-03 |
| 15 | .9565-03 | .00 | .26-10 | .31-05 | .00 | .593-04 | .226-03 | .000 | .162-04 | .182-04 | .295-04 | .000 | .396-05 | .179-03 | .518-03 |
| 35 | .9534-03 | .00 | .16-07 | .83-05 | .00 | .567-04 | .219-03 | .000 | .169-04 | .180-04 | .164-04 | .000 | .413-05 | .190-03 | .520-03 |
| 35 | .9451-03 | .00 | .37-06 | .11-04 | .00 | .473-04 | .185-03 | .000 | .169-04 | .185-03 | .387-04 | .000 | .439-05 | .234-03 | .531-03 |
| 34 | .9349-03 | .00 | .93-05 | .62-05 | .00 | .388-04 | .154-03 | .000 | .169-04 | .154-03 | .249-04 | .000 | .442-05 | .276-03 | .544-03 |
| 33 | .9349-03 | .00 | .93-05 | .62-05 | .00 | .388-04 | .154-03 | .000 | .169-04 | .154-03 | .459-04 | .000 | .442-05 | .276-03 | .544-03 |
| 32 | .9381-03 | .00 | .23-03 | .29-05 | .00 | .317-04 | .129-03 | .000 | .276-04 | .535-04 | .535-04 | .000 | .359-05 | .315-03 | .156-03 |
| 31 | .1168-02 | .00 | .11-03 | .11-05 | .00 | .248-04 | .103-03 | .000 | .263-04 | .866-04 | .866-04 | .000 | .286-05 | .340-03 | .584-03 |
| 30 | .1275-02 | .00 | .13-04 | .28-06 | .00 | .191-04 | .826-04 | .000 | .231-04 | .130-03 | .130-03 | .000 | .223-05 | .366-03 | .622-03 |
| 29 | .1288-02 | .00 | .00 | .00 | .00 | .144-04 | .668-04 | .000 | .190-04 | .168-03 | .168-03 | .000 | .169-05 | .421-03 | .711-03 |
| 28 | .1288-02 | .00 | .00 | .00 | .00 | .130-04 | .659-04 | .000 | .169-04 | .169-04 | .209-03 | .000 | .152-05 | .443-03 | .747-03 |
| 26 | .1288-02 | .00 | .00 | .00 | .00 | .116-04 | .575-04 | .000 | .177-04 | .233-03 | .233-03 | .000 | .136-05 | .470-03 | .791-03 |
| 25 | .1288-02 | .00 | .00 | .00 | .00 | .106-04 | .545-04 | .000 | .169-04 | .258-03 | .258-03 | .000 | .123-05 | .502-03 | .844-03 |
| 24 | .1016-02 | .00 | .65-03 | .00 | .00 | .101-04 | .535-04 | .000 | .165-04 | .275-03 | .275-03 | .000 | .118-05 | .525-03 | .881-03 |
| 23 | .3637-03 | .00 | .33-03 | .00 | .00 | .100-04 | .514-04 | .000 | .164-04 | .277-03 | .277-03 | .000 | .116-05 | .528-03 | .884-03 |
| 27 | .3009-04 | .00 | .29-04 | .00 | .00 | .100-04 | .500-04 | .000 | .164-04 | .277-03 | .277-03 | .000 | .118-05 | .528-03 | .884-03 |
| 27 | .1463-05 | .00 | .14-05 | .00 | .00 | .100-04 | .494-04 | .000 | .164-04 | .277-03 | .277-03 | .000 | .118-05 | .528-03 | .884-03 |
| 27 | .6562-07 | .00 | .64-07 | .00 | .00 | .100-04 | .534-04 | .000 | .164-04 | .277-03 | .277-03 | .000 | .118-05 | .528-03 | .884-03 |
| 27 | .1683-08 | .00 | .17-08 | .00 | .00 | .100-04 | .534-04 | .000 | .164-04 | .277-03 | .277-03 | .000 | .118-05 | .528-03 | .884-03 |
| 26 | .0000 | .00 | .00 | .00 | .00 | .100-04 | .514-04 | .000 | .164-04 | .277-03 | .277-03 | .000 | .118-05 | .528-03 | .884-03 |
| 25 | .0000 | .00 | .00 | .00 | .00 | .100-04 | .534-04 | .000 | .164-04 | .277-03 | .277-03 | .000 | .118-05 | .528-03 | .884-03 |
| 24 | .0000 | .00 | .00 | .00 | .00 | .100-04 | .534-04 | .000 | .164-04 | .277-03 | .277-03 | .000 | .118-05 | .528-03 | .884-03 |
| 23 | .0000 | .00 | .00 | .00 | .00 | .100-04 | .534-04 | .000 | .164-04 | .277-03 | .277-03 | .000 | .118-05 | .528-03 | .884-03 |
| 22 | .0000 | .00 | .00 | .00 | .00 | .100-04 | .524-04 | .000 | .164-04 | .277-03 | .277-03 | .000 | .118-05 | .528-03 | .884-03 |
| 21 | .0000 | .00 | .00 | .00 | .00 | .100-04 | .534-04 | .000 | .164-04 | .277-03 | .277-03 | .000 | .118-05 | .528-03 | .884-03 |
| 20 | .0000 | .00 | .00 | .00 | .00 | .100-04 | .534-04 | .000 | .164-04 | .277-03 | .277-03 | .000 | .118-05 | .528-03 | .884-03 |
| 19 | .0000 | .00 | .00 | .00 | .00 | .100-04 | .534-04 | .000 | .164-04 | .277-03 | .277-03 | .000 | .118-05 | .528-03 | .884-03 |
| 18 | .0000 | .00 | .00 | .00 | .00 | .100-04 | .534-04 | .000 | .164-04 | .277-03 | .277-03 | .000 | .118-05 | .528-03 | .884-03 |
| 17 | .0000 | .00 | .00 | .00 | .00 | .100-04 | .534-04 | .000 | .164-04 | .277-03 | .277-03 | .000 | .118-05 | .528-03 | .884-03 |
| 16 | .0000 | .00 | .00 | .00 | .00 | .100-04 | .534-04 | .000 | .164-04 | .277-03 | .277-03 | .000 | .118-05 | .528-03 | .884-03 |
| 15 | .0000 | .00 | .00 | .00 | .00 | .100-04 | .534-04 | .000 | .164-04 | .277-03 | .277-03 | .000 | .118-05 | .528-03 | .884-03 |
| 14 | .0000 | .00 | .00 | .00 | .00 | .100-04 | .534-04 | .000 | .164-04 | .277-03 | .277-03 | .000 | .118-05 | .528-03 | .884-03 |
| 13 | .0000 | .00 | .00 | .00 | .00 | .100-04 | .534-04 | .000 | .164-04 | .277-03 | .277-03 | .000 | .118-05 | .528-03 | .884-03 |
| 12 | .0000 | .00 | .00 | .00 | .00 | .100-04 | .534-04 | .000 | .164-04 | .277-03 | .277-03 | .000 | .118-05 | .528-03 | .884-03 |
| 11 | .0000 | .00 | .00 | .00 | .00 | .100-04 | .534-04 | .000 | .164-04 | .277-03 | .277-03 | .000 | .118-05 | .528-03 | .884-03 |
| 10 | .0000 | .00 | .00 | .00 | .00 | .100-04 | .534-04 | .000 | .164-04 | .277-03 | .277-03 | .000 | .118-05 | .528-03 | .884-03 |
| 9 | .0000 | .00 | .00 | .00 | .00 | .100-04 | .534-04 | .000 | .164-04 | .277-03 | .277-03 | .000 | .118-05 | .528-03 | .884-03 |
| 8 | .0000 | .00 | .00 | .00 | .00 | .100-04 | .534-04 | .000 | .164-04 | .277-03 | .277-03 | .000 | .118-05 | .528-03 | .884-03 |
| 7 | .0000 | .00 | .00 | .00 | .00 | .100-04 | .534-04 | .000 | .164-04 | .277-03 | .277-03 | .000 | .118-05 | .528-03 | .884-03 |
| 6 | .0000 | .00 | .00 | .00 | .00 | .100-04 | .534-04 | .000 | .164-04 | .277-03 | .277-03 | .000 | .118-05 | .528-03 | .884-03 |
| 5 | .0000 | .00 | .00 | .00 | .00 | .100-04 | .534-04 | .000 | .164-04 | .277-03 | .277-03 | .000 | .118-05 | .528-03 | .884-03 |
| 4 | .0000 | .00 | .00 | .00 | .00 | .100-04 | .534-04 | .000 | .164-04 | .277-03 | .277-03 | .000 | .118-05 | .528-03 | .884-03 |
| 3 | .0000 | .00 | .00 | .00 | .00 | .100-04 | .534-04 | .000 | .164-04 | .277-03 | .277-03 | .000 | .118-05 | .528-03 | .884-03 |
| 2 | .0000 | .00 | .00 | .00 | .00 | .100-04 | .534-04 | .000 | .164-04 | .277-03 | .277-03 | .000 | .118-05 | .528-03 | .884-03 |
| 1 | .0000 | .00 | .00 | .00 | .00 | .100-04 | .534-04 | .000 | .164-04 | .277-03 | .277-03 | .000 | .118-05 | .528-03 | .884-03 |

TIME= 500.00 TOTAL ITERSNS= 1070

| NODE | DISTANCE FROM BACK (IN) | CONDUCTED HEAT FLUX (BTU/F ² -SEC) | | DECOMP TOTAL | | | DENSITIES (LBM/FT ³) | | | INTERNAL PRESSURE (LBF/FT ²) | | | MOL AT | VELOCITY (FT/SEC) |
|------|-------------------------|---|---------|--------------|----------|---------|----------------------------------|---------|--------------|--|--------------|-------|--------|-------------------|
| | | TEMP (DEG F) | DECOMP | CARBON | GRAPHITE | SILICA | DEPU | PIRO | TROGEN | HYDROGEN | BURN | TOTAL | | |
| 35 | 1.8864 | 2258.67 | - | 20.1547 | +0.000 | 14.6579 | +0.000 | 5.49865 | +0.000 | 24.500 | +0.0029+0.03 | | | |
| 34 | 1.8702 | 2262.03 | +0.1518 | 21.0084 | +0.000 | 15.1808 | +0.000 | 6.2777 | +0.0020+0.03 | 19.735 | +0.1174+0.0 | | | |
| 34 | 1.8540 | 2263.43 | +0.943 | 23.5730 | +0.000 | 16.4121 | +0.000 | 7.1809 | +0.0059+0.03 | 17.409 | +0.3265+0.0 | | | |
| 34 | 1.8378 | 2263.23 | +0.207 | 25.2416 | +0.000 | 17.5084 | +0.000 | 7.7832 | +0.0070+0.03 | 16.008 | +0.3344+0.0 | | | |
| 34 | 1.8216 | 2261.08 | +0.7047 | 27.0206 | +0.000 | 18.6123 | +0.000 | 8.4085 | +0.0059+0.03 | 15.071 | +0.3415+0.0 | | | |
| 33 | 1.7652 | 2239.11 | +0.2359 | 24.3065 | +0.000 | 19.0354 | +0.000 | 9.3511 | +0.0076+0.03 | 14.863 | +0.3511+0.0 | | | |
| 32 | 1.7087 | 2199.67 | +0.4316 | 29.3171 | +0.000 | 19.5871 | +0.000 | 9.7201 | +0.0080+0.03 | 14.942 | +0.4441+0.0 | | | |
| 31 | 1.6523 | 2141.72 | +0.0115 | 27.6216 | +0.000 | 17.7371 | +0.000 | 9.6845 | +0.0162+0.03 | 15.009 | +0.4358+0.0 | | | |
| 30 | 1.5958 | 2067.43 | +2.016 | 21.8136 | +0.000 | 11.8432 | +0.000 | 9.9506 | +0.0256+0.03 | 15.222 | +0.4359+0.0 | | | |
| 29 | 1.5393 | 1979.72 | +2.364 | 20.5022 | +0.000 | 10.5223 | +0.000 | 9.9799 | +0.0340+0.03 | 15.516 | +0.4317+0.0 | | | |
| 28 | 1.4829 | 1878.34 | +2.412 | 20.1104 | +0.000 | 10.1177 | +0.000 | 9.9927 | +0.0416+0.03 | 15.867 | +0.4145+0.0 | | | |
| 27 | 1.4424 | 1761.54 | +2.493 | 20.0189 | +0.000 | 10.0210 | +0.000 | 9.9978 | +0.0474+0.03 | 16.263 | +0.3946+0.0 | | | |
| 26 | 1.3700 | 1625.94 | +2.370 | 20.0022 | +0.000 | 10.0024 | +0.000 | 9.9994 | +0.0555+0.03 | 16.700 | +0.3478+0.0 | | | |
| 25 | 1.3135 | 1464.72 | +2.347 | 20.0001 | +0.001 | 10.0000 | +0.000 | 10.0000 | +0.0604+0.03 | 17.452 | +0.3992+0.0 | | | |
| 24 | 1.2934 | 1419.02 | +2.203 | 20.1650 | +0.050 | 10.0000 | +0.000 | 10.0000 | +0.0810+0.03 | 17.413 | +0.3642+0.0 | | | |
| 24 | 1.2853 | 1369.25 | +2.191 | 21.0770 | +0.070 | 10.0000 | +0.000 | 10.0000 | +0.0824+0.03 | 17.615 | +0.3648+0.0 | | | |
| 24 | 1.2712 | 1311.30 | +1.919 | 24.8359 | +0.0359 | 10.0000 | +0.000 | 10.0000 | +0.0815+0.03 | 17.977 | +0.3266+0.0 | | | |
| 24 | 1.2571 | 1236.01 | +1.6686 | 26.2045 | +0.02045 | 10.0000 | +0.000 | 10.0000 | +0.0875+0.03 | 17.955 | +0.2256+0.0 | | | |
| 23 | 1.2429 | 1130.60 | +1.3550 | 31.9193 | +1.19193 | 11.9193 | +0.000 | 10.0000 | +0.0953+0.03 | 18.053 | +0.9713+0.1 | | | |
| 23 | 1.2288 | 1024.63 | +1.1385 | 33.4663 | +1.34663 | 13.4663 | +0.000 | 10.0000 | +0.0983+0.03 | 18.091 | +0.2528+0.1 | | | |
| 23 | 1.2147 | 882.20 | +0.937 | 13.6774 | +1.36774 | 13.6774 | +0.000 | 10.0000 | +0.0999+0.03 | 18.103 | +0.4960+0.2 | | | |
| 23 | 1.2006 | 782.57 | +0.6414 | 33.9213 | +13.9213 | 13.9213 | +0.000 | 10.0000 | +0.0995+0.03 | 18.107 | +0.4679+0.3 | | | |
| 22 | 1.1865 | 705.24 | +0.616 | 33.9864 | +13.9864 | 13.9864 | +0.000 | 10.0000 | +0.0996+0.03 | 18.109 | +0.3456+0.3 | | | |
| 22 | 1.1724 | 635.10 | +0.4422 | 33.9995 | +13.9995 | 13.9995 | +0.000 | 10.0000 | +0.0998+0.03 | 18.110 | +0.2167+0.3 | | | |
| 22 | 1.1583 | 566.37 | +0.427 | 33.9949 | +13.9949 | 13.9949 | +0.000 | 10.0000 | +0.0997+0.03 | 18.111 | +0.1015+0.3 | | | |
| 22 | 1.1441 | 501.51 | +0.3022 | 34.0000 | +14.0000 | 14.0000 | +0.000 | 10.0000 | +0.0997+0.03 | 18.111 | +0.7124+0.1 | | | |
| 21 | 1.0877 | 334.51 | +0.2284 | 34.0000 | +14.0000 | 14.0000 | +0.000 | 10.0000 | +0.0999+0.03 | 18.111 | +0.00000 | | | |
| 20 | 1.0312 | 235.44 | +0.1557 | 34.0000 | +14.0000 | 14.0000 | +0.000 | 10.0000 | +0.0999+0.03 | 18.111 | +0.00000 | | | |
| 19 | 9948 | 176.54 | +0.0942 | 34.0000 | +14.0000 | 14.0000 | +0.000 | 10.0000 | +0.0999+0.03 | 18.111 | +0.00000 | | | |
| 18 | 9183 | 56.50 | +0.050 | 34.0000 | +14.0000 | 14.0000 | +0.000 | 10.0000 | +0.0999+0.03 | 18.111 | +0.00000 | | | |
| 17 | 8619 | 12.63 | +0.048 | 34.0000 | +14.0000 | 14.0000 | +0.000 | 10.0000 | +0.0999+0.03 | 18.111 | +0.00000 | | | |
| 16 | 8054 | 11.45 | +0.013 | 34.0000 | +14.0000 | 14.0000 | +0.000 | 10.0000 | +0.0999+0.03 | 18.111 | +0.00000 | | | |
| 15 | 7748 | 10.06 | +0.066 | 34.0000 | +14.0000 | 14.0000 | +0.000 | 10.0000 | +0.0999+0.03 | 18.111 | +0.00000 | | | |
| 14 | 6925 | 10.31 | +0.034 | 34.0000 | +14.0000 | 14.0000 | +0.000 | 10.0000 | +0.0999+0.03 | 18.111 | +0.00000 | | | |
| 13 | 6360 | 10.16 | +0.016 | 34.0000 | +14.0000 | 14.0000 | +0.000 | 10.0000 | +0.0999+0.03 | 18.111 | +0.00000 | | | |
| 12 | 5796 | 10.93 | +0.003 | 34.0000 | +14.0000 | 14.0000 | +0.000 | 10.0000 | +0.0999+0.03 | 18.111 | +0.00000 | | | |
| 11 | 5231 | 10.56 | +0.003 | 34.0000 | +14.0000 | 14.0000 | +0.000 | 10.0000 | +0.0999+0.03 | 18.111 | +0.00000 | | | |
| 10 | 4667 | 10.41 | +0.002 | 34.0000 | +14.0000 | 14.0000 | +0.000 | 10.0000 | +0.0999+0.03 | 18.111 | +0.00000 | | | |
| 9 | 4102 | 10.34 | +0.001 | 34.0000 | +14.0000 | 14.0000 | +0.000 | 10.0000 | +0.0999+0.03 | 18.111 | +0.00000 | | | |
| 8 | 3537 | 10.32 | +0.000 | 34.0000 | +14.0000 | 14.0000 | +0.000 | 10.0000 | +0.0999+0.03 | 18.111 | +0.00000 | | | |
| 7 | 2973 | 10.30 | +0.000 | 34.0000 | +14.0000 | 14.0000 | +0.000 | 10.0000 | +0.0999+0.03 | 18.111 | +0.00000 | | | |
| 6 | 2407 | 10.30 | +0.000 | 34.0000 | +14.0000 | 14.0000 | +0.000 | 10.0000 | +0.0999+0.03 | 18.111 | +0.00000 | | | |
| 5 | 116 | 10.30 | +0.000 | 34.0000 | +14.0000 | 14.0000 | +0.000 | 10.0000 | +0.0999+0.03 | 18.111 | +0.00000 | | | |
| 4 | 1279 | 10.30 | +0.000 | 34.0000 | +14.0000 | 14.0000 | +0.000 | 10.0000 | +0.0999+0.03 | 18.111 | +0.00000 | | | |
| 3 | 0715 | 10.30 | +0.000 | 34.0000 | +14.0000 | 14.0000 | +0.000 | 10.0000 | +0.0999+0.03 | 18.111 | +0.00000 | | | |
| 2 | 0150 | 10.30 | +0.000 | 484.0000 | +46.0000 | 10.0000 | +0.000 | 10.0000 | +0.0997+0.03 | 18.111 | +0.00000 | | | |
| 1 | 0.000 | 10.30 | +0.000 | -20.0000 | +10.0000 | 10.0000 | +0.000 | 10.0000 | +0.0997+0.03 | 18.111 | +0.00000 | | | |

97
GAS FLOW
NODE RATE(LBM/
PYR-SEC)

SOURCES AND SINKS
(LBM/Node-SEC)
DEPO S1-C INT COMB OXYGEN PYRO DEPU TROGEN HYDROGEN BURN ILMBFTJ V0101

t = 500

| | | | | | | |
|----|----------|-----|---------|-----|---------|---------|
| 35 | *6800-03 | .00 | *586-03 | .00 | *221-07 | *323-02 |
| 34 | *7399-03 | .00 | *395-03 | .00 | *109-03 | *334-03 |
| 34 | *7683-03 | .00 | *262-03 | .00 | *153-02 | *363-02 |
| 34 | *7673-03 | .00 | *11-05 | .00 | *105-02 | *391-02 |
| 34 | *7662-03 | .00 | *171-03 | .00 | *215-03 | *409-02 |
| 33 | *7662-03 | .00 | *25-05 | .00 | *497-03 | *254-02 |
| 33 | *7637-03 | .00 | *110-03 | .00 | *452-03 | *254-02 |
| 32 | *7599-03 | .00 | *38-05 | .00 | *450-03 | *286-02 |
| 32 | *446-04 | .00 | *35-04 | .00 | *464-03 | *38-02 |
| 31 | *8045-03 | .00 | *32-05 | .00 | *396-03 | *37-02 |
| 31 | *64-04 | .00 | *23-05 | .00 | *251-03 | *351-02 |
| 30 | *8464-03 | .00 | *14-04 | .00 | *591-04 | *35-02 |
| 29 | *8995-03 | .00 | *15-04 | .00 | *498-04 | *216-02 |
| 28 | *9132-03 | .00 | *51-05 | .00 | *419-04 | *216-02 |
| 27 | *9179-03 | .00 | *14-05 | .00 | *351-04 | *121-02 |
| 26 | *9191-03 | .00 | *47-07 | .00 | *29-04 | *121-02 |
| 25 | *9194-03 | .00 | *00 | .00 | *236-04 | *122-02 |
| 24 | *9194-03 | .00 | *26-04 | .00 | *591-04 | *122-02 |
| 24 | *8933-U3 | .00 | *11-03 | .00 | *202-04 | *275-02 |
| 24 | *7787-03 | .00 | *26-03 | .00 | *163-03 | *275-02 |
| 24 | *5233-02 | .00 | *29-03 | .00 | *160-03 | *20-02 |
| 23 | *2300-03 | .00 | *16-03 | .00 | *178-04 | *20-02 |
| 23 | *6441-04 | .00 | *50-04 | .00 | *172-04 | *15-02 |
| 23 | *1637-04 | .00 | *12-04 | .00 | *171-04 | *14-02 |
| 23 | *4197-75 | .00 | *29-15 | .00 | *170-04 | *14-02 |
| 22 | *1286-05 | .00 | *95-1 | .00 | *170-04 | *14-02 |
| 22 | *3374-04 | .00 | *27-15 | .00 | *170-04 | *14-02 |
| 22 | *6974-07 | .00 | *64-07 | .00 | *170-04 | *14-02 |
| 22 | *6044-05 | .00 | *50-05 | .00 | *170-04 | *14-02 |
| 21 | *0000 | .00 | *00 | .00 | *170-04 | *14-02 |
| 20 | *0000 | .00 | *00 | .00 | *170-04 | *14-02 |
| 19 | *0000 | .00 | *00 | .00 | *170-04 | *14-02 |
| 18 | *0000 | .00 | *00 | .00 | *170-04 | *14-02 |
| 17 | *0000 | .00 | *00 | .00 | *170-04 | *14-02 |
| 16 | *0000 | .00 | *00 | .00 | *170-04 | *14-02 |
| 15 | *0000 | .00 | *00 | .00 | *170-04 | *14-02 |
| 14 | *0000 | .00 | *00 | .00 | *170-04 | *14-02 |
| 13 | *0000 | .00 | *00 | .00 | *170-04 | *14-02 |
| 12 | *0000 | .00 | *00 | .00 | *170-04 | *14-02 |
| 11 | *0000 | .00 | *00 | .00 | *170-04 | *14-02 |
| 10 | *0000 | .00 | *00 | .00 | *170-04 | *14-02 |
| 9 | *0000 | .00 | *00 | .00 | *170-04 | *14-02 |
| 8 | *0000 | .00 | *00 | .00 | *170-04 | *14-02 |
| 7 | *0000 | .00 | *00 | .00 | *170-04 | *14-02 |
| 6 | *0000 | .00 | *00 | .00 | *170-04 | *14-02 |
| 5 | *0000 | .00 | *00 | .00 | *170-04 | *14-02 |
| 4 | *0000 | .00 | *00 | .00 | *170-04 | *14-02 |
| 3 | *0000 | .00 | *00 | .00 | *170-04 | *14-02 |
| 2 | *0000 | .00 | *00 | .00 | *170-04 | *14-02 |
| | | | | | | |

PROGRAM LISTING

This is a sequenced listing of the CHAD computer program (including subroutines).

```

- FOR BLKD/D2, BLKD/D2, BLKD/C2
BLOCK DATA
COMMON /BLOCKA/
1ABSORP(10), ABSC      ,ACTENC      ,ACTENS      ,ACTENV(4,10)  ,CHD00000
2BSTAR      ,CCPC(4)    ,CCPG(4)      ,CHARPT(101)  ,CKC(4)      ,CHD00010
3COEFT(4,10), CONDC   ,CONDV(100)   ,CONST(4,10)  ,COVERX(100)  ,CHD00040
4CPBAR      ,CPC       ,CPV(100)     ,DIFREC      ,UMATER(10)  ,CHD00050
5EFCOLC     ,EFCOLS    ,EFCOLV(4,10), EMIS(10)   ,EMISC      ,CHD00060
6HOFM(10)   ,HCOM      ,HCOMG       ,HSUB        ,MAT(100)    ,CHD00070
7MATOMN     ,MATMNE    ,MN          ,NN          ,NNP         ,CHD00080
8NNSAVE     ,NRDIV     ,NREND       ,NRGO        ,NST         ,CHD00090
9PARTIN(101), PHI      ,OBYRAD     ,OCOMB       ,OEXTR      ,CHD00100
10GPCOM     ,GSUBL     ,RECPRO     ,REORDC     ,REORDS    ,CHD00110
2REORDV(4,10), RHOSZ   ,RHOS(305)   ,RHOCPX(101) ,FLOC       ,CHD00120
3RHOV(10)   ,SABL      ,SABLc      ,SDOT        ,SDOTC      ,CHD00130
4SLOPE(10)  ,TMELT(10) ,TSZ         ,TS(205)    ,TRCHAR     ,CHD00140
5WFZ        ,WF(205)   ,XCHAR      ,XINIT      ,XLEFT(101)  ,CHD00150
6XMASS      ,XMDOTC   ,XMDOTD    ,XMDOTG    ,XMDOTL    ,CHD00160
7XMDOTR    ,XMDOTS   ,XTOTAL     ,XVIRG(101) ,XZONE     ,CHD00170
COMMON/BLOCKC/
1BLPRES(20+11), COMMAX ,CUTOFF     ,F(20,11)   ,CHD00180
2FLOW(20,11), HCONV(20,11), IERROR  ,JUNCT      ,L           ,CHD00190
3N          ,NOSECH   ,QBACK      ,QCONV(20,11), QGAS(20,11) ,CHD00200
40MISC     ,TIME      ,TPRINT     ,TWALL(20,11), XIWALL(20,11) ,CHD00210
5XIR(20,11)
COMMON /BLOCKJ/
1FLUXI(200), TEDEP(200), XEDEP(101), EDEP(101), NTEDEP, CHD00220
2NXEDEP, ITEPEP, EDFLUX(100)
COMMON /BLOCKK/NN1, QCOND(205)
COMMON/BLOCKN/COORD
COMMON/BLOCKR/DIFC(4), EROC(4), ERODE
COMMON /CHCOM/ DTAU, IBE(10), IBS(10), IBSPN, CHD00230
1IGTYP(10), IHDN(4), IM, IZB(4), IZG(3,10), CHD00240
2IZGT(3), JRSW, NCSN(10), NSHL(3), NSHR(3), CHD00250
3NZEN(3), NZSN(3), RHO1(305), RHO2(305), RHO3(410), CHD00260
4I          ,TEMPA2(205), TEMPAP(421), TEMPAP(421), TEMPAP(205), CHD00270
5          ,DELEX(100), DISTL(100), DUM(10), ICOM, CHD00280
6IYS, LFT, MG, MDUM, MCEN(10), NCUT, ND(3), NLZN, SN, SN1, CHD00290
7SCHECK
COMMON /NASCOM/ CHARRO, AIRM,
1CARBN1(205), CARBN5(205), SILCA1(205), SILCA5(205), PYRO(205), DEP(205) CHD00300
2HYD(205), AERO(205), AERN(205), BURN(205), WFD(205), WDEP(205), WS(20) CHD00310
35), WBRN(205), EMWT(205), FRG(205) CHD00320
4, TIME(50), TFT(50), NPTS CHD00330
5, POR(205), PERM1(205), PERM2(205), VISC(205), GCON, RHOTS, CARTS, SILTS, CHD00340
6PORT, PERT1, PERT2, DCOM, DC00, DCOPY, DCOPD, DCOS1, DCOCM, DCON, CFXH, CFXO, CHD00350
7CFXPY, CFXDP, CFXSI, CFXCM, CFXN, DIFC(205), SOX(205) CHD00360
8, ALLGAS(205), GRAF1(205), GRAF5(205), SPEED(205), DIFCH(205), DIFR(205) CHD00370
9, Y, SCO, VISCON, AF, BF, CILICA, REO, PMW, DMW, HMW, AOMW, ANMW, SMW, BMW, CX(6) CHD00380
1, QS, QBRN, ODEP
DATA NST, L, N, COORD, AIRM, GCON/1, I, 1, 1, 28, 96, 1545, / CHD00390
DATA CFXO, CFXN, CFXH, CFXPY, CFXDP, CFXSI, CFXCM/7#0, / CHD00400
C THE ABOVE DATA STATEMENTS ARE NORMALLY LEFT UNCHANGED CHD00410
C MATERIAL 1 DATA CHD00420
DATA (ACTENV(I,1), I=1,2)/23300, 0, / CHD00430

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DATA (EFCOLV(I,1),I=1,2)/11209.,0./ CHD00540
DATA (REORDV(I,1),I=1,2)/1.,0./ CHD00550
DATA HOFM(1)/350./ CHD00560
DATA (COEFT(I,1),I=1,4)/.43,0.,0.,0./ CHD00570
DATA (CONST(I,1),I=1,4)/.244E-5,11.53E-8,-1.67E-11,0./ CHD00580
DATA EMIS(1),ABSORP(1),RHOV(1),SLOPE(1)/.9,.9,34.,1.2/ CHD00590
C MATERIAL 2 DATA CHD00600
DATA (ACTFNV(I,2),I=1,2)/0.,0./ CHD00610
DATA (EFCOLV(I,2),I=1,2)/0.,0./ CHD00620
DATA (REORDV(I,2),I=1,2)/0.,0./ CHD00630
DATA HOFM(2)/120./ CHD00640
DATA (COEFT(I,2),I=1,4)/.09936,.1642E-4,.4055E-8,.1389E-10/ CHD00650
DATA (CONST(I,2),I=1,4)/.04125,.961E-5,0.,0./ CHD00660
DATA EMIS(2),ABSORP(2),RHOV(2),SLOPE(2)/.2,.6,484.,.7/ C'D00670
C CHAR DATA CHD00680
DATA ACTENC,EFCOLC,REORDC,HCOM /39855.,.673E9,.5,0./ CHD00690
DATA ACTENS,EFCOLS,REORDS,HSUB /0.,0.,0.,0.,0./ CHD00700
DATA (CPC(I),I=1,4)/.42,0.,0.,0./ CHD00710
DATA (CKC(I),I=1,4)/.168E-2,-.2968E-5,.1751E-8,-.2402E-12/ CHD00720
DATA EMISC,ABSC,RHOC,TRCHAR/.65,1.0,20.,1./ CHD00730
DATA CHARRO/10./ CHD00740
C GAS DATA CHD00750
DATA (CCPG(I),I=1,4),HCOMG/.7,0.,0.,0.,6173./ CHD00760
C INTERNAL FLOW AND DIFFUSION CONSTANTS CHD00770
DATA CARTS,RHOTS,SILTS,PORT,PERT1,PERT2/131.,70.,137.3,.75,
11.E-10,10./ CHD00780
DATA VISCO,VISCON/1.E-5,530./ CHD00790
DATA DCOCM,DCODP,DCOH,DCON,DCOO,DCOPY,DCOSI/7*1./ CHD00800
DATA ANMW,AOMW,BMW,DMW,HMW,PMW,SMW/28.,32.,28.,20.,16.,44./ CHD00810
C MISCELLANEOUS CONSTANTS CHD00820
DATA BSTAR,(DTFC(I),I=1,4)/.43,-.649,-2.54,-2.30,-.878/ CHD00830
DATA QSI,QDEP,QBRN/0.,0.,0./ CHD00840
DATA AF,BF,SILICA,REO/2.0921E3,40765.,8.194,1./ CHD00850
DATA (CX(I),I=1,6)/.01365,116.2,1777.,6.06E-4,.0114,4.72/ CHD00900
END CHD00910
CHD00920

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- FOR BLOCK,BLOCK
  SUBROUTINE BLOCK(XMC,TC,GAS,SLOPE,H,F,PHI)           CHD00930
  XMG=GAS                                              CHD00940
  TG=SLOPE                                             CHD00950
  IF(F-1.1) 10,10,20                                   CHD00960
  10 A=(XMC*TC**3+XMG*TG**3)/3.                         CHD00970
  GO TO 30                                              CHD00980
  20 A=(XMC*TC**3+XMG*TG**3)/3.                         CHD00990
  30 B=A/(H*1.E-20)                                     CHD01000
  IF(B-88.140,40,50                                     CHD01010
  40 PHI=EX> (~B)                                       CHD01020
  GO TO 60                                              CHD01030
  50 PHI=0,                                              CHD01040
  60 RETURN                                              CHD01050
  END                                                   CHD01060

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000015

0001

- FOR CHARM/S4,CHARM/S4
 SUBROUTINE CHARM
 C**** CHARM SUBROUTINE IN CHAP --JULY 1966 VERSION
 C LISTING FOR GAUDETTE 8528 TAPE

| | | | | | | |
|---|---|-------------------|-----------------------------|---------------|----------|----------|
| COMMON /BLOCKA/ | | | | | | |
| 1ABSORP(10) | •ABSC | •ACTENC | •ACTENS | •ACTENV(4,10) | CHD01070 | CHD01110 |
| 2BSTAR | •CCPC(4) | •CCPG(4) | •CHARPT(101) | •CKC(4) | CHD01080 | CHD01120 |
| 3COEFT(4,10) | •CONDc | •CONDV(100) | •CONST(4,10) | •COVERX(100) | CHD01090 | CHD01130 |
| 4CPBAR | •CPC | •CPV(100) | •DIFREC | •UMATER(10) | CHD01140 | CHD01150 |
| 5EFCOLC | •EFCOLS | •EFCOLV(4,10) | •EMIS(10) | •EMISC | CHD01160 | CHD01170 |
| 6HOFM(10) | •HCOM | •HCOMG | •HSUB | •MAT(100) | CHD01180 | CHD01190 |
| 7MATOMN | •MATMNE | •MN | •NN | •NNP | CHD01200 | CHD01220 |
| 8NNSAVE | •NRDIV | •NREND | •NRGO | •NST | CHD01230 | CHD01240 |
| 9PARTIN(101) | •PHI | •QBYRAD | •QCOMB | •QEXTR | CHD01250 | CHD01260 |
| 10QPCOM | •QSUBL | •RECPRO | •REORDC | •REORDS | CHD01270 | CHD01280 |
| 2REORDV(4,10) | •RH05Z | •RH05(305) | •RHOCPX(101) | •RHOC | CHD01290 | CHD01300 |
| 3RHOV(10) | •SABL | •SABLc | •SDOT | •SDOTC | CHD01310 | CHD01320 |
| 4SLOPE(10) | •TMELT(10) | •TSZ | •TS(205) | •TRCHAR | CHD01330 | CHD01340 |
| 5WFZ | •WF(205) | •XCHAR | •XINIT | •XLEFT(101) | CHD01350 | CHD01360 |
| 6XMASS | •XMDOtC | •XMDOtD | •XMDOtG | •XMDOtL | CHD01370 | CHD01380 |
| 7XMDOTR | •XMDOtS | •XTOTAL | •XVIRG(101) | •XZONE | CHD01390 | CHD01400 |
| COMMON /BLOCKB/ USER(243),BLDEN(20,11) | | | | | | CHD01420 |
| COMMON/BLOCKC/ | | | | | | CHD01430 |
| 1BLPRES(20,11) | | •COMMEX | •CUTOFF | •F(20,11) | CHD01440 | CHD01450 |
| 2FLOW(20,11) | •HCONV(20,11),IERROR | | •JUNCT | •L | CHD01460 | CHD01470 |
| 3N | •NOSECH | •QBACK | •QCONV(20,11),QGAS(20,11) | | CHD01480 | CHD01490 |
| 4QMISC | •TIME | •TPRINT | •TWALL(20,11),XIWALL(20,11) | | CHD01500 | CHD01510 |
| 5XIR(20,11) | | | | | CHD01520 | CHD01530 |
| COMMON /BLOCKJ/ | | | | | | CHD01540 |
| 1FLUXI(200),TEDEP(200),XEDEP(101),EDEP(101),NTEDEP, | | | | | CHD01550 | CHD01560 |
| 2NXEDEP,ITEPEP,EDFLUX(100) | | | | | CHD01570 | CHD01580 |
| COMMON /BLOCKK/NN1,QCOND(205) | | | | | | CHD01590 |
| COMMON/BLOCKN/COORD | | | | | | CHD01600 |
| COMMON/BLOCKR/DIFC(4),EROC(4),ERODE | | | | | | CHD01610 |
| COMMON /CHCOM/ DTAU, IBE(10), IBS(10), IBSPN, | | | | | | CHD01620 |
| 1IGTYP(10), IHON(4), IM, | I2B(3), | I2G(3,10), | | | CHD01630 | CHD01640 |
| 2IZGT(3), JRSW, | NCSN(10), | NSHL(3), | NSHR(3), | | CHD01650 | CHD01660 |
| 3NZEN(3), NZSN(3), | RHO1(305), | RHO2(305), | RHO3(410), | | CHD01670 | CHD01680 |
| 4I | •TEMPA2(205),TEMPA3(42),TEMPA4(42),TEMPA5(205), | | | | CHD01690 | CHD01700 |
| 5 | DELX(100),DISTL(100),DUM(10),ICOM, | | | | CHD01710 | CHD01720 |
| 6IYS,LFT,MG,MDUM,NCEN(10),NCUT,ND(3),NLZON,SN,SN1, | | | | | CHD01730 | CHD01740 |
| 7SCHECK | | | | | CHD01750 | CHD01760 |
| COMMON/NUCOM/ NADA: | | | | | | CHD01770 |
| 1EM(42) | | | | | CHD01780 | CHD01790 |
| COMMON /DACOM/ A(42), | | | | | | CHD01800 |
| 1ABVAL,ABVALM,ABVALS,B(42),C(42), | | CC(205),COND(42), | | | CHD01810 | CHD01820 |
| 2CONDXX,D(42),DD(205),DELTX(101),DGAS,DO, | | | | | CHD01830 | CHD01840 |
| 3DTAUC,DTAUS,DTAUX,DTF,DTR(3),EDFX,EDFXX,EMI(42), | | | | | CHD01850 | CHD01860 |
| 4ETA,ETAS,FHT(42),FHTX,FHTXX,GAGC,GAS1,GK,GX,GY,GZ, | | | | | CHD01870 | CHD01880 |
| 5HDA(5,10),IBSPM,IERR,IGC,IGL,IGLD,IGR,IGRL,IGT,IG2, | | | | | CHD01890 | CHD01900 |
| 6IHYS,INEG,IN1,IN2,IP,IPPLUS,ITER,ITERT,IX,IY,IZ,J,JBE, | | | | | CHD01910 | CHD01920 |
| 7JBEM,JBEX,JBND1,JBND2,JBS,JBSMP,JBSPN,JBX,JBX,JCEN, | | | | | CHD01930 | CHD01940 |
| 8JCENM,JCSN,JCSNM,JE,JE1,JE2,JHDN,JHDN1,JLSW,JSLAB,JX,JZ, | | | | | CHD01950 | CHD01960 |
| 9K1,LANDID,LRT,MARK,NADD(42),NASW,NBNST,NBND1(11), | | | | | CHD01970 | CHD01980 |
| 1NBSW,NDC,NDCM,NLSW(10),NOF,NOTIME,NPBSW,NPEIN,NPS2N,NPTSW, | | | | | CHD01990 | CHD02000 |

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2NRID,NR IDC,NRSW(10),NRZGN,NSLABH(10),NSLABH(10),NSW,NXSW, CHD01610
3NZON,NZONC,CNE,PSI,QSAVE,QTOT,QTOTAL,REFCTR,SBK,SDN, CHD01620
4SDCTN,SNS,SRA,TAR,TALOUT,TAUST(3),TAU1,TAU2,TAU2S,TEMPA, CHD01630
5TEMPST(3),THREE,TWO,WFP,WFX,WFX,XI,XMCOM,XSAVE CHD01640
COMMON /NASCOM/ CHARRO,AIRM, CHD01650
1CARBN1(205),CARBN5(205),SILCA1(205),SILCA5(205),PYRO(205),DEP(205)CHD01660
2+HYD(205),AERO(205),AERN(205),BURN(205),WFD(205), WDEP(205),WSI(205)CHD01670
35),WBRN(205),EMWT(205),PRG(205) CHD01680
4,TIMFX(50),TFT(50),NPTS CHD01690
5,POR(205),PERM1(205),PERM2(205),VISCI(205),GCON,RHOTS,CARTS,SILTS, CHD01700
6FORT,PERT1,PERT2,DCOH,DCOO,DCOPY,DCODP,DCOSI,DCOCM,DCON,CFXH,CFXO,CHD01710
7CFXPY,CFXDP,CFXSI,CFXCM,CFXN,DIFCO(205),SOX(205) CHD01720
8+ALLGAS(205),GRAFI(205),GRAFS(205),SPEED(205),DIFCH(205),DIFRI(205)CHD01730
9,VISCO,VISCON,AF,BF,SILICA,REO,PMW,DMW,HMW,AOMW,ANMW,SMW,BMW,CX(6)CHD01740
1,OSI,QBRN,QDEP,DACT CHD01750
COMMON /TABCOM/ NDOTS(4),TIME1(100),TIME2(100),TIME3(100), CHD01760
1TIME4(100),DSTEP(100),PSTEP(100),XRI(100),RH(100),QMU(100), CHD01770
2TT(100),PP(100),FF(100),AST(100) CHD01780
DIMENSION AREAC(42),COND0(43),EMBM(42),NBND2(10),NHDN(3), CHD01790
1PC(42),RATE(42),RH04(306), DELTAX(1),TEMPA1(1) . CHD01800
C*** DIMENSION STATEMENTS CHD01810
C CHD01820
C DIMENSION AREA(42),ARFAV(42) CHD01830
C C*** COMMON STATEMENTS CHD01840
C CHD01850
C CHD01860
C C*** EQUIVALENCE STATEMENTS CHD01870
C CHD01880
C CHD01890
EQUIVALENCE (NBND1(2),NBND2(1)) CHD01900
EQUIVALENCE (WF(1),RATE(1)) CHD01910
EQUIVALENCE (IHDN(2),NHDN(1)) CHD01920
EQUIVALENCE (RH03(103),RH04(1)) CHD01930
EQUIVALENCE (COND0(2),COND(1)) CHD01940
EQUIVALENCE (TEMPA1(1),TS(1)),(DELTAX(1),PARTIN(1)) CHD01950
EQUIVALENCE (EMBM(1),PC(1)) CHD01960
EQUIVALENCE (XMDOTG,GAS) CHD01970
EQUIVALENCE (MNOD,NNP) CHD01980
EQUIVALENCE (RH03(307), PC(1)), (RH03(350),AREAC(1)) CHD01990
EQUIVALENCE (RHOCPX(44),AREA(1),ARFAV(43)) CHD02000
C CHD02020
C*** ENTRY POINT TO SUBROUTINE CHD02030
C CHD02040
C TAUOUT=TAU1+COMMEX CHD02050
GO TO (10,13527),NST CHD02060
C CHD02070
C*** INITIAL SECTION--10-2599 (PASS THROUGH ON FIRST ENTRY ONLY) CHD02080
C CHD02090
C*** SETUP OF VARIOUS COEFFICIENTS-- SPECIFIC HEAT, CHD02100
C*** DECOMPOSITION REACTION FREQUENCY FACTORS,HEAT OF DECOMPOSITION CHD02110
C CHD02120
10 CONTINUE CHD02130
TWALL(1,1)=TS(NNP)
DO 11 J=1,4 CHD02170
11 CCPC(J) = RHOC*CCPC(J)/12. CHD02220
CHD02230

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DO 16 I=1,10
DO 12 J=1,4
12 COEFT(J,I) = COEFT(J,I)*RHOV(I)/12.
ONE = RHOV(I)-RHOC
IF (ONE) 13,13,10016
13 CONTINUF
DO 14 J=1,4
EFCOLV(J,I) = 0.
HDA(J,I) = 0.
14 CONTINUE
GO TO 16
10016 CONTINUF
TWO = 12./ONE
DO 20016 J=1,4
EFCOLV(J,I) = EFCOLV(J,I)*RHOV(I)/ONE**REORDV(J,I)
20016 HDA(J,I) = (CCPG(J)-TWO*(COEFT(J,I)-CCPC(J)))/FLOAT(J)
TEMPA = 536.67
HDA(5,I) = HOFM(I)-(HDA(1,I)+(HDA(2,I)+(HDA(3,I)+HDA(4,I)
1*TFMPA)*TEMPA)*TFMPA*TFMPA
16 RHOV(I)=ONE+1.E-10
DO 9 K=1,42
AREA(K)=1.
9 AREA(K)=1.
C
C
C*** ZEROING AND INITIALIZATION
C
C      ZONE CONTROL VALUES SET
IZB(1) = 119
IZB(2) = 187
IZB(3) = 187
IBSPM = 204
IBSPN = 203
IHDN(1) = 1
NHDN(1) = 4
NHDN(2) = 4
NHDN(3) = 4
NZSN(1) = NN
NZFN(1) = MNOD
NRZON = 1
NLZON = 1
C
IP = 3
NPE1N = 1
NPS2N = 1
C      NODE DIVIDERS SET
ND(1) = NN
ND(2) = 500
C      ZEROING
DO 17 J=1,3
NSHL(J) = 0
17 NSHR(J) = 0
DGAS = 0.
GAS1 = 0.
I=0

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CHD02240
CHD02250
CHD02260
CHD02270
CHD02280
CHD02290
CHD02300
CHD02310
CHD02320
CHD02330
CHD02340
CHD02350
CHD02360
CHD02370
CHD02380
CHD02390
CHD02400
CHD02410
CHD02420
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CHD02730
CHD02740
CHD02750
CHD02760
CHD02770
CHD02780
CHD02790
CHD02800
CHD02810
CHD02820
CHD02830
CHD02840
CHD02850

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WF(1)=0. CHD02860
ISAVE1=0 CHD02862
ISAVE2=0 CHD02863
ISAVF4=0 CHD02864
ISAVE5=0 CHD02865
ISAVE6=0 CHD02866
QGAS(1,1)=0. CHD02867
CHD02870
CHD02880
CHD02890
CHD02900
CHD02910
CHD02920
CHD02930
CHD02940
CHD02950
CHD02950
CHD02970
CHD02980
CHD02990
CHD03000
CHDC3010
CHD03020
CHD03030
CHD03040
CHD03050
CHD03060
CHD03070
CHD03080
CHD03090
CHD03100
CHD03110
CHD03120
CHD03130
CHD03140
CHD03150
CHD03160
CHD03170
CHD03180
CHD03190
CHD03200
CHD03210
CHD03220
CHD03230
CHD03240
CHD03250
CHD03260
CHD03270
CHD03280
CHD03290
CHD03300
CHD03310
CHD03320
CHD03330
CHD03340
C
      ITFR = 0
      NOTIMF = 0
C     OTHER VALUES SET
      PERT1=PEPT1*32*2
      PERT2=PERT2*32*2
      NRIDC = 1
      NZONC = 1
      NST = 2
      ETA = .005
      NRSW = 1
      NCUT = 1
      NPTSW = 1
      LFT = 1
      LRT = 2
      DO 18 J=1,3
      TAUST(J) = 0.
      DTR(J) = 0.
      TEMPST(J) = TS(NN)
18 CONTINUF
C
C****      SETUP OF TEMPERATURES AND DENSITIES
C****      PLACEMENT OF NODAL WIDTH VALUES INTO DELX ARRAY
C
      XLEFT(1)=0.
      XSAVE=0.6*PARTIN(1)+XLEFT(1)
      DO 19 J=1,NN
      I = MAT(J)
      RHO1(J) = RHOV(I)
      XLEFT(J+1)=XLEFT(J)+PARTIN(J)
19 DELX(J) = PARTIN(J)
      DO 20 I=1,MNOD
      TEMPAT(I) = TS(I)
      TEMPAS(I) = TS(I)
      RHO2(I) = RHO1(I)
      RHO3(I) = RHO1(I)
      J = I+IRSPM
      RHO1(J) = RHO1(I)
      RHO2(J) = RHO1(I)
      RHO3(J) = RHO1(I)
      RHO4(J) = RHO1(I)
      RHO5(J) = RHO1(I)
20 RHO5(J) = RHO1(I)
      I = IZB(1)-1
      K = NHDN(1)+1
      TEMPAT = TEMPAT(MNOD)
      ONE = (TEMPAT(MNOD)-TEMPAT(NN))/FLOAT(NHDN(1))
      DO 30 J=1,K

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I = I+1 CHD03350
TEMPA1(I) = TEMPA CHD03360
TEMPA2(I) = TFMPA CHD03370
TEMPA5(I) = TEMPA CHD03380
TEMPA = TEMPA+ONF CHD03390
RHO1(I) = RHO1(NN) CHD03400
RHO2(I) = RHO1(I) CHD03410
30 RHO5(I) = RHO1(I) CHD03420
HOLD=RHO-CARRO CHD03430
DO 40 J=1,205 CHD03440
CARBN1(J)=CHARRO CHD03450
CARBNS(J)=CHARRO CHD03460
GRAF1(J)=0. CHD03470
GRAF5(J)=0. CHD03480
SILCA1(J)=HOLD CHD03490
SILCA5(J)=HOLD CHD03500
PYRO(J)=1. CHD03510
FMWT(J)=AIRM CHD03520
40 CONTINUF CHD03530
DO 50 J=1,100 CHD03532
50 EDFLUX(J)=0. CHD03534
C
C**** SETTING OF TIMES AND DELTA TIMES
C
TAUOUT = COMMAX CHD03540
DTAU = COMMAX CHD03550
211 DTAUS = DTAU CHD03560
DTAUC = DTAU CHD03570
DTAUX = 0.5*DTAU CHD03580
TAU1 = 0. CHD03590
TAU2 = DTAU CHD03600
C
C**** NORMALIZED DISTANCES AND NORMALIZED NODE WIDTHS
C
IYS = ND(1) CHD03610
SN1 = XLEFT(MNOD)-XLEFT(IYS) CHD03620
DO 230 J=IYS,MNOD CHD03630
DISTL(J) = (XLEFT(J)-XLEFT(IYS))/SN1 CHD03640
230 DELX(J) = DELX(J)/SN1 CHD03650
C
SCHFCK = 0.5*SN1 CHD03660
C
C**** CALCULATION CONTROL--2600-2684
C
2600 NPBSW = IP CHD03670
MARK = 1 CHD03680
IG = 1 CHD03690
LANDID = 1 CHD03700
NRID = NRIDC CHD03710
NDC = 1 CHD03720
NDCM = 1 CHD03730
2603 IG2 = IG CHD03740
GO TO (2606,2614,2615),NPBSW CHD03750
2606 NBND1(IG) = NBSW+5 CHD03760
NCSN(IG) = 1 CHD03770

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| | | |
|-------|---|----------|
| 2608 | NBNST = 4 | CHD03880 |
| | NCEN(IG) = NPF1N | CHD03890 |
| | NSW = 1 | CHD03900 |
| | GO TO 2640 | CHD03910 |
| 2614 | NBN1(IG) = " | CHD03920 |
| | NCSN(IG) = NZSN | CHD03930 |
| | GO TO 2620 | CHD03940 |
| 2615 | NBN1(IG) = NBSW+5 | CHD03950 |
| | NCSN(IG) = 1 | CHD03960 |
| 2620 | NZON = NZONC | CHD03970 |
| | NBNST = 5 | CHD03980 |
| | IGC = 0 | CHD03990 |
| 2625 | IF (NCSN(IG)-NZSN(NZON)) 2628,2644,2644 | CHD04000 |
| 2628 | IF (NZSN(NZON)-ND(NDC)) 2635,2635,2679 | CHD04010 |
| 2629 | IF (NCSN(IG)-ND(NDC)) 12620,12629,12629 | CHD04020 |
| 12629 | LANDID=3 | CHD04030 |
| | NDC = NDC+1 | CHD04040 |
| | NDCM=1 | CHD04050 |
| | IGLD=IG | CHD04060 |
| | GO TO 2635 | CHD04070 |
| 12630 | NCEN(IG)=ND(NDC) | CHD04080 |
| | NDC = NDC+1 | CHD04090 |
| | LANDID=2 | CHD04100 |
| | NSW = 5 | CHD04110 |
| | NDCM = 2 | CHD04120 |
| | GO TO 2640 | CHD04130 |
| 2635 | NCEN(IG) = NZSN(NZON) | CHD04140 |
| | NSW = 2 | CHD04150 |
| 2640 | IGTYP(IG) = 0 | CHD04160 |
| | JHDN = 1 | CHD04170 |
| | IBS(IG) = NCSN(IG) | CHD04180 |
| | GO TO 2660 | CHD04190 |
| 2644 | IGC = IGC+1 | CHD04200 |
| | IF (NZEN(NZON)-ND(NDC)) 2648,2646,2645 | CHD04210 |
| 2645 | IF (NCSN(IG) - ND(NDC)) 12646,12645,12645 | CHD04220 |
| 12645 | LANDID = 3 | CHD04230 |
| | NDC = NDC + 1 | CHD04240 |
| | NDCM=1 | CHD04250 |
| | IGLD=IG | CHD04260 |
| | GO TO 2648 | CHD04270 |
| 12646 | NSW = 2 | CHD04280 |
| | GO TO 2647 | CHD04290 |
| 2646 | NSW = 3 | CHD04300 |
| 2647 | NCEN(IG) = ND(NDC) | CHD04310 |
| | NDC = NDC+1 | CHD04320 |
| | NDCM = 2 | CHD04330 |
| | LANDID = 2 | CHD04340 |
| | GO TO 2655 | CHD04350 |
| 2648 | NCEN(IG) = NZEN(NZON) | CHD04360 |
| | IF (NZEN(NZON)-MNOD1) 2650,2651,2651 | CHD04370 |
| 2650 | NSW = 3 | CHD04380 |
| | GO TO 2655 | CHD04390 |
| 2651 | NBNST = NASW | CHD04400 |
| | NSW = 4 | CHD04410 |
| 2655 | IGTYP(IG) = NZON | CHD04420 |

| | |
|--------------------------------------|----------|
| JHDN = NHDN(NZON) | CHD04430 |
| IZG(NZON,IGC) = IG | CHD04440 |
| IZGT(NZON) = IGC | CHD04450 |
| IF (IGC-1, 2657,2657,2656 | CHD04460 |
| 2656 IBS(IG) = IBE(IG-1) | CHD04470 |
| GO TO 2658 | CHD04480 |
| 2657 IBS(IG) = IZB(NZON) | CHD04490 |
| 2658 IF (NZON-NRZON) 2660,2659,2660 | CHD04500 |
| 2659 NRSW(IG) = 3 | CHD04510 |
| NRID = 2 | CHD04520 |
| GO TO 2661 | CHD04530 |
| 2660 NRSW(IG) = NRID | CHD04540 |
| 2661 NSLAB(IG) = NCEN(IG)-NCSN(IG) | CHD04550 |
| NSLABH(IG) = NSLAB(IG)*JHDN | CHD04560 |
| IF (NSLARH(IG)-40) 2666,2666,2680 | CHD04570 |
| 26 NBND2(IG) = NBNDST | CHD04580 |
| IBE(IG) = IBS(IG)+NSLABH(IG) | CHD04590 |
| NDCM = 1 | CHD04600 |
| IF (LANDID-2) 2667,2669,2668 | CHD04610 |
| 2667 NLSW(IG) = 1 | CHD04620 |
| GO TO 2670 | CHD04630 |
| 2668 NLSW(IG) = 2 | CHD04640 |
| GO TO 2670 | CHD04650 |
| 2669 NLSW(IG) = 1 | CHD04660 |
| IGLD=IG+1 | CHD04670 |
| LANDID = 3 | CHD04680 |
| 2670 IGL = IG | CHD04690 |
| IG = IG+1 | CHD04700 |
| GO TO (2671,2672,2673,2675,2674),NSW | CHD04710 |
| 2671 NPBSW = 2 | CHD04720 |
| GO TO 2603 | CHD04730 |
| 2672 NCSN(IG) = NCEN(IGL) | CHD04740 |
| GO TO 2644. | CHD04750 |
| 2673 NZON = NZON+1 | CHD04760 |
| IGC = 0 | CHD04770 |
| 2674 NCSN(IG) = NCEN(IGL) | CHD04780 |
| GO TO 2625 | CHD04790 |
| 2675 MG = IGL | CHD04800 |
| NOF = IBE(IGL) | CHD04810 |
| GO TO 2685 | CHD04820 |
| 2680 NSLAB(IG) = 40/JHDN | CHD04830 |
| NCEN(IG) = NCSN(IG)+NSLAB(IG) | CHD04840 |
| NBND2(IG) = 5 | CHD04850 |
| NSLABH(IG) = NSLAB(IG)*JHDN | CHD04860 |
| IBE(IG) = IBS(IG)+NSLABH(IG) | CHD04870 |
| GO TO (12683,12682) +NDCM | CHD04880 |
| 12682 NDC = NDC - 1 | CHD04890 |
| NDCM = 1 | CHD04900 |
| 12683 CONTINUE | CHD04910 |
| IF (LANDID-2) 2682,2682,2683 | CHD04920 |
| 2682 NLSW(IG) = 1 | CHD04930 |
| GO TO 2684 | CHD04940 |
| 2683 NLSW(IG) = 2 | CHD04950 |
| 2684 IG = IG+1 | CHD04960 |
| NCSN(IG) = NCEN(IG-1) | CHD04970 |

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GO TO (2608,2625,2644,2644,2625),NSW CHD04980
C*** CALCULATION OF NODE WIDTHS FOR MINOR NODES CHD04990
C
2685 DO 2686 IG=1,MG CHD05000
NZON = IGTYP(IG) CHD05010
ONE = NHDN(NZON) CHD05020
JCSN = NCSN(IG) CHD05030
JCFNM = NCEN(IG)-1 CHD05040
DO 2686 K=JCSN,JCFNM CHD05050
DELTX(K) = DELX(K)/ONE CHD05060
DELTAX(K) = DELTX(K) CHD05070
CHD05080
CHD05090
2686 CONTINUE CHD05100
DELTX(JCFNM+1) = DELTX(JCFNM) CHD05110
DELTAX(JCFNM+1) = DELTAX(JCFNM) CHD05120
CHD05130
C*** CHECK COMMEX (DELTA TIME FROM CHAP) CHD05140
C*** AND RESET DTAU, PREDICTED TEMPERATURES, AND PREDICTED DENSITIES CHD05150
C*** IF DTAU LARGER THAN COMMEX CHD05160
C
12687 CONTINUE CHD05170
IGR=IZG(NRZON+1) CHD05180
IF (IGR-1)12688,12688,12689 CHD05190
12688 IGR=2 CHD05200
12689 CONTINUF CHD05210
BLPRES(N,L)=FONEV(TAU1,ISAVE2,TIME4,PP,NDOTS(4),1) CHD05220
CALL SUBZ (ZWALL,TEMPA1(NOF),BLPRES(N,L)) CHD05230
BLDEN(N,L)=BLPRES(N,L)*AIRM/(ZWALL*GCON*TEMPA1(NOF)) CHD05240
FLOW(N,L)=TBSTEP(TAU1,TIME4,FF,NDOTS(4)) CHD05250
FIN(L)=FONEV(TAU1,ISAVE2,TIME4,AST,NDOTS(4),1) CHD05270
HCONV(N,L)=FONEV(TAU1,ISAVE6,TIME3,RH,NDOTS(3),1) CHD05277
CFXO=0.71*BLDEN(N,L) CHD05278
CFXN=0.79*BLDEN(N,L) CHD05280
CALL FLOWS CHD05290
CALL DIFUS (DO ,1,DCOH ,CFXn ,AEPO) CHD05300
CALL DIFUS (DN ,2,DCOH ,CFXN ,AERN) CHD05310
CALL DIFUS (DH ,3,DCOH ,CFXH ,HYD) CHD05320
CALL DIFUS (DPY,4,DCOPY,CFXPY,PYRO) CHD05330
CALL DIFUS (DSI,6,DCOSI,CFXSI,SOX) CHD05340
CALL DIFUS (DCM,7,DCOCM,CFXC',BURN) CHD05350
CALL MOLWT CHD05360
2687 CONTINUF CHD05370
IF (TAOUT-TAU1-.99*DTAU) 2688,2690,2690 CHD05380
2688 DTF=(TAOUT-TAU1)/DTAU CHD05390
GO TO 3296 CHD05400
C
C*** SETUP OF COEFFICIENTS AND CALCULATION OF TEMPERATUR--2690-3370CHD05420
C
C*** ENTRANCE HERE FROM 3360+ FOR RECALC OF ALL GROUPS--DTAU/2 CHD05430
C
2690 NXSW = 1 CHD05440
ITFR = 1 CHD05450
ITERT = ITERT+1 CHD05460
IERR = 1 CHD05470
CHD05480
CHD05490
CHD05500

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C**** ENTRANCE HERE FROM 3275+ FOR RECALC OF ALL GROUPS CHD05510
C C CHD0520
2693 CONTINUF CHD05530
IG = 1 CHD05540
WFX = 0. CHD05550
FHTX = 0. CHD05560
PCX = 0. CHD05570
JBX = 0. CHD05580
EDFX = 0. CHD05590
WFDX=0. CHD05600
WRNX=0. CHD05610
WDEPX=0. CHD05620
WSIX=0. CHD05630
DEPX=0. CHD05643
DWFDX=0. CHD05647
C C CHD05648
C**** CALCULATION OF MASS RECEDITION RATES CHD05650
C C CHD05660
TEMPA = 0.5*(TEMPA1(NOF)+TEMPA9(NOF)) CHD05690
GAS = GAS1+DGAS*DTAUX CHD05700
CALL RECEED(TEMPA) CHD05710
I=MAT(NN) CHD05720
SLOP=1.12*SLOPE(I) CHD05730
CALL BLOCK(XMDOTC,TRCHAR,GAS,SLOP,HCONV(N,L),FLOW(N,L),PHI) CHD05740
REFCTR=1. CHD05750
PSI=PHI*F(N,L)*4632.5*0.5**((1.E4/TWALL(N+1)) CHD05760
EROC(1)=-3.672 CHD05770
EROC(2)=.3347 CHD05780
IF (PSI.LT.3.3) GO TO 4600 CHD05790
IF (PSI.GT.9.0) GO TO 4550 CHD05800
EROC(1)=-4.22915 CHD05810
EROC(2)= 1.34309 CHD05820
GO TO 4600 CHD05830
4550 EROC(1)=-9.04655 CHD05840
EROC(2)=6.36877 CHD05850
4600 PSI=ALOG10(PSI+1.E-15) CHD05860
ERODE=EROC(1)+PSI*(EROC(2)+PSI*(EROC(3)+PSI*EROC(4))) CHD05870
ERODE=(20./16.5)*10.*ERODE CHD05880
JRSW=NRSW(MG) CHD05890
GO TO (2694,2695,2694),JRSW
2694 CONTINUF
SDOTN=(-XMDOTC-ERODE)/(RHOC+RH02(NOF-1))*12.
GO TO 2692
2695 SDOTN=(-XMDOTC-ERODE)/(CARBN1(NOF-1)+SILCA1(NOF-1)+GRAF1(NOF-1))
1*12.
2692 CONTINUF
SDN = SDOTN*DTAU/2.
SN = SN1+SDN
C
C**** CHECK SIZE OF FRONT NODE AND ADJUST DTAU, IF CHD05900
C**** NECESSARY TO PREVENT TIME STEP BEING TOO LARGE CHD05910
C
IF (SN+SDN) 2269.,22710,22710 CHD05920
22696 DTF = -SN1/(2.*SDN) CHD05930
NCUT = 2 CHD05940
CHD05950
CHD05960
CHD05970
CHD05980
CHD05990
CHD06000
CHD06010
CHD06020
CHD06030

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GO TO 3296 CHD06040
22710 CONTINUE CHD06050
C CHD06060
TEMPA3(1) = 0.5*(TEMPA1(1)+TEMPA5(1)) CHD06070
C CHD06080
C**** CALCULATE DELTAX CHD06090
C CHD06100
DO 2696 J=IYS,MNOD CHD06110
2696 DELTAX(J) = DELTX(J)*SN CHD06120
C CHD06130
C**** ENTRANCE HERE FROM 3225+ FOR CALC OF NEXT GROUP CHD06140
C CHD06150
C**** GROUP INITIALIZATION CHD06160
C CHD06170
12696 JBS = IBS(IG) CHD06180
JBSM = JBS-1 CHD06190
JLSW = NLSW(IG) CHD06200
JRSW = NRSW(IG) CHD06210
JE1 = NC_APH(IG) CHD06220
JE = JE +1 CHD06230
JE2 = JE-1 CHD06240
ND1 = NBND1(IG)-3 CHD06250
ND2 = NBND2(IG) CHD06260
IGL = IG-1 CHD06270
JRF = IRF(IG) CHD06280
JBEM = JBE-1 CHD06290
JCEN = NCSN(IG) CHD06300
JCEN = -NCEN(IG) CHD06310
JCENM = JCEN-1 CHD06320
IGC = IGTYP(IG) CHD06330
JHDN = NHDN(IGC) CHD06340
JSLAB = NSLAB(IG) CHD06350
JBSPM = IBSPN+JCSN CHD06360
JBSPN = JBSPM-1 CHD06370
CHD06380
C TWO = SDN/(2*FCN) CHD06390
WFXX = WFX CHD06400
FHTXX = FHTX CHD06410
CONDXX = CONDX CHD06420
JBXX = JBX CHD06430
PCXX = PCX CHD06440
EDFXX=EDFX CHD06450
WFDX=WFDX CHD06460
WDEPXX=WDEPX CHD06470
WSIXX = WSIX CHD06480
WBRNXX=WBRNX CHD06490
DEPXX=DEPX CHD06503
DWFDXX=DWFD) CHD06507
C CHD06510
C**** SETUP OF NADD ARRAY (NUMBER OF CHD06520
C**** MAJOR NODES OF SAME MATERIAL AND WIDTH) CHD06530
C CHD06540
JX = 1 CHD06550
IY = JCSN CHD06560
IZ = JCENM-1 CHD06570

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12697 NADD(JX)=1 CHD06580
2697 IX = IY CHD06590
    IY = IX+1 CHD06600
    IF ((IX-IZ) 2698,2698,2702 CHD06610
2698 IF (DELTAX(IY)-DELTAX(IX)) 2701,2699,2701 CHD06620
2699 IF (MAT(IY)-MAT(IX)) 2701,2700,2701 CHD06630
2700 NADD(JX) = NADD(JX)+1 CHD06640
    GO TO 2697 CHD06650
2701 JX = JX+1 CHD06660
    GO TO 12697 CHD06670
C CHD06680
2702 GO TO (2708,2703),JLSW CHD06690
C CHD06700
C***      CALCULATION OF THE LANDAU MULTIPLYING FACTOR CHD06710
C CHD06720
2703 CONTINUE CHD06730
    KK = 0 CHD06740
    DO 2707 J=JCSN,JCFN CHD06750
        KK = KK+1 CHD06760
        I = KK CHD06770
        EMI(KK) = TWO*DISTL(J)/DELTX(J) CHD06780
        IF (J-JCEN) 2704,2707,2707 CHD06790
2704 K = 2 CHD06800
2705 IF (K-JHDN) 2706,2706,2707 CHD06810
2706 EMI(KK+1) = EMI(KK)+TWO CHD06820
    KK = KK+1 CHD06830
    K = K+1 CHD06840
    GO TO 2705 CHD06850
2707 EMI(I) = TWO*2.*DISTL(J)/(DELTX(J)+DELTX(J-1)) CHD06860
2708 CONTINUE CHD06870
C CHD06880
C***      ENTRANCE HERE FROM 3325+ FOR RECALC OF FRONT GROUP CHD06890
C***      CALCULATE TEMP A3 AND TEMP A4 CHD06900
C CHD06910
2710 DO 2711 J=2,JE CHD06920
    K = JBSM+J CHD06930
    TEMP A3(J) = 0.5*(TEMP A1(K)+TEMP A5(K)) CHD06940
2711 TEMP A4(J-1) = 0.5*(TEMP A3(J)+TEMP A3(J-1)) CHD06950
    TEMP A4(JF) = TEMP A3(JE) CHD06960
    NSTILL=1 CHD06970
    GO TO (2791,2712,2714),JRSW CHD06980
2712 I=MAT(JCSN) CHD06990
    IF (RHO1(JBS)-.01) 2791,2791,2714 CHD07000
2714 CONTINUE CHD07010
    NSTILL=2 CHD07020
    GO TO (2750,2716),JLSW CHD07030
2716 CONTINUE CHD07040
C CHD07050
C***      CALCULATION OF DFNSITY FOR LANDAU GROUP CHD07060
C CHD07070
    K = 0 CHD07080
    KL = JBSM CHD07090
    I = MAT(JCSN) CHD07100
    KK = JBSPM+JSLAB CHD07110
2720 K = K+1 CHD07120

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        KL = KL+1                               CHD07130
        CALL RHOSB (K,KL)                      CHD07140
        IF (K-1) 2720,2720,2732                CHD07150
2732 IF (K-JE1) 2734,2733,2736            CHD07160
2733 RHO1(KL+1) = RHO1(KK)                CHD07170
        RHO5(KL+1)=RHO5(KK)
2734 D(K) = (RHO1(KL+1)-RHO1(KL-1))*EMI(K)+RHO1(KL)*EMBM(K)+AREAC(K) CHD07180
        1*DTAU                                CHD07190
        GO TO 2720                            CHD07200
2736 ONE = EMBM(K)-3.*EMI(K)             CHD07210
        C(K) = 4.*EMI(K)/ONE                  CHD07220
        D(K) = ((EMBM(K)+3.*EMI(K))*RHO1(KL)-(4.*RHO1(KL-1) CHD07240
        1-RHO1(KL-2))*EMI(K)+AREAC(K)*DTAU)/ONE
        THREE = -EMI(K)/ONE                  CHD07250
        K = K-1                                CHD07260
        TWO = EMBM(K)+EMI(K)*C(K+1)           CHD07270
        C(K) = EMI(K)*(1.+THREE)/TWO          CHD07280
        D(K) = (D(K)+EMI(K)*D(K+1))/TWO       CHD07290
2737 K = K-1                                CHD07300
        IF (K-1) 2740,2740,2738            CHD07310
2738 ONE = EMBM(K)+C(K+1)*EMI(K)          CHD07320
        C(K) = EMI(K)/ONE                  CHD07330
        D(K) = (D(K)+D(K+1)*EMI(K))/ONE      CHD07340
        GO TO 2737                            CHD07350
2740 RHO5(JBS) = RHO1(JBS)+AREAC(1)*DTAU/EMBM(1) CHD07360
        KL = JBS                                CHD07370
        DO 2742 K=2,JE1                      CHD07380
        KL = KL+1                                CHD07390
2742 RHO5(KL) = D(K)-C(K)*RHO5(KL-1)      CHD07400
        RHO5(KK) = D(JE)-C(JE)*RHO5(KL)-RHO5(KL-1)*THREE
        GO TO 2774                                CHD07410
C
C**** CALCULATION OF DENSITY FOR REGULAR GROUP
C
2750 IX = 0                                CHD07420
        K = 0                                  CHD07430
        KL = JBSM                             CHD07440
        KK = JBSPM                           CHD07450
        IM = JCSN                            CHD07460
2760 IX = IX+1                            CHD07470
        I = MAT(IM)                          CHD07480
        IM = IM+NADD(IX)                     CHD07490
        IJ = JHDN*NADD(IX)                   CHD07500
        KK = KK+NADD(IX)                     CHD07510
        DO 2763 J=1,IJ                      CHD07520
        K = K+1                                CHD07530
        KL = KL+1                            CHD07540
        IF (RHO1(KL)-.01*RHOV(1)) 2761,2761,2767
2761 RHO1(KL)=0.                         CHD07550
        RHO5(KL)=0.
        GO TO 2763                            CHD07560
2762 CONTINUE                            CHD07570
        CALL RHOSB(K,KL)                      CHD07580
        RHO5(KL)=RHO1(KL)+AREAC(K)/EMBM(K)*DTAU
2763 CONTINUE                            CHD07590

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K=K+1
CALL RHOSBIK,KK)
RH05(KK) = RH01(KK)+AREAC(K)/EMBM(K)*DTAU
K=K-1
IF (IM-JCEN) 2760,2764,2764
2764 CONTINUE
C
C**** CHECK TO SEE THAT RH05 IS GREATER THAN ZEROS CALCULATE
C**** RH03, RH04, GAS FLOW, AND REACTION HEAT
C
2774 IX = 0
K = 0
IJ=0
IK=JHDN
KK = JBSPL
KL = JUSM
IM = JCSN
2775 IX = IX+1
I = MAT(IM)
IJ=IJ+JHDN*NADD(IX)
12775 KK = KK+1
2776 K = K+1
KL = KL+1
IF (RH05(KL)=.01) 2777,2778,2778
2777 RH05(KL) = 0.
2778 RH03(K) = (RH01(KL)+RH05(KL))/2.
GO TO (12779,2779),JLSW
12779 WFP = (RH01(KL) - RH05(KL))/DTAU
GO TO 2780
2779 WFP = RATE(KL)*(RH01(KL)-RH05(KL))-AREAC(K)
2780 WFD(KL)=WFP*DELTAX(IM)*AREAV(K)/12.
TEMPA = TEMPAA(K)
TWO = HDA(5,I)+(HDA(1,I)+(HDA(2,I)+(HDA(3,I)+HDA(4,I)
1*TEMPA)*TEMPA)*TEMPA)*TFMPA
IF (K-1) 2781,2781,2782
2781 ONE = 0.5*WFD(KL)
WFD(KL)=WFDX+ONE
WF(KL) = WFX+ONE
FHT(K) = FHTX-ONE*TWO
GO TO 2783
2782 RH04(K-1) = (RH03(K-1)+RH03(K))/2.
FHT(K) = -TWO*WFD(KL)
WF(KL) = WF(KL-1)+WFD(KL)
2783 IF (K-IK) 2776,12783,12783
12783 CONTINUE
IK = IK+JHDN
IF (K-IJ) 12784,2784,2784
12784 RH05(KK) = RH05(KL+1)
IF (RH05(KK)=.01) 12785,12786,12786
12785 RH05(KK) = 0.
12786 CONTINUE
GO TO 12775
2784 IF (RH05(KK)=.01) 2785,2786,2786
2785 RH05(KK) = 0.
2786 RH03(KK) = (RH01(KK)+RH05(KK))/2.

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RHO4(K) = (RHO3(K)+RHO5(KK))/2.
GO TO (12787,2787),JLSW
12787 WFP = (RHO1(KK)-RHO5(KK))/DTAU
GO TO 2788
2787 WFP = RATE(KL+1)*(RHO1(KK)-RHO5(KK))-AREAC(K+1)
2788 ONE=WFP*0.5*DELTAX(IM)*AREAV(K+1)/12.
WFX = WF(KL)+ONE
WFDX=ONE
TFMPA = TEMPA3(K+1)
TWO = HDA(5,I)+(HDA(1,I)+(HDA(2,I)+(HDA(3,I)+HDA(4,I)
1*(TFMPA)*TEMPA)*TFMPA)*TFMPA
FHTX = -ONE*TWO
IM = IM+NADD(IX)
IF ((IM-JCENM) 2775,2775,2780
2789 WF(JBE) = WFX
WFD(JBE)=WFDX
GO TO 3000
C
2791 DO 2793 J=1,JE
K = JBSM+J
RHO3(J) = RHO5(K)
2793 RHO4(J) = RHO5(K)
GO TO (2794,2797,3000),JRSW
2794 DO 2795 J=JRS,JBE
WFD(J)=0.
2795 WF(J) = 0
GO TO 3000
2797 DO 2798 J=JBS,JBE
WFD(J)=0.
2798 WF(J) = WFX
WFD(JRS)=WFDX
3000 CONTINUF .
C
C***   CALCULATION OF DEPOSITION AND OTHER REACTIONS
C
DWFDX=DWFDX+.3767*(WFX-WFXX)
GO TO (4990,5000,4990),JRSW
4990 DO 4995 J=JBS,JBE
WBRN(J)=0.
WSI(J)=0.
WDEP(J)=0.
4995 CONTINUF
GO TO 5110
5000 CONTINUE
KL=JBSM
DEL=0.
SAVE= 0.
DELA = DELTAX(JCEN)
DELTAX(JCEN) = 0.
DO 5100 J=1,JE
KL=KL+1
TEMPA=TEMPA3(J)
K=LLD(KL)
WF(KL)=WF(KL)+SAVE
DACT=DWFDX-DEPX

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CALL SIC (K,KL,TEMPA+DEL)
CALL DFPO (K,KL,TFMPA+DFL)
DEPX=DEPX+1.3333*WDEP(KL)
ONE=DWFDX-DEPX
IF (ONE) 3090,5092,5092
5090 WDFP(KL)=WDEP(KL)+.75*ONE
DEPX=DWFDX
5092 CONTINUE
HOW=W$1(KL)-WDEP(KL)+WBRN(KL)
WF(KL)=WF(KL)+HOW
SAVE=SAVE+HOW
DFL=DFLTAX(K)
5100 CONTINUE
GO TO (5108,5101),JLSW
5101 CONTINUE
K=0
EF=7.*SDN/SN1
DO 5102 J=JBS+JBEM
K=K+1
EK=K
EK=EK+EF
SILCAS(J+1)=SILCAS(J+1)*(1.+EK)-SILCAS(J)*EK
CARBN5(J+1)=CARBN5(J+1)*(1.+EK)-CARBN5(J)*EK
5102 CONTINUE
5108 CONTINUE
DELTAX(JCEN)=DELA
WDEP(JBS)=WDEP(JBS)+WDEPX
WSI(JBS)=WSI(JBS)+WSIX
WBRN(JBS)=WBRN(JBS)+WBRNX
5110 CONTINUE
WDFPX=WDFP(JBE)
WSIX=WSI(JBE)
WBRNX=WBRN(JBE)
WFX=WF(JBE)
5400 CONTINUE
C
C***** CALCULATION OF THERMAL CAPACITY, CONDUCTIVITY, ENERGY DEPOSITION C
C
IX = 0
K = 0
KK = JBSPM
K1 = 1
IM = JCSN
3005 IX = IX+1
I = MAT(IM)
IJ = JHDN*NADD(IX)
KK = KK+NADD(IX)
DO 3015 J=1,IJ
K = K+1
PC(K) = PCAPF(K)
EDFLUX(K)=EDFLUX(K)*DELTAX(IM)/12.*IRHOV(I)+RHOC
COND(K)=COND(F(K))
IY=JBS+K
QCOND(IY)=2.*COND(K)*(ITEMPA3(K+1)-TEMPA3(K))
3015 CONTINUE

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PC(K1) = (PCX+PC(K1))/2. CHD09230
EDFLUX(K1)=(EDFX+EDFLUX(K1))/2. CHD09240
K1 = K+1 CHD09250
ONE = RH03(K1) CHD09260
RH03(K1) = RH03(KK) CHD09270
PCX = PCAPF(K1) CHD09280
EDFX=EDFLUX(K1)*DELTAX(IM)/12.*(RHOV(I)+PHOC) CHD09290
RH03(K1) = ONE CHD09300
IM = IM+NADD(IX) CHD09310
IF (IM-JCFN) 3005,3031,3031 CHD09320
3031 JBX = JRSM+K CHD09330
CONDX = COND(K) CHD09340
C CHD09350
C**** CALCULATION OF MATRIX ELEMENTS CHD09360
C CHD09370
3040 TEMPA1(JBSM) = TEMPA1(JBXX) CHD09380
J = 0 CHD09390
COND(J) = CONDXX CHD09400
WF(JBSM) = WF(JBXX) CHD09410
DO 3060 J=1,JE1 CHD09420
IX = J+JRSM CHD09430
IPLUS = IX+1 CHD09440
INFG = IX-1 CHD09450
CALL CPRA (J,IX,TEMPA3(J),CPBAR) CHD09460
GAGC = -WF(INEG)*CPRAR/4. CHD09470
GO TO (3046,3045),JLSW CHD09480
3045 GAGC = GAGC+PC(J)*EMI(J) CHD09490
3046 C(J) = GAGC+COND(J) CHD09500
A(J) = -GAGC+COND(J-1) CHD09510
GK = A(J)+C(J) CHD09520
D(J) = C(J)*TEMPA1(IPLUS)+(PC(J)-GK)*TEMPA1(IX) CHD09530
1+A(J)*TEMPA1(INEG)+EDFLUX(J) CHD09540
R(J) = PC(J)+GK CHD09550
GO TO (3060,3052,3046),JRSW CHD09560
3052 CONTINUE CHD09570
D(J)=D(J)+WDEP(IX)*QDEP+WSI(IX)*QSI+WRN(IX)*QBRN CHD09580
GO TO (3060,3056),NSTILL CHD09590
3056 D(J) = D(J)+FHT(J) CHD09600
3060 CONTINUE CHD09610
C CHD09620
C**** DIRECTOR--STARTING BOUNDARY OF GROUP CHD09630
C*** 1--(3115)--FIXED TEMP (BOUNDARY FOR PROBLEM START IN INTERIOR) CHD09640
C*** 2--(3120)--INTERIOR (NORMAL TYPE FOR BOUNDARY BETWEEN GROUPS) CHD09650
C*** 3--(3105)--FLUX DRIVE (BACK SURFACE) CHD09660
C*** 4--(3110)--TEMP DRIVE (BACK SURFACE) CHD09670
C CHD09680
GO TO (3115,3120,3105,3110),JBND1 CHD09690
3105 D(1)=COND(1)*TEMPA1(JBS+1)+(PC(1)-COND(1))*TEMPA1(JBS) CHD09700
ONE = PC(1)+COND(1) CHD09720
CC(JBS) = -COND(1)/ONE CHD09730
DD(JBS) = C(1)/ONE CHD09740
GO TO 3200 CHD09750
3110 SBK = 2.*COND(1) CHD09760
3115 CC(JBS) = 0. CHD09770
DD(JBS) = TEMPA2(JBS) CHD09780

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GO TO 3200                               CHD09790
C*** INTERIOR BOUNDARY                  CHD09800
3120 ONE = B(J)+A(1)*CC(JBXX)           CHD09810
    CC(JBS1) = -C(1)/ONE                 CHD09820
    DD(JBS1) = (D(1)+A(1)*DD(JBXX))/ONE   CHD09850
3200 DO 3202 J=2,JE1                   CHD09840
    K = JRSM+J                           CHD09850
    ONE = B(J)+A(J)*CC(K-1)             CHD09860
    CC(K) = -C(J)/ONE                  CHD09870
3202 DD(K) = (D(J)+A(J)*DD(K-1))/ONE   CHD09880
C                                         CHD09890
C*** DIRECTOR--ENDING BOUNDARY OF GROUP  CHD09900
C*** 1--(3240)--FLUX DRIVE (FRONT SURFACE) CHD09910
C*** 2--(3260)--TEMP DRIVE (FRONT SURFACE) CHD09920
C*** 3--(3260)--NOT IN USE              CHD09930
C*** 4--(3225)--FIXED TEMP (BOUNDARY FOR PROBLEM END IN INTERIOR) CHD09940
C*** 5--(3225)--INTERIOR (NORMAL TYPE FOR BOUNDARY BETWEEN GROUPS) CHD09950
C                                         CHD09960
GO TO (3240,3210,3260,3225,3225),JBND2  CHD09970
3210 TEMPA5(NOF)=FONEV(TAU2,ISAVE1,TIME3,TT,NDOTS(3)+1)  CHD09980
GO TO 3260                               CHD09990
3225 IG = IG+1                          CHD10000
    TEMPA3(1) = TEMPA3(JE)               CHD10010
GO TO 12696                             CHD10020
3240 PC(JE) = PCX                        CHD10030
    EDFLUX(JE)=EDFX                    CHD10040
    CALL CPRA (JE,NOF,TFMPA3(JE),CPBAR)  CHD10050
    GAGC = -WF(NOF-1)*CPBAR/4.+PC(JE)*EMI(JE)  CHD10060
    IX = IBSPM+JCENM                  CHD10070
    IM = JCENM                         CHD10080
    TEMPA4(JE) = TEMPA3(JE)            CHD10090
    RHO4(JE) = .103(IX)                CHD10100
    I = MAT(JCENM)                   CHD10110
    COND(JE)=COND(JE)                 CHD10120
    QCOND(NOF+1)=4.*COND(JE)*(TEMPA3(JE)-TEMPA4(JE))  CHD10130
    A(JE) = -GAGC+COND(JE)            CHD10140
    C(JE) = GAGC+COND(JE)            CHD10150
    GK = A(JE)+C(JE)                 CHD10160
    B(JE) = PC(JE)+GK                CHD10170
    GX = .25*(COND(JE)+COND(JE))     CHD10180
C                                         CHD10190
C                                         CHD10200
C*** CALCULATION OF FRONT SURFACE HEAT INPUT  CHD10210
C                                         CHD10220
C                                         CHD10230
TEMPA = 0.5*(TEMPA1(NOF)+TEMPA5(NOF))  CHD10240
I = MAT(NN)                            CHD10250
IX = 1                                 CHD10260
13239 CONTINUF                         CHD10270
    KK=IBSPN+MNOD                     CHD10280
    IF (RHO1(KK)=.98*RHOV(I)) 13240,13241,13241  CHD10290
13240 ONE = ARSC                      CHD10300
    TWO = EMISC                      CHD10310
    GO TO 13242                      CHD10320
13241 ONF = ARSORP(I)                 CHD10330

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TWO = EMIS(1)
13242 QBYRAD=TWO*.481E-12*TEMPA**4 CHD10340
      TIME=TAU1 CHD10350
      CALL GPCOM CHD10355
      XCOM=XMDOTL+XMDOTG*(DIFREC-1.711) CHD10360
      IF(XCOM)3241,3242,3242 CHD10370
      3241 XCOM=0. CHD10380
      3242 QCOMB=HCOM*XCOM CHD10390
      QSURL=HSUB*XMDOTS CHD10400
      XIR(N,L)=FONEV(TAU1,ISAVE4,TIME3,XRI,NDOTS(3),1) CHD10410
      QMISC=FONEV(TAU1,ISAVE5,TIME3,QMU,NDOTS(3),1) CHD10420
      HCONV(N,L)=FONEV(TAU1,ISAVE6,TIME3,RH,NDOTS(3),1) CHD10430
      QTOT = QMISC+QCOMB-QSURL+QGPCOM CHD10440
      CALL SUBZ (ZWALL,TEMPA,BLPRES(N,L)) CHD10450
      CALL IWR (ZWALL,TEMPA,X1) CHD10460
      QCONV(N,L) = HCONV(N,L)*(XIR(N,L)-X1) CHD10470
      QTOTAL = QTOT+ONE*QGAS(N,L)+PHI*QCONV(N,L)-QBYRAD CHD10480
      QTOTAL=QTOTAL*AREA(JE) CHD10490
      GO TO (13243,13244),IX CHD10500
13243 CONTINUE CHD10510
      QSAVE = QTOTAL CHD10520
      TEMPA = TEMPA+10. CHD10530
      CALL RECFED(TEMPA) CHD10540
      IX=2 CHD10550
      GO TO 13242 CHD10560
13244 CONTINUF CHD10570
      DQ = -(QTOTAL-QSAVE)/10. CHD10580
      GZ = DQ/2. CHD10590
      GY = QSAVE+GZ*TEMPA5(NOF) CHD10600
      ONE = C(JE)/GX CHD10610
      D(JE)=(PC(JE)-GK)*TEMPA1(NOF)+GK*TEMPA1(NOF-1)+ONE*GY+EDFLUX(JE) CHD10620
      GO TO (3244,3246,3243),JRSW CHD10630
3246 GO TO (3247,3243),NSTILL CHD10640
3247 D(JE) = D(JE)+2.*FHTX CHD10650
3248 CONTINUE CHD10660
      D(JE)=D(JE)+2.*(WDEP(NOF)*QDEP+WS(NOF)*QSI+WBRN(NOF)*QBRN) CHD10670
3249 ONE = B(JE)+ONE*GZ+GK*CC(NOF-1) CHD10680
C
C*** TEMPERATURE CHECK AND DETERMINATION OF DIRECTION CHD10690
C*** OF FURTHER CALCULATION CHD10700
C
C. CALCULATION AND CHECK OF SURFACE TEMPERATURE CHD10710
C
      ABVALS = 0. CHD10720
      ABVALM = 0. CHD10730
      TEMPA = TEMPAS(NOF) CHD10740
      TEMPAS(NOF) = (D(JE)+GK*DD(NOF-1))/ONE CHD10750
      ABVAL = ABS((TEMPAS(NOF)-TEMPA)/TEMPA) CHD10760
      ETAS=AMIN1(ETA,40./TEMPA) CHD10770
      IF (ABVAL-ABVALS) 1*246,13246,13245 CHD10780
13245 ABVALS = ABVAL CHD10790
13246 CONTINUE CHD10800
      IF(ABVAL-ETAS)3260,3260,3245 CHD10810
3245 IERR = 2 CHD10820
      IF (TEMPAS(NOF)) 3250,3260,3260 CHD10830

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3250 TEMPAS(NOF) = 10.
C      CALCULATION AND CHECK OF TEMPERATURES
3260 IGT = IG2
GAS=WFX
DGHS=(GAS-GAS1)/DTAUX
3261 DO 3265 I=1,JE1
J = IBE(IG)-1
K = J+1
TEMPA5 = TEMPAS(J)
TEMPAS(J) = DD(J)-CC(J)*TEMPAS(K)
ABVAL = ABS((TEMPA5(J)-TEMPA5)/TEMPA5)
IF (ABVAL-ABVALS) 13262,13262,13261
13261 ABVALS = ABVAL
13262 CONTINUE
GO TO (3262,3265),IERR
3262 CONTINUE
IF (ABVAL-ETA) 3265,3265,3263
3263 FRR = 2
IF (TEMPA5(J)) 3264,3265,3265
3264 TEMPAS(J) = 10.
3265 CONTINUE
IF (IG-MG) 3267,3266,3266
3266 ABVALM = ABVALS
ABVALS = 0.
3267 CONTINUE
GO TO (3270,3274),NXSW
3270 NXSW = 2
IX = 1
GO TO (3274,3375),IERR
3274 IF (IG-IGT) 3275,3275,3277
3275 IF (IGL) 3278,3278,3276
3276 IGT = 1
3277 IX = IBE(IGL)
JBS = IBS(IGL)
TEMPA5(IX) = TEMPAS(JBS)
IG = IGL
IGL = IGL-1
JE1 = NSLABH(IG)
GO TO 3261
3278 GO TO (3280,3290), IFRR
C
C*** NO ERROR IN TEMPERATURES--DETERMINE NEW TIME STEP
C
3280 ONE = ETA*DTAU
IF (ITER-2) 3282,3285,3287
3282 IF (ABVALM-1.1*ABVALS) 3283,3284,3284
3283 DTAUC = 0.80*ONE/ABVALS
GO TO 3400
3284 DTAUC = 1.0*ONE/(ABVALM+1E-6)
GO TO 3400
3285 C,AUC=ONE/AMAX1(ABVAL,3,ABVALM+1E-6)
3287 DTAUC = 0.80*DTAUC
GO TO 3400
C
C*** ERROR IN TEMPERATURES--REITERATE OR CUT TIME STEP

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C**** AND RESTART ON CALCULATION
C
3240 CONTINUF
    IF (ITER-3) 3370,3295,3295
3295 DTF = ETA/AMAX1(ABVALS,ABVALM)
    IF (DTF-.5) 13295,13297,13296
13295 DTF = .25
    GO TO 13297
13296 DTF = 0.5
13297 CONTINUF
C
C****      RESET OF DTAU, PREDICTED TEMPERATURES, AND PREDICTED DENSITIES
C
3296 CONTINUF
    ONE = DTF*DTAU
    TWO = DTAU-ONE
    TAU2 = TAU2-TWO
    DTAU = ONE
    DTAUX = DTAUX-TWO/2.
    DTAUC = DTAU
3340 DO 3360 I=1, MG
    JBS = IBS(I)
    JBE = IBE(I)
    DO 3350 J=JBS,JBE
        TEMP2(J) = TEMP1(J)+DTF*(TEMP2(J)-TEMPA1(J))
3350 TEMP4(J) = TEMP2(J)
    IF (NRSW(I)-3) 3360,3355,3360
3355 DO 3356 J=JBS,JBE
    RHO2(J) = RHO1(J)+DTF*(RHO2(J)-RHO1(J))
3356 RHO5(J) = RHO2(J)
    JBS = IBSPM+NCSN(IG)
    JBF = JBS+NSLAB(IG)-1
    DO 3357 J=JBS,JBE
        RHO2(J) = RHO1(J)+DTF*(RHO2(J)-RHO1(J))
3357 RHO5(J) = RHO2(J)
3360 CONTINUE
    GO TO 2690
3370 IG=1
    IX = 2
3375 IERR=1
    ITER = ITER+1
    ITERT = ITERT+1
    GO TO (3395,1693),IX
3395 CONTINUE
    JBS = IBS(MG)
    TEMP3(1) = 0.5*(TEMP1(JBS)+TEMPA3(JBS))
    WFX = WFXX
    FHTX = FHTXX
    CONDX = CONDXX
    JRX = JRXX
    PCX = PCXX
    EDFX=EDFXX
    WFDX=WFDXX
    WDEPX=WDEPXX
    WSIX = WSIXX
CHD11430
CHD11440
CHD11450
CHD11460
CHD11470
CHD11480
CHD11490
CHD11500
CHD11510
CHD11520
CHD11530
CHD11540
CHD11550
CHD11560
CHD11570
CHD11580
CHD11590
CHD11600
CHD11610
CHD11620
CHD11630
CHD11640
CHD11650
CHD11660
CHD11670
CHD11680
CHD11690
CHD11700
CHD11710
CHD11720
CHD11730
CHD11740
CHD11750
CHD11760
CHD11770
CHD11780
CHD11790
CHD11800
CHD11810
CHD11820
CHD11830
CHD11840
CHD11850
CHD11860
CHD11870
CHD11880
CHD11890
CHD11900
CHD11910
CHD11920
CHD11930
CHD11940
CHD11950
CHD11960
CHD11970

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WBRNX=WBRNXX          CHD11980
DFPX=DFPXX            CHD11993
DWFDX=DWFDXX          CHD11997
GO TO 2710            CHD11998
C                      CHD12000
C*** NEW TIME STEP    CHD12010
C                      CHD12020
3400 CONTINUE          CHD12030
C                      CHD12040
C*** SETTING OF TIMES AND DELTA TIMES CHD12050
C                      CHD12060
      DTAUS = DTAU      CHD12070
      NOTIME = NOTIME+1 CHD12080
3424 CONTINUE          CHD12090
3426 DTAU = DTAUC     CHD12100
IF (TAU2+1.1*DTAU-TAUOUT) 3500,3427,3427
3427 TAU2S=1.0000001*TAU2 CHD12110
IF (TAU2S-TAUOUT) 3428,3430,3430
3428 DTAU = TAUOUT-TAU2 CHD12120
GO TO 3500            CHD12130
3430 TAU2 = TAUOUT    CHD12140
NPTSW = 2              CHD12150
3432 TAUOUT = TAU2+COMMEX CHD12160
GO TO 3424            CHD12170
3.00 CONTINUE          CHD12180
TAU1 = TAU2            CHD12190
TAU2 = TAU2+DTAU       CHD12200
DTAUX = 0.5*(DTAU+DTAUS) CHD12210
C                      CHD12220
C*** CALCULATION OF SURFACE DISTANCE AT J AND SETTING OF GAS AT J-1/2 CHD12230
C                      CHD12240
      SN1 = SN+SDN      CHD12250
      GAS1 = GAS          CHD12260
C                      C. 2270
C*** PREDICTIONS OF TEMPERATURES AND DENSITIES FOR NEXT STEP. CHD12270
C*** PLACEMENT OF VALUES INTO BASIC NODES CHD12280
C                      CHD12290
      DO 3505 J=1,2      CHD12300
      TAUST(J) = TAUST(J+1) CHD12310
      TEMPST(J) = TEMPST(J+1) CHD12320
3505 DTR(J) = DTR(J+1) CHD12330
      TAUST(1) = TAU1      CHD12340
      TEMPST(1) = TEMPAS(NOF) CHD12350
      IF (TAUST(1)-1.001*TAUST(1)) 3509,3509,3508
13508 CONTINUE          CHD12360
      PTR(1) = (TEMPAS(NOF)-TEMPA1(NOF))/DTAUS CHD12370
      IF (DTR(1)-DTR(2)) 3506,3509,3507 CHD12380
3506 IF (DTR(2)-DTR(1)) 3509,3309,3508 CHD12390
3507 IF (DTR(2)-DTR(1)) 3508,3509,3509 CHD12400
3508 CONTINUE          CHD12410
      TEMPST(1) = (TEMPST(2)+TEMPST(3)+(TEMPST(3)-TEMPST(1)) CHD12420
      1*(TAUST(3)-(AUST(2))/(TAUST(3)-TAUST(1)))/2. CHD12430
      TEMPAS(NOF) = TEMPST(1) CHD12440
      DTR(1) = (TEMPAS(NOF)-TEMPA1(NOF))/DTAUS CHD12450
3509 CONTINUE          CHD12460

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JRF=1                               CHD12510
DO 23504 IG=1, MG                 CHD12520
JBS=IBS(IG)                         CHD12530
JBEX=JRE                            CHD12540
JBF=IBE(IG)                         CHD12550
JBEM=JBE-1                           CHD12560
QCOND(JBS)=QCOND(JRFX)             CHD12570
K=NCSN(IG)-1                         CHD12580
IF (IGTYP(IG) 123505, 23504, 23503 CHD12590
23503 DO 23504 J=JBS, JREM, JHDN   CHD12600
K=K+1                               CHD12610
23504 QCOND(K)=QCOND(J)            CHD12620
23505 QCOND(JBEX)=QCOND(JBS)       CHD12630
QCOND(NOF)=QCOND(NOF+1)             CHD12640
QCOND(MNOD)=QCOND(NOF)              CHD12650
QCOND(1)=QBACK                      CHD12660
JBS=IRS(1)                           CHD12670
QCOND(JBS)=QBACK                   CHD12680
3510 TWO = DTAU/DTAUS               CHD12690
ONE = 1.+TWO                          CHD12700
JBE = 0                               CHD12710
DO 3526 IG=1, MG                   CHD12720
JBS = IBS(IG)                         CHD12730
IF (JBS-JBE) 13511, 13510, 13511   CHD12740
13510 KK = JBS+1                     CHD12750
GO TO 13512                         CHD12760
13511 KK = JBS                      CHD12770
13512 CONTINUJF                      CHD12780
JBE = IBE(IG)                        CHD12790
JBEM = JRE-1,                         CHD12800
DO 3511 J=KK, JBE                  CHD12810
SILCA1(J)=SILCA5(J)                 CHD12820
CARBN1(J)=CARBN5(J)                 CHD12830
GRAF1(J)=GRAFS(J)                  CHD12840
TEMPA2(J) = ONE*TEMPA5(J)-TWO*TEMPA1(J) CHD12850
TEMPA1(J) = TEMPAS(J)                CHD12860
3511 TEMPAS(J) = TEMPAS2(J)          CHD12870
IX = IGTYP(IG)                      CHD12880
IF (IX) 3317, 3517, 3514            CHD12890
3514 JHDN = NHDN(IX)                CHD12900
3515 JCSN = NCSN(IG)                CHD12910
JCSNM = JCSN-1                      CHD12920
K = JCSNM                           CHD12930
JCEN = NCEN(IG)                     CHD12940
DO 3516 J=JBS, JBEM, JHDN          CHD12950
K = K+1                             CHD12960
WFD(K)=WFD(J)                      CHD12970
SILCA1(K)=SILCA1(J)                 CHD12980
CARBN1(K)=CARBN1(J)                 CHD12990
GRAF1(K)=GRAF1(J)                  CHD13000
TEMPA1(K) = TEMPAS1(J)              CHD13010
WF(K) = WF(J)                       CHD13020
TEMPA2(K) = TEMPAS2(J)              CHD13030
3516 TEMPAS(K) = TEMPAS2(J)          CHD13040
3517 IF (NRSW(IG)-2) 3526, 3518, 3518   CHD13050

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3518 CONTINUF
3519 IX = 1
3520 DO 1523 J=JRS+JBEM
    RH02(J) = ONE*RHO5(J)-TWO*RHO1(J)
    IF (RH02(J)) 3521,3522,3522
3521 RH02(J) = 0.
3522 RH01(J) = RH05(J)
3523 RH05(J) = RH02(J)
    GO TO (3524,3526),IX
3524 K = JCSNM
    DO 3525 J=JRS+JBEM+JHDN
        K = K+1
        RH01(K) = RH01(J)
        RH02(K) = RH02(J)
3525 RH05(K) = RH05(J)
    JBS = JCSN+IBSPM
    JBEM = JCEN+IBSPN
    IX = 2
    GO TO 3520
3526 CONTINUE
    WFD(MNOD)=WFD(NOF)
    WDEP(MNOD)=WDEP(NOF)
    WS1(MNOD)=WS1(NOF)
    WBRN(MNOD)=WBRN(NOF)
    WDEP(NH)=WDEP(NOF-4)
    WS1(NN)=WS1(NOF-4)
    WBRN(NN)=WBRN(NOF-4)
    TFMPA1(MNOD)=TEMPA1(NOF)
    TEMPAA2(MNOD)=TEMPA2(NOF)
    TEMPAA3(MNOD)=TEMPA3(NOF)
    GRAF1(MNOD)=GRAF1(NOF)
    SILCA1(MNOD)=SILCA1(NOF)
    CARBN1(MNOD)=CARBN1(NOF)
    WF(MNOD)=WF(NOF)
    GO TO (13529,13525),NPTSW
13525 CONTINUE
    NPTSW = 1
    DO 13526 J=1,153
        DD(J) = RH05(J)
        CC(J) = RH05(J+152)
13526 CONTINUF
    DO 14000 J=1,203
14000 RH05(J)=RH05(J)+SILCA1(J)+CARBN1(J)+GRAF1(J)
    DO 14001 J=205,305
14001 RH05(J)=RH05(J)+SILCA1(J-203)+CARBN1(J-203)+GRAF1(J-203)
    RH05(IBSPM) = 0.
    NRDIV = NHDN(1)
    NRGO = NZSN(1)
    NKEND = NZEN(1)
    TWALL(N,L) = TEMPAA1(NOF)
    XLEFT(MNOD) = SN1+XLEFT(IYSI)
    RETURN
13527 CONTINUE
    DO 13528 J=1,153
        RH05(J) = DD(J)

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13528 RH05(J+152) = CC(J) CHD13610
13529 CONTINUE CHD13620
C CHD13630
C*** FRONT CONTROL CHD13640
C CHD13650
C IF (SN1-SCHECK) 13530,13530,13531 CHD13660
13530 CONTINUE CHD13670
CALL FRONT CHD13680
MARK = 2 CHD13690
13531 CONTINUE CHD13700
IF (NZONC-1) 2687,23529,2687 CHD13710
23529 CONTINUE CHD13720
C CHD13730
C*** CHECK LOCATION OF REACTION ZONE CHD13740
C CHD13750
C CHD13760
IGR = IZG(NRZON,1) CHD13770
JX = IZGT(NRZON) CHD13780
IGRL = IZG(NRZON,JX) CHD13790
IG = IGRL CHD13800
JHDN = NHDN(NRZON) CHD13810
IM = NCSN(IGR) CHD13820
I = MAT(IM) CHD13830
JBS = IBS(IGR) CHD13840
JBF = IBF(IGR) CHD13850
JBEM = JBE-1 CHD13860
JHDN1 = JHDN+1 CHD13870
IF (RH01(JBS)-.03*RHOV(1)) 23527,23527,23528 CHD13880
23527 IN1 = JBS-1 CHD13890
GO TO 3530 CHD13900
23528 CONTINUE CHD13910
KL = 0 CHD13920
DO 3528 J=JBS,JBEM CHD13930
IM = (KL/JHDN)+NCSN(IGR) CHD13940
KL = KL+1 CHD13950
I = MAT(IM) CHD13960
IF (ABS(RH01(J)-RHOV(1))-03*RHOV(1), 3528,3527,3527 CHD13970
3527 IN1 = J-1 CHD13980
GO TO 3530 CHD13990
3528 CONTINUE CHD14000
IN1 = JBFM CHD14010
3530 JBS = IBS(IG) CHD14020
JBE = IBE(IG) CHD14030
JBEM = JBE-1 CHD14040
K = JBE CHD14050
KL = JHDN CHD14060
DO 3532 J=JBS,JBEM CHD14070
K = K-1 CHD14080
IM = NCEN(IG)-KL/JHDN CHD14090
KL = KL+1 CHD14100
IF (RH01(K)-.19*RHOV(1)) 3532,3532,3531 CHD14110
3531 IN2 = K CHD14120
GO TO 3533 CHD14130
3532 CONTINUE CHD14140
IF (IG-IGR) 13533,13533,13532 CHD14150
13532 IG = IG-1

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13533 GO TO 3530
13533 CONTINUE
    IN2 = JBS-1
C
C**** ZONE SHIFT
C
3533 IF (IXLEFT(MNOD)-XSAVE) 3536, 3536, 3534
3536 WRITE(6,100) TIME
100 FORMAT(1H ///////////////////////////////////////////////////////////////////52X15)
    1H CASE TERMINATED//51X7HTIMF = F10.4)
    CALL EXIT
3534 J=NZEN(NRZON)-NCEN(MG)
    JBEM = IRE(IGR1)-1
    IF (JBEM-IN2) 3535, 3535, 3542
3535 IF (J+1) 3540, 3538, 3545
3538 NLZON = NLZON-1
3540 CALL SHIFT1 (NRZON,LRT+1)
    MARK = 2
    GO TO 3545
3542 IF (JBEM-IN2-JHDN-1) 3545, 3543, 3543
3543 CALL SHIFT1 (NRZON,LRT,-1)
    MARK = 2
    IF (J1 3545, 3544, 3544
3544 CONTINUE
    IZGT(2) = 1
    IZG(2+1) = MG+1
    IGTYP(MG+2) = 1
    IBE(MG+1) = IZB(2)
    IBS(MG+2) = IBE(MG)-NHDN(1)
    NCSN(MG+2) = NCEN(MG)-1
    NZSN(NRZON+1) = NCSN(MG+2)
    NZEN(NRZON+1) = NCSN(MG+2)
    CALL SHIFT1 (NRZON+1,LRT+1)
    MARK = 2
    NLZON = NLZON+1
3545 IF ((NZEN(NRZON)-NZSN(NRZON)+1)*JHDN-68) 3546, 3554, 3554
3546 JBS = IBS(IGR1)
    IF (IN1-JBS-1) 3550, 3550, 3554
3550 IF (NZSN(NRZON)-1) 3556, 3556, 3552
3552 CALL SHIFT1 (NRZON,LFT,-1)
    MARK = 2
    GO TO 3556
3554 IF (IN1-JBS-JHDN-1) 3556, 3556, 3555
3555 CALL SHIFT1 (NRZON,LFT+1)
    MARK = 2
3556 CALL SHIFT2
    IF ((NZEN(NRZON)-NZSN(NRZON)), 3558, 3557, 3558
3557 NZONC = 2
    NRIDC = 2
    GO TO 2600
3558 CONTINU
    GO TO (12687,2600),MARK
END

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- FOR COMBIN, COMBIN

SUBROUTINE COMBIN

C**** THE COMBIN SUBROUTINE COMBINES 2 MAJOR NODES INTO 1.

DIMENSION ASTORE(20), BSTORE(20), CSTORE(20),
 11, STORE(20), RS10PF(20), SSSTORE(20)

DIMENSION UHOLD(20), VHOLD(20), WHOLD(20), XHOLD(20)

DIMENSION NHDN(3), PHO4(305)

DIMENSION DFLTAX(11), TFMPA1(11)

DIMENSION PSTORE(20), QSTORE(20)

DIMENSION USTORE(20), VSTORE(20), WSTORE(20)

COMMON /BLOCKA/

1ABSORP(10) → ABSCE 1ACTENC → ACTENS 1ACTENV(4,1) → ACTENV(4,1,1) CHD14700
 2BSTAR → CCPC(4) 1CCPG(4) → CHARPT(10) 1CKC(4) → CHD14710
 3COEFT(4,10) → CONDC 1CONDV(100) → CONST(4,10) 1COVERX(100) → CHD14720
 4CPBAR → CPC 1CPV(100) → DIFPEC 1UMATER(10) → CHD14730
 5EFCOLC → EFCOLS 1EFCOLV(4,10) → EMIS(10) 1EMISC → CHD14740
 6HDFM(10) → HCOM 1HCOMG → HSUR 1MAT(100) → CHD14750
 7MATMN → MATMNF 1MN → NN 1NNP → CHD14760
 8NNSAVE → NRDIV 1NREND → NRGO 1NST → CHD14770
 9PARTIN(101) → PHI 1QBYRAD → QCOMB 1QEXTR → CHD14780
 10GPCOM → QSUBL 1RECPR → REORDC 1REORDS → CHD14790
 2REORDV(4,10), RH05Z → RH05(305) 1RH05(305) → RHOC → CHD14800
 1RH0V(10) → SABL 1SABL → SDOT → SDOTC → CHD14810
 4SLOPE(10) → TMELT(10) 1TSZ → TS(205) → TRCHAR → CHD14820
 5WFZ → WF(205) 1XCHAR → XINIT → XLEFT(101) → CHD14830
 6XMASS → XMDO TC 1XMDO TD → XMDO TG → XMDO TL → CHD14840
 7XMDO TR → XMDO TS → XTOTAL → XVIRG(101) → XZONE → CHD14850

COMMON/BLOCKC/

1BLPRES(20,11) → COMMAX 1CUTOFF → F(20,11) → CHD14860
 2FLOW(20,11) → HCONV(20,11), IERROR → JUNCT → L → CHD14870
 3N → NOSECH 1QBACK → QCONV(20,11), OGAS(20,11) → CHD14880
 4QMISC → TIME 1TPRINT → TWALL(20,11), XIWALL(20,11) → CHD14890
 5XIR(20,11)
 COMMON /CHCOM/ DTAU, 1BE(10), 1BS(10), 1BSPN, CHD14900
 1IGTYP(10), 1HDN(4), 1M, 1ZA(3), 1ZG(3,10), CHD14910
 2IZGT(1), JRSW, NCSN(10), NSHL(1), NSHR(1), CHD14920
 3ZNEN(3), NZSN(3), RH01(305), RH02(305), RH03(410), CHD14930
 4I → TEMPA2(205), TEMPA3(42), TEMPA4(42), TEMPA5(205), CHD14940
 5 → DELX(100), DISTL(100), DUM(10), ICOM, CHD14950
 6IYS, LFT, MG, MDUM, NCEN(10), NCUT, ND(3), NLZON, SN, CN1, CHD14960
 7SCHECK
 COMMON /NASCOM/ CHARRO, AIRM.
 1CARBN1(205), CARBN5(205), SILCA1(205), SILCA5(205), PYRO(205), DEP(205) → CHD15110
 2HYD(205), AERO(205), AERN(205), BURN(205), WFD(205), WDEP(205), WS1(20) → CHD15120
 35, WBRN(205), EMWT(205), PRG(205) → CHD15130
 4, TIMEX(50), TFT(50), NPTS → CHD15140
 5, POR(205), PERM1(205), PERM2(205), VISC(205), GCON, RHOTS, CARTS, SILTS, → CHD15150
 6PORT, PERT1, PERT2, DCOH, DCOO, DCOPY, DCODP, DCOS1, DCOCM, DCON, CFXH, CFXO, → CHD15160
 7CFXPY, CFXDP, CFXSI, CFXCM, CFXN, DIFCO(205), SOX(205) → CHD15170
 8, ALLGAS(205), GRAF1(205) → CHD15180
 EQUIVALENCE (1HDN(2), NHDN(1)) → CHD15190
 EQUIVALENCE (RH03(103), RH04(1)) → CHD15200
 EQUIVALENCE (TEMPA1(1), TS(1)), (DELTAX(1), PARTIN(1)) → CHD15210
 EQUIVALENCE (MNOD, NNP) → CHD15220
 SF = 1. → CHD15230

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KX = 0
IX = 0
DSTORE(1) = 0.
IG = MG-1
1 KHDN = JHDN
KST = JST
J=NCEN(IG-1)
ONF = DELTAX(J)*CF
JX = IGTYP(IG)
JHDN = NHDN(JX)
JST = IRE(IG)-JHDN
K = JST-1
JY = JHDN+IX
E DO 10 I=1,JY
K = K+1
KX = KX+1
UHOLD(KX)=WFD(K)
VHOLD(KX)=WDFP(K)
WHOLD(KX)=WSI(K)
XHOLD(KX)=WBRN(K)
USTORF(KX)=EMWT(K)
VSTORF(KX)=WF(K)
WSTORF(KX)=GRAF1(K)
ASTORF(KX)=TEMPA1(K)
RSTORF(KX)=TEMPA2(K)
CSTORF(KX)=TEMPA5(K)
DSTORE(KX+1) = DSTORE(KX)+ONF
PSTORF(KX)=SILCA1(K)
QSTORF(KX)=CARBN1(K)
RSTORF(KX)=RHO1(K)
10 SSTORE(KX)=RHO2(K)
SF = SN1/SN
IX = IX+1
IG = MG
GO TO (3,12)+IX
12 CONTINUE
J = KST
IF (ICOM-2) 14 +14+13
13 KST = JST
KHDN = JHDN
14 CONTINUF
TEMPA1(KST)=TEMPA1(J)
TEMPA2(KST)=TEMPA2(J)
TEMPA5(KST)=TEMPA5(J)
SILCA1(KST)=SILCA1(J)
CARBN1(KST)=CARBN1(J)
WFD(KST)=WFD(J)
WDFP(KST)=WDFP(J)
WSI(KST)=WSI(J)
WBRN(KST)=WBRN(J)
EMWT(KST)=EMWT(J)
WF(KST)=WF(J)
GRAF1(KST)=GRAF1(J)
RHO1(KST)=RHO1(J)
RHO2(KST)=RHO2(J)
CHD15240
CHD15250
CHD15260
CHD15270
CHD15280
CHD15290
CHD15300
CHD15310
CHD15320
CHD15330
CHD15340
CHD15350
CHD15360
CHD15370
CHD15380
CHD15390
CHD15400
CHD15410
CHD15420
CHD15430
CHD15440
CHD15450
CHD15460
CHD15470
CHD15480
CHD15490
CHD15500
CHD15510
CHD15520
CHD15530
CHD15540
CHD15550
CHD15560
CHD15570
CHD15580
CHD15590
CHD15600
CHD15610
CHD15620
CHD15630
CHD15640
CHD15650
CHD15660
CHD15670
CHD15680
CHD15690
CHD15700
CHD15710
CHD15720
CHD15730
CHD15740
CHD15750
CHD15760
CHD15770
CHD15780

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DX = .000000*DSTORE(KX)/FLOAT(KHDN) CHD15790
DIS = 0. CHD15800
K = 1 CHD15810
DO 30 J=1,KHDN CHD15820
DIS = DIS+DX CHD15830
KX = KST+J CHD15840
20 ONE = DSTORE(K+1)-DIS CHD15850
IF (ONE) 21+23+23 CHD15860
21 K = K+1 CHD15870
GO TO 20 CHD15880
23 THREE = DSTORE(K+1)-DSTORE(K) CHD15890
ONE = ONE/THREE CHD15900
TWO = (DIS-DSTORE(K))/THREE CHD15910
WFD(KX)=ONE*UHOLD(K)+TWO*UHOLD(K+1) CHD15920
WDFP(KX)=ONE*VHOLD(K)+TWO*VHOLD(K+1) CHD15930
WSI(KX)=ONE*WHOLD(K)+TWO*WHOLD(K+1) CHD15940
WRBN(KX)=ONE*XHOLD(K)+TWO*XHOLD(K+1) CHD15950
EMWT(KX)=ONE*USTORE(K)+TWO*USTORE(K+1) CHD15960
WF(KX)=ONE*VSTORE(K)+TWO*VSTORE(K+1) CHD15970
GRAF1(KX)=ONE*WSTORE(K)+TWO*WSTORE(K+1) CHD15980
TEMPA1(KX) = ONE*ASTORE(K)+TWO*ASTORE(K+1) CHD15990
TEMPA2(KX) = ONE*BSTORE(K)+TWO*BSTORE(K+1) CHD16000
TEMPA5(KX) = ONE*CSTORE(K)+TWO*CSTORE(K+1) CHD16010
SILCA1(KX)=ONE*PSOPF(K)+TWO*PSOPF(K+1) CHD16020
CARBN1(KX)=ONE*RSOPF(K)+TWO*RSOPF(K+1) CHD16030
RHO1(KX) = ONE*RSTORE(K)+TWO*RSTORE(K+1) CHD16040
* 30 RHO2(KX) = ONE*SSTORE(K)+TWO*SSTORE(K+1) CHD16050
K = IRSPN+NN CHD16060
RHO1(K) = RHO1(K+1) CHD16070
RHO2(K) = RHO2(K+1) CHD16080
PFTURN CHD16090
END CHD16100

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- FOR CONDF,CONDF
 FUNCTION CONDF(K)
 C*** THE CONDF SUBROUTINE CALCULATES HEAT CONDUCTIVITY CHD16110
 DIMENSION NHDN(3), RH04(206) CHD16120
 DIMENSION DELTAX(1), TEMPAA(1) CHD16130
 COMMON /BLOCKA/ CHD16140
 1ABSORP(10) ,ABSC ,ACTENC ,ACTENS ,ACTENV(4,10), CHD16150
 2BSTAR ,CCPC(4) ,CCPG(4) ,CHARPT(101) ,CKC(4) , CHD16160
 3COEFT(4,10) ,CONDc ,CDUM(100) ,CONST(4,10) ,COVERX(100) , CHD16170
 4CPBAR ,CPC ,CPV(100) ,DIFREC ,SUMATER(10) , CHD16180
 5EFCOLC ,EFCOLS ,EFCOLV(4,10) ,EMIS(10) ,EMISC , CHD16190
 6HOFM(10) ,HCOM ,HCOMG ,HSUB ,MAT(100) , CHD16200
 7MATOMN ,MATMNE ,MN ,NN ,NNP , CHD16210
 8NNSAVE ,NRDIV ,NREND ,NRGO ,NST , CHD16220
 9PARTIN(101) ,PHI ,QBYRAD ,QCOMB ,QEXTR , CHD16230
 10GPCOM ,QSUBL ,RECPCO ,REORDC ,REORDS , CHD16240
 2REORDV(4,10) ,RH05Z ,RH05(305) ,RHOC , CHD16250
 3RH0V(10) ,SABL ,SABLc ,SDOT ,SDOTC , CHD16260
 4SLOPE(10) ,TMELT(10) ,TSZ ,TS(205) ,TRCHAR , CHD16270
 5WFZ ,WF(205) ,XCHAR ,XF ,XLEFT(101) , CHD16280
 6XMASS ,XMDOTC ,XMDOTD ,XMDOTL , CHD16290
 7XMDOTR ,XMDOTS ,XTOTAL ,XZONE , CHD16300
 COMMON /BLOCKC/
 1BLPRES(20,11) ,COMMAX ,F(20,11) , CHD16310
 2FL0W(20,11) ,HCONV(20,11) ,IERROR ,L , CHD16320
 3N ,NOSECH ,OBACK ,O ,NGAS(20,11) , CHD16330
 40MISC ,TIME ,TPRINT ,TWALL(20+11),XIWALL(20,11) , CHD16340
 5XIR(20+11) ,
 COMMON /CHCOM/ DTAU, IBE(10), IBS(10), IBSPN, CHD16350
 11GTYP(10), IHDN(4), IM, IZB(3), IZG(3,10), CHD16360
 2IZGT(3), JRSW, NCSN(10), NSHL(3), NSHR(3), CHD16370
 3NZFN(3), NZSN(3), RH01(305), RH02(305), RH03(410), CHD16380
 4I ,TEMPA2(205),TEMPA3(42),TEMPA4(42),TEMPA5(205), CHD16390
 5 ,DELX(100),DISTL(100),DUM(10),ICOM, CHD16400
 6IYS,LFT,MG,NDDUM,NCEN(10),NCUT,ND(3),NLZON,SN,SN1, CHD16410
 7SCHECK ,
 COMMON /DACOM/ A(42), CHD16420
 1ABVAL ,ABVALM,ABVALS,B(42),C(42), CC(205),COND(42), CHD16430
 2CONDXX ,CONDXX, D(42),DD(205),DELTX(101),DGAS,DQ, CHD16440
 3DTAUC ,DTAUS ,DTAUX ,DTF ,DTR(3),EDFX,EDFXX,EMI(42), CHD16450
 4ETA,ETAS,FHT(42),FHTX,FHTXX,GAGC,GAS1,GK,GX,GY,GZ, CHD16460
 5HDA15,101,IBSPM,IERR,IGC,IGL,IGLD,IGR,IGRL,IGT,IG2, CHD16470
 6IHYS,INEG,IN1,IN2,IP,IPLUS,ITER,ITERT,IX,IY,IZ,J,JBE, CHD16480
 7JREM,JBFX,JBN1,JBN2,JBS,JBSM,JBSPM,JBSPN,JBX,JBXX,JCEN, CHD16490
 8JCENM,JCSN,JCSNM,JE,JE1,JE2,JHDN,JHDN1,JLSW,JSLAB,JX,JZ, CHD16500
 9K1,LANDID,LRT,MARK,MADD(42),NASW,NBNDST,NBND1(11), CHD16510
 1NBSW,NDC,NDCM,NLSW(10),NOF,NOTIME,NPBSW,NPE1N,NPS2N,NPTSW, CHD16520
 2NPID,NRIDC,NRSW(10),NRZON,NSLAB(10),N\$LABH(10),NSW,NXSW, CHD16530
 3NZON,NZONC,ONE,PSI,QSAVE,QTOT,QTOTAL,REFCTR,SBK,SDN, CHD16540
 4SDOTN,SNS,SRA,TAR,TAUOUT,TAUST(3),TAU1,TAU2,TAU2S,TEMPA, CHD16550
 5TEMPST(3),THREE,TWO,WFP,WFX,WFXX,XI,XMCOM,XSAVE CHD16560
 COMMON /NASCOM/ CHARRO,AIRM, CHD16570
 1CARBN1(205),CAPBNS(205),SILCA1(205),SILCA5(205),PYRO(205),DEP(205) CHD16580
 2HYD(205),AERO(205),AERN(205),BURN(205),WFD(205),WDEP(205),WSI(20) CHD16590
 3,WRBN(205),EMWT(205),PRG(205) CHD16600
 COMMON /NASCOM/ CHARRO,AIRM, CHD16610
 1CARBN1(205),CAPBNS(205),SILCA1(205),SILCA5(205),PYRO(205),DEP(205) CHD16620
 2HYD(205),AERO(205),AERN(205),BURN(205),WFD(205),WDEP(205),WSI(20) CHD16630
 3,WRBN(205),EMWT(205),PRG(205) CHD16640

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4,TIMEX(50),TFT(50),NPTS CHD16650
5,POR(205),PERM1(205),PERM2(205),VISC(205),GCON,RHOTS,CARTS,SILTS, CHD16660
6PORT,PERT1,PERT2,DCOH,DCOO,DCOPY,DCODP,DCOSI,DCOCM,DCON,CFXH,CFXO,CHD16670
7CFXPY,CFXDP,CFXSI,CFXCM,CFXN,DIFCO(205),SOX(205) CHD16680
8,ALLGAS(205),GRAFI(205) CHD16690
EQUIVALENCE (IHDN(2),NHDN(1)) CHD16700
EQUIVALENCE (RHO3(103),RHO4(1)) CHD16710
EQUIVALENCE (TEMPA1(1),TS(1)),(DELTAX(1),PARTIM(1)) CHD16720
EQUIVALENCE (MNOD,NNP) CHD16730
DIMENSION AREA(42),ARFAV(42) CHD16740
EQUIVALENCE (RHOCPX(44),AREA(1),AREAV(43)) CHD16750
KL=JBSM+K CHD16760
TEMPA=TEMPA4(K) CHD16770
GO TO (13,4,4),JRSW CHD16780
4 CONTINUE CHD16790
IF (TEMPA4(K)-4460.+7,7,5 CHD16800
5 TEMP=4460. CHD16810
7 CONDC=CKC(1)+TEMPA*(CKC(2)+TEMPA*(CKC(3)+TEMPA*CKC(4))) CHD16820
13 CONDV = CONST(1,I)+TEMPA4(K)*(CONST(2,I)+TEMPA4(K) CHD16830
1*(CONST(3,I)+TEMPA4(K)*CONST(4,I))) CHD16840
CONDV=CONDV/1.622+2.164*TEMPA4(K)/(BLPRES(N,L)+1.E-10)+.0001120 CHD16850
GO TO (15,17,17),JRSW CHD16860
15 CONDF = CONDV CHD16870
GO TO 18 CHD16880
17 CONDF = (CONDV-CONDc)*RHO4(K)/RH0V() + CONDC CHD16890
18 CONDF=CONDF*ARFA1(K)/(2.*DELTAX(1M)) CHD16900
RETURN CHD16910
END CHD16920

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- FOR CPRA,CPRA
SUBROUTINE CPRA(J,K,TEMPA,CPBAR) CHD16930
COMMON /RLOCKA/USFR(58),CCPG(4) CHD16940
COMMON /NASCOM/ CHARRO,AIRM,
1CARBN1(205),CARBN5(205),SILCA1(205),SILCA5(205),PYRO(205),DEP(205)CHD16950
2,HYD(205),AERO(205),AERN(205),BURN(205),WFD(205), WDEP(205),WSI(205)CHD16970
351,WRRN(205),FMWT(205),PRG(205) CHD16980
4,TIMEX(50),TFT(50),NPTS CHD16990
5,POR(205),PERM1(205),PERM2(205),VISC(205),GCON+RHOTS,CARTS,SILTS, CHD17000
6PORT,PERT1,PERT2,DCOH,DCOO,DCOPY,DCODP,DCOST,DCOCM,DCON,CFXH,CFXO,CHD17010
7CFXPY,CFXDP,CFXS1,CFXCM,CFXN,DIFCO(205),SOX(205) CHD17020
8,ALLGAS(205),GRAF1(205) CHD17030
CPBAR=CCPG(1)+TEMPA*(CCPG(2)+TEMPA*(CCPG(3)+TEMPA*CCPG(4))) CHD17040
END CHD17050

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- FOR DEPO,DEPO
  SUBROUTINE DEPO (K,KL,TMPA,DEL)          CHD17060
                                              CHD17070
C****  CARBON DEPOSITION                  CHD17080
                                              CHD17090
                                              CHD17100
COMMON /BLOCKA/
1ABSORP(10)  ABSC      ACTENC      ACTENS      ACTENV(4,10)  CHD17110
2BSTAR       CCPC(4)   CCPG(4)      CHARPT(10)   CKC(4)      CHD17120
3COEFT(4,10) CONDC     CONDV(100)    CONST(4,10)  COVERX(100) CHD17130
4CPBAR       CPC        CPV(100)     DIFREC      UMATER(10)   CHD17140
5EFCOLC     EFCOLS     EFCOLV(4,10) EMIS(10)   EMISC      CHD17150
6HOFM(10)   HCOM      HCOMG       HSUB        MAT(100)    CHD17160
7MATMN      MATMNF     MN          NN          NNP         CHD17170
8NNSAVE     NRDIV     NRENDD     QBYRAD      OCOMA      QEXTR      CHD17180
9PARTIN(101) PHI        RECPRD     RHO5(305)   RHOCPX(101) RHOC       CHD17190
10GPCOM    QSEUL      RHO5(305)    RHOCPX(101) REORDC    REORDS    CHD17200
2REORDV(4,10) RHO5Z     SDOT        TS(205)    SDOTC      TRCHAR    CHD17210
3RHOV(10)   SABL       SABLc      XINIT      XLEFT(101)  CHD17220
4SLGPE(10)  TMELT(10) TS2         XCHAR      XMDOTG    XMDOTL   CHD17230
5WFZ        WF(205)    XCHAR      XMDOT     XMDOTL    CHD17240
6XMASS     XMDOTC    XMDOT     XTOTAL      XVIRG(101) XZONE      CHD17250
7XMDOTR   XMDOTS     XTOTAL
COMMON/BLOCKC/
1BLPRES(20,11) COMMAX    CUTOFF      F(20,11)   CHD17260
2FLOW(20,11)  HCONV(20,11) IERROR     JUNCT      L          CHD17270
3N          NOSECH     QBACK      QCONV(20,11) QGAS(20,11) CHD17280
40MISC     TIME        TPRINT     TWALL(20,11) XIWALL(20,11) CHD17290
5XIR(20,11)
COMMON /BLOCKJ/
1FLUXI(200),TEDEP(200),XEDEP(101),EDEP(101),NTEDEP, CHD17300
2NXEDEP,ITEPEP,EDFLUX(100)  CHD17310
COMMON /BLOCKK/NN1,QCOND(205)  CHD17320
COMMON/BLOCKN/COORD  CHD17330
COMMON/BLOCKR/DIFC(4),EROC(4),ERODE  CHD17340
COMMON /CHCOM/ DTAU,  IBE(10),  IBS(10),  IRSPN,  CHD17350
1IGTYP(10),  IHDN(4),  IM,      IZB(3),   IZG(3,10), CHD17360
2IZGT(3),   JRSW,    NCSN(10),  NSHL(3),  NSHR(3),  CHD17370
3NZEN(3),   NZSN(3),  RHO1(305), RHO2(305), RHO3(410), CHD17380
4I          TEMPAP(20), TEMPAP(42), TEMPAP(42), TEMPAP(205), CHD17390
5          DELX(100), DISTL(100), DUM(10), ICOM,   CHD17400
6IYS,LFT,MG,MDUM,NCEN(10),NCUT,ND(3),NLZON,SN,SNi, CHD17410
7SCHECK
C****  DIMENSION STATEMENTS
DIMENSION DELTAX(1),TEMPA1(1)          CHD17420
EQUIVALENCE (TEMPA1(1),TS(1)),(DELTAX(1),PARTIN(1)) CHD17430
COMMON /NASCOM/ CHARRO,AIRM,             CHD17440
1CARBN1(205),CARBN5(205),SILCA1(205),SILCA5(205),PYRO(205),DEP(205) CHD17450
2,HYD(205),AERO(205),AERN(205),BURN(205),WFD(205), WDFP(205),WSI(205) CHD17460
35),WRBN(205),FMWT(205),PRG(205)  CHD17470
4,TIMEX(50),TFT(50),NPTS,             CHD17480
5,POR(205),PERM1(205),PERM2(205),VISC(205),GCON,RHOTS,CARTS,SILTS, CHD17490
6PORT,PERT1,PERT2,DCOH,DCON,DCOPY,DCODP,DCOS1,DCOCM,DCON,CFXH,CFXO,CHD17500
7CFXPY,CFXDP,CFXS1,CFXCM,CFXN,DIFCO(205),SOX(205)  CHD17510
8,ALLGAS(205),GRAF1(205),GRAF5(205),SPEED(205),DIFCH(205),DIFR(205) CHD17520

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9,VISCO+VISCON+AF+BF+SILICA+REQ+PMW+DMW+HMW+AUMW+ANMW+SMW+BMW,CX(6)CHD17600
1,QSI,QBRN,QDEP,DACT                                         CHD17605
REAL MCXT,METC                                         CHD17610
FMFP=EMWT(KL)/ALLGAS(KL)*PRG(KL)/2116.                     CHD17620
METC= PYRO(KL)/16.*FMFP                                     CHD17640
HYDC=.2*METC                                              CHD17645
IF (HYDC-.02834) 10,10,20                                    CHD17650
10 M=1
GO TO 30
20 M=2
30 CONTINUE
50 ARM=1.
60 CONTINUE
CAR=ARM*4882.4*RHOC
MCXT=928000.*EXP(-51894./TEMPA)*CX(3*M-2)
YH=HYDC*CX(3*M-1)
ZM=METC*CX(3*M)
ZMH=ZM*YH
WDEP(KL)=-CAR*MCXT*4.*((YH+(HYDC**2*CX(3*M)/20048.-ZM/4.))+ZMH-ZMYH)CHD17800
1*YH)/(1.-YH+ZM-2.*ZMH)**2
HERE=(DELTAX(K)+DEL)/26,
TEST=.72*DACT/HERE
IF (WDEP(KL)-TEST) 80,80,70
70 WDEP(KL)=TEST
GO TO 90
80 IF (WDEP(KL)) 85,90,90
85 WDEP(KL)=0.
90 CONTINUE
CARAN5(KL)=CARBN5(KL)+WDEP(KL)*DTAU
WDEP(KL)=WDEP(KL)*HERE
RETURN
END

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```
- FOR DIAG6,DIAG6
  SUBROUTINE DIAG6
    COMMON /BLOCKC/ DUMMY(BR2),IERROR
    I=87
    CALL PICKUP(I,X)
    WRITE(6,1) X
1 FORMAT(1H1,4X,45HEX$ EXIT THROUGH MERR$ BECAUSE OF DIVIDE OVERFLOW/SX,CHD17990
144HTHE ADDRESS OF THE OFFENDING INSTRUCTION IS ,012)
    IERROR=17
    CALL ERROR3
  END
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CHD17940
CHD17950
CHD17960
CHD17970
CHD17980
CHD18000
CHD18010
CHD18020
CHD18030

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FOR DIAG7,DIAG7
  SUBROUTINE DIAG7
    COMMON /BLOCKC/
    1BLPREF(20+11)      ,COMMAX      ,CUTOFF      ,F(20+11)      ,CHD18040
    2FLOW(20+11)      ,HCONV(20+11),IFERROR      ,JUNCT      ,L      ,CHD18050
    3N      ,NOSECH      ,QRACK      ,QCONV(20+11),QGAS(20+11)      ,CHD18060
    4QMISC      ,TIME      ,TPRINT      ,TWALL(20+11),XIWALL(20+11),CHD18070
    5XIR(20+11)
    WRITE(6,1)
1   FORMAT(//1H ,4X,29H EXIT BECAUSE OF JUMP TO MFRR$)
    IFERROR=17
    CALL FRROR3
  END
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- FOR DIFUS,DIFUS

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SUBROUTINE DIFUS (DIFCAL,NSOUR ,DC0,CFIX,CONC)          CHD18160
COMMON /BLOCKA/
1ABSORP(10),ABSC,ACTENC,ACTENS,ACTENV(4,10),CHD18170
2RSTAR,CCPC(4),CCPG(4),CHARPT(101),CKC(4),CHD18180
3COEFT(4,10),COND,CONDV(100),CONST(4,10),COVERX(100),CHD18190
4CPBAR,CPC,CPV(100),DIFREC,UMATER(10),CHD18200
5EFCOLC,EFCOLS,EFCOLV(4,10),EMIS(10),EHISC,CHD18210
6HOFM(10),HCOM,HCOMG,HSUB,MAT(100),CHD18220
7MATOMN,MATMNE,MN,NN,MAT(100),CHD18230
8NSAVF,NRDIV,NREND,NRGO,NST,CHD18240
9PARTIN(101),PHI,QBYRAD,QCOMM,NEXT,CHD18250
10GPCOM,OSUBL,RECPRO,REORDC,REORDS,CHD18260
2REORDV(4,10),RH052,RH05(305),PHOCPX(101),RHOC,CHD18270
3RH0V(10),SABL,SABL,SDOT,SDOTC,CHD18280
4SLOPE(10),TMELT(10),TSZ,TS(205),TRCHAR,CHD18290
5WFZ,WF(205),XCHAR,XINIT,XLEFT(101),CHD18300
6XMASS,XMDOTC,XMDOTD,XMDOTG,XMDOTL,CHD18310
7XMDOTR,XMDOTS,XTOTAL,XVIRG(101),XZONE,CHD18320
COMMON /BLOCKB/ USER(24),BLDEN(20,11)                  CHD18330
COMMON /BLOCKC/
1BLPRES(20,11),COMMEX,CUTOFF,F(20,11),CHD18340
2FLOW(20,11),HCONV(20,11),IERROR,JUNCT,L,CHD18350
3N,NOSECH,QBACK,QCONV(20,11),QGAS(20,11),CHD18360
40MISC,TIME,TPRINT,TWALL(20,11),XIWALL(20,11),CHD18370
5XIR(20,11),CHD18380
COMMON /BLOCKJ/
1FLUX1(200),TEDEP(200),XEDEP(101),EDEP(101),NTDFP,CHD18390
2NXEDEP,ITEPEP,EDFLUX(100),CHD18400
COMMON /BLOCKK/NN1,QCOND(205)                         CHD18410
COMMON/BLOCKN/COORD                                     CHD18420
COMMON/BLOCKR/DIFC(4),EROC(4),ERODE                  CHD18430
COMMON /CHCOM/ DTAU,IBE(10),IBSPN,CHD18440
1IGTYP(10),IHDN(4),IM,IZB(3),IZG(3,10),CHD18450
2IZGT(3),JRSW,NCSN(10),NSHL(3),NSHR(3),CHD18460
3NZEN(3),NZSN(3),RH01(305),RH02(305),RH03(410),CHD18470
4I,TEMPA2(205),TEMPA3(42),TEMPA4(42),TEMPA5(205),CHD18480
5DELX(100),DISTL(100),DUM(10),ICOM,CHD18490
6IYS,LFT,MG,MDUM,NCEN(10),NCUT,ND(3),NLZON,SN,SN1,CHD18500
7SCHECK,CHD18510
COMMON/NUCOM/ NADA,CHD18520
1EM(42),CHD18530
COMMON /DACOM/ A(42),CHD18540
1ABVAL,ABVALM,ABVALS,B(42),C(42),CC(205),COND(42),CHD18550
2CONDXX,CONDXX,D(42),DD(205),DELT(101),DGAS,DQ,CHD18560
3DTAUC,DTAUS,DTAUX,DTF,DTR(3),EDFX,EDFXX,EMI(42),CHD18570
4ETA,ETAS,FHT(42),FHTX,FHTXX,GAGC,GAS1,GK,GX,GY,GZ,CHD18580
5HDA(5,10),IBSPM,IERR,IGC,IGL,IGLD,IGR,IGRL,IGT,IG2,CHD18590
6IHYS,INEG,IN1,IN2,IP,IPLUS,ITER,ITERT,IX,IY,IZ,J,JBE,CHD18600
7JBEM,JBEX,JBND1,JBND2,JBS,JBSM,JBSPN,JBX,JBXX,JCEN,CHD18610
8JCENM,JCSN,JCSNM,JE,JE1,JE2,JHDN,JHDN1,JLSW,JSLAB,JX,JZ,CHD18620
9K1,LANDID,LRT,MARK,NADD(42),NASW,NBNDST,NBND1(11),CHD18630
1NBSW,NDC,NDCM,NLSW(10),NOF,NOTIME,NPBSW,NPEIN,NPS2N,NPTSW,CHD18640
2NRID,NRIDC,NRSW(10),NRZON,NSLAB(10),NSLABH(10),NSW,NXSW,CHD18650
3NZON,NZONC,ONE,PSI,QSAVE,QTOT,QTOTAL,REFCTR,SBK,SDN,CHD18660

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4 SDOTN,SNS,SRA,TAR,TAUOUT,TAUST(3),TAU1,TAU2,TAU2S,TEMPA, CHD18690
5 TEMPST(3),THREE,TWO,WFP,WFX,WFXX,XI,XMCOM,XSAVE CHD18700
COMMON /NASCOM/ CHARRO,AIRM, CHD18710
1 CARBN1(205),CARBN5(205),SILCA1(205),SILCA5(205),PYRO(205),DEF(205)CHD18720
2,HYD(205),AERO(205),AERN(205),BURN(205),WFD(205), WDEP(205),WSI(205)CHD18730
35,WBRN(205),EMWT(205),PRG(205) CHD18740
4,TIMEX(50),TFT(50),NPTS CHD18750
5,POR(205),PERM1(205),PERM2(205),VISC(205),GCON,RHOTS,CARTS,SILTS, CHD18750
6,PORT,PERT1,PERT2,DCOM,DCOO,DCOPY,DCODP,DCOS1,DCOCM,DCON,CFXH,CFXQ,CHD18770
7,CFXPY,CFXDP,CFXS1,CFXCM,CFXN,DIFCO(205),SOX(205) CHD18780
8,ALLGAS(205),GRAF1(205),GRAFS(205),SPEED(205),DIFCH(205),DIFR(205)CHD18790
DIMENSION NBND2(10),NHDN(3) CHD18800
EQUIVALENCE (NBND1(1),NBND2(1)) CHD18810
EQUIVALENCE (IHDN(1),NHDN(1)) CHD18820
EQUIVALENCE (TEPA1(1),TS(1)),(DELTAX(1),PARTIN(1)) CHD18830
DIMENSION DELTAX(1),TEPA2(1) CHD18840
DIMENSION SOURCE(205),CONC(1) CHD18850
DIFCOS=0. CHD18860
ALPH=0. CHD18870
DCU=DCO*PHI*HCONV(N,L)/BLDEN(N,L) CHD18880
DO 100 IG=IGR,M3 CHD18890
CALL GRIN(IG) CHD18900
DO 9 J=JBS,JBE CHD18910
DIFCO(J)=DIFR(J)*POR(J) CHD18920
GO TO 1,2,3,4,5,6,7,NSOUR CHD18930
1 SOURCE(J)=-1.3733*WBRN(J) CHD18940
GO TO 9 CHD18950
2 SOURCE(J)=.01798*WFD(J) CND18960
GO TO 9 CHD18970
1 SOURCE(J)=.00002*WFD(J)+.11111*WDEP(J) CHD18980
DIFCO(J)=DIFCH(J)*POR(J) CHD18990
GO TO 9 . CHD19000
4 SOURCE(J)=.3767*WFD(J)-1.3333*WDEP(J) CHD19010
GO TO 9 CHD19020
5 SOURCE(J)=0. CHD19030
GO TO 9 CHD19040
6 SOURCE(J)=.61111*WSI(J) CHD19050
GO TO 9 CHD19060
7 SOURCE(J)=.6053*WFD(J)+2.3333*WBRN(J)+.38889*WSI(J) CHD19070
9 CONTINUE CHD19080
K=0 CHD19090
ALP=SPEED(JBS)*POR(JBS) CHD19100
DO 10 J=JBS,JBEM CHD19110
K=K+1 CHD19120
KL=LLD(J) CHD19130
KK=LLD(J-1) CHD19140
IF (KK-KL) 307,307,306 CHD19150
306 KK=KL-1 CHD19160
307 CONTINUE CHD19170
IF (POR(J)) 309,309,312 CHD19180
309 ALPHA=0. CHD19190
D(K)=0. CHD19200
GO TO 313 CHD19210
312 CONTINUE CHD19220
ALPHA=SPEED(J+1)*POR(J+1) CHD19230

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      DI(K)=SOURCE(J)/POR(J)          CHD19240
313  CONTINUF                      CHD19250
      A(K)=(DIFCOS+DIFCO(J))*6./DELTAX(KY)    CHD19260
      SAVF=(DIFCO(J)+DIFCO(J+1))*6./DELTAX(KL)    CHD19270
      C(K)=-SAVF                      CHD19280
      R(K)=SAVF+A(K)+   ALP          CHD19290
      A(K)=-A(K)-   ALPH          CHD19300
      ALPH=ALP                        CHD19310
      ALP=ALPHA                       CHD19320
      DIFCOS=DIFCO(J)                CHD19330
10   CONTINUE                         CHD19340
      IF (IG-IGR) 11,11,12          CHD19350
11   B(1)=A(1)+B(1)                  CHD19360
      CC(JRS)=C(1)/B(1)            CHD19370
      DD(JBS)=D(1)/B(1)            CHD19380
      GO TO 13                      CHD19390
12   ONE=A(1)-CC(JBXX)*A(1)        CHD19400
      CC(JRS)=C(1)/ONE             CHD19410
      DD(JRS)=(D(1)-A(1)*DD(JBXX))/ONE    CHD19420
13   CONTINUF                      CHD19430
      DO 20 J=2,JF1                 CHD19440
      K=JBSM+J                      CHD19450
      ONF=A(J)-CC(K-1)*A(J)        CHD19460
      IF (ONE) 15,14,15            CHD19470
14   CC(K)=0                        CHD19480
      DD(K)=0                        CHD19490
      GO TO 20                      CHD19500
15   CONTINUE                         CHD19510
      CC(K)=C(J)/ONE               CHD19520
      DD(K)=(D(J)-A(J)*DD(K-1))/ONE    CHD19530
20   CONTINUF                      CHD19540
      JBXX=JBEM                      CHD19550
100  CONTINUF                     CHD19560
      A(1)=-ALPH-SAVE              CHD19570
      B(1)= ALPHA+DCU+SAVF         CHD19580
      D(1)=DCU*CFIX+SOURCF(JRF)/(POR(JRF)+1.E-10)  CHD19590
      IF (B(1)-CC(JBE-1)*A(1)) 105,103,105    CHD19600
104  CONC(JBE)=0.                  CHD19610
      GO TO 106                    CHD19620
105  CONTINUF                     CHD19630
      CONC(JBE)=(D(1)-A(1)*DD(JBE-1))/(B(1)-CC(JBF-1)*A(1))  CHD19640
      IF (CONC(JBF)) 103,103,106    CHD19650
106  CONTINUF                     CHD19660
      JBX=JRF                      CHD19670
      DO 200 IG=MG,IGR,-1          CHD19680
      CALL GRIN(IG)                CHD19690
      CONC(JBF)=CONC(JBX)          CHD19700
      DO 150 J=JBEM,JBS,-1        CHD19710
      CONC(J) = DD(J) - CC(J)*CONC(J+1)  CHD19720
      IF (CONC(J)) 108,108,150    CHD19730
108  CONC(J) = 0.                  CHD19740
150  CONTINUE                      CHD19750
      JBX=JBS                      CHD19760
200  CONTINUF                     CHD19770
      HOLD=CONC(JBX)              CHD19780

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|------------------------|----------|
| IF (IGR-1) 205,205,210 | CHD19790 |
| 205 IGRL=1 | CHD19800 |
| GO TO 215 | CHD19810 |
| 210 IGRL=IGR-1 | CHD19820 |
| 215 CONTINUE | CHD19830 |
| DO 250 IG=1,IGRL | CHD19840 |
| CALL GRIN(IG) | CHD19850 |
| DO 230 J=JBS,JBE | CHD19860 |
| 230 CONC(J)=HOLD | CHD19870 |
| 250 CONTINUE | CHD19880 |
| RRETURN | CHD19890 |
| END | CHD19900 |

- FOR ERROR3, FRROR3
 SURROUTINE FRROR3
 COMMON /BLOCKA/
 1ABSORP(101) ,ABSC ,ACTENC ,ACTFNS ,ACTENV(4,10) ,CHD19910
 2BSTAR ,CCPC(4) ,CCPG(4) ,CHARPT(101) ,CKC(4) ,CHD19920
 3COEFT(4,10) ,COND C ,CONDV(100) ,CONST(4,10) ,COVERX(100) ,CHD19930
 4CPBAR ,CPC ,CPV(100) ,DIFREC ,UMATFR(10) ,CHD19940
 5EFCOLC ,EFCOLS ,EFCOLV(4,10) ,FMIS(10) ,EMISC ,CHD19950
 6HOFM(10) ,HCOM ,HCOMG ,HSUR ,MAT(100) ,CHD19960
 7MATOMN ,MATMNE ,MN ,NN ,NNP ,CHD19970
 8NNSAVE ,NRDIV ,NREND ,NRGO ,NST ,CHD20000
 9PARTIN(101) ,PHI ,QBYRAD ,QCOMB ,QEXTP ,CHD20010
 10GPCOM ,QSUBL ,RECPRO ,REFORDC ,REFORDS ,CHD20020
 2REORDV(4,10) ,RH052 ,RH05(205) ,RHOCPX(101) ,PHOC ,CHD20030
 3RH0V(10) ,SABL ,SABL C ,SDOT ,SDOTC ,CHD20040
 4SLOPE(10) ,TMELT(10) ,TSZ ,TS(205) ,TRCHAR ,CHD20050
 5WFZ ,WF(205) ,XCHAR ,XINIT ,XLEFT(101) ,CHD20060
 6XMASS ,XMDOTC ,XMDOTD ,XMDOTG ,XMDOTL ,CHD20070
 7XMODTR ,XMDOTS ,XTOTAL ,XVIRG(101) ,XZONE ,CHD20080
 COMMON/BLOCKB/
 1ALT ,AOFA ,AOFACH ,BETA(20) ,PLCOM(20,11) ,CHD20100
 2BLDEN(20,11) ,BLENT(20,11) ,BLTEM(20,11) ,BLVEL(20,11) ,BLRN(20,11) ,CHD20110
 3BMULT ,DIST(20,11) ,FSCOM ,FSGAM ,LENGTH(21) ,CHD20120
 4NDIM ,NTEMP ,NTHETA ,NTIME ,PAMB ,CHD20130
 5PSP ,PTOTAL ,QAMB ,QSHOUL ,CHD20140
 6R(20,11) ,REFCOM(20,11) ,REFDEN(20,11) ,REFRN(20,11) ,REFTEM(20,11) ,CHD20150
 7REFENT(20,11) ,RHOA ,RHOBIS ,RNPERF ,CHD20160
 8REFVIS(20,11) ,SWEEP ,THETA(11) ,THETSH ,CHD20170
 9RTRAN ,SOFS ,VISCOS ,X(20,11) ,XEQ(20,11) ,CHD20180
 1TTOTAL ,UAMB ,XLTRAN ,XMACH ,XX ,CHD20190
 2XIAMB ,XISP ,ZWALL ,REFPR(20,11) ,HMAX ,CHD20200
 3ATEMP ,BLVIS(20,11) ,ZWALL ,CHD20210
 COMMON /BLOCKC/
 1BLPRES(20,11) ,COMMEX ,CUTOFF ,F(20,11) ,CHD20220
 2FLOW(20,11) ,HCONV(20,11) ,IERROR ,JUNCT ,L ,CHD20230
 3N ,NOSECH ,QBACK ,QCONV(20,11) ,QGAS(20,11) ,CHD20240
 4QMISC ,TIME ,TPRINT ,TWALL(20,11) ,XIWALL(20,11) ,CHD20250
 5XIR(20,11) ,CHD20260
 COMMON /BLOCKD/
 1ALPHA(200) ,AMBPI(200) ,AMBT(200) ,AMULT(200) ,AXLD(200) ,CHD20270
 2BWTEST ,IATMOS ,IPR ,IPRINT(20,10) ,CHD20280
 3IQ ,IX ,KK ,MELTN ,MELTL ,CHD20290
 4MVTEST ,KK ,NKK ,NCHARM ,NMATLU ,CHD20300
 5NMATL ,NMATLD ,NSTRES ,NTBW ,NTIME1 ,CHD20310
 6NTIME2 ,PRINT ,PUT(20) ,QBAC(200) ,QINC(20) ,CHD20320
 7QINCR ,QM(200) ,QTIME(20) ,QTABLE(6,200) ,CHD20330
 8RPRINC ,RQINC ,RXINC ,T(200) ,TRW(200) ,CHD20340
 9TEMP(7) ,TT(200) ,V(200) ,TNT(20) ,TORIBW(200) ,CHD20350
 1TSIN(101) ,XTIME(20) ,Z(200) ,XINC(20) ,CHD20360
 2XINCR ,Z(200) ,ZZ(200) ,TRIBW(200) ,CHD20370
 COMMON /BLOCKE/
 1DIV ,IP ,IWPLT ,LPLOTH(20) ,LPLOTQ(20) ,CHD20380
 2LPLQCW(20) ,NCAM ,NCPL(20) ,NDRUMA ,NDRUMB ,CHD20390
 3NDRUMC ,NDRUMD ,NDRUME ,NDRUMF ,NLOCPh ,CHD20400
 4NLOCPO ,NNLOCW ,NNODEC ,NNODET ,NNSP ,CHD20410

| | | | | | |
|---|---|--------------------------------|--------------------------|----------------|-----------|
| 5NPAGE | ,NPLOTH(20) | ,NPLOTQ(20) | ,NPLOCW(20) | ,NTIMEP | ,CHD20450 |
| 6NPL(20) | ,NVALUC(20) | ,NVALUT(20) | ,PLOTM | ,PINC(20) | ,CHD20460 |
| 7PINCR | ,PPRINT | ,PTIME(20) | ,RPLINC | ,SPECS(31) | ,CHD20470 |
| 8STOPPL | ,TM | ,NNPRFV | | | CHD20480 |
| COMMON /BLOCKF/ | | | | | |
| IASTR(205) | ,AXLDEQ | ,CCOMSC(4) | ,CCOMSV(4,10),CFMODC(4) | ,CHD20500 | |
| 2CEMODV(4,10) | ,CEXP(4) | ,CEXPV(4,10) | ,CLCOFF | ,CMWGAS(4) | ,CHD20510 |
| 3CNUC(4) | ,CNUV(4,10) | ,CSHRSC(4) | ,CSHRSV(4,10),CSTRO(205) | ,CHD20520 | |
| 4CTENSC(4) | ,CTFNSV(4,10) | ,GP(205) | ,PERMC | ,PIN | ,CHD20530 |
| 5POROSC | ,POROSV(10) | ,PSTR1(205) | ,PSTR2(205) | ,PSTR3(205) | ,CHD20540 |
| 6RIN | ,RSTRC(205) | ,SHRSTR(205) | ,SSMAX(205) | ,RAD(205) | CHD20550 |
| 7,NSLART | | | | | CHD20560 |
| COMMON/BLOCKG/ | | | | | |
| 1QBOLD | ,QBWTOT | ,QCLD(20,10) | ,QCOLD | ,QCONVT(20,10) | ,CHD20580 |
| 2QGAST(20,10) | ,QGLD(20,10) | ,QGOLD | ,QMISCT | ,QMOLD | CHD20590 |
| COMMON /CHCOM/ DTAU, | | | | | |
| 1IGTYP(10) | ,IHDN(4) | ,IBE(10) | ,IBS(10) | ,IBSPN, | CHD20600 |
| 2IZGT(3) | ,JRSW, | ,IM, | ,IZB(3), | ,IZG(3,10), | CHD20610 |
| 3NZEN(3) | ,NZSN(3) | ,NCN(10) | ,NSHL(3), | ,NSHR(3), | CHD20620 |
| 4I | ,RHO1(305) | ,RHO2(305) | ,RHO3(410), | | CHD20630 |
| 5 | ,TEMPA2(205),TEMPA3(42),TEMPA4(42),TEMPA5(205), | | | | CHD20640 |
| 6IYS,LFT,MG,MDUM,NCEN(10),NCUT,ND(3),NLZON,SN,SN1, | | | | | CHD20650 |
| 7SCHFCK | | | | | CHD20670 |
| COMMON /BLOCKH/ | | | | | |
| 1DABS(50) | ,DABSC(50) | ,DACTEC(50) | ,DACTES(50) | ,DACTEV(4,50), | CHD20690 |
| 2DBSTAR(50) | ,DCCPC(4,50) | ,DCCPG(4,50) | ,DCCSC(4,50) | ,DCCSV(4,50) | ,CHD20700 |
| 3DCEMC(4,50) | ,DCEMV(4,50) | ,DCEXP(4,50) | ,DCEXPV(4,50) | ,DCKC(4,50) | ,CHD20710 |
| 4DCLCOE(50) | ,DCNUC(4,50) | ,DCNUV(4,50) | ,DCOE(4,50) | ,DCON(4,50) | ,CHD20720 |
| 5DCSHSC(4,50) | ,DCSHSV(4,50) | ,DCTS(4,50) | ,DCTS(4,50) | ,DDIFFU(50) | ,CHD20730 |
| 6DEFCC(50) | ,DEFCC(50) | ,DEFCCV(4,50) | ,DEMIS(50) | ,DEMISC(50) | ,CHD20740 |
| 7DHCOM(50) | ,DHCOMG(50) | ,DHOFM(50) | ,DHSUR(50) | ,DMWGAS(4,50) | ,CHD20750 |
| 8DPERMC(50) | ,DPORC(50) | ,DPORV(50) | ,DREORC(50) | ,DREORS(50) | ,CHD20760 |
| 9DREORV(4,50) | ,DRHOC(50) | ,DRHOV(50) | ,DSLOPE(50) | ,DTMELT(50) | ,CHD20770 |
| 1D1RCHA(50) | ,DMATER(50) | ,XMATER(100,2) | | ,TITLE(70) | ,CHD20780 |
| 2MELT1(50) | ,MELT2(50) | ,THICK(100) | ,MNODE(100) | | CHD20790 |
| COMMON /BLOCKM/CARD(14) | | | | | |
| COMMON /NASCOM/ DCHARR(5883) | | | | | |
| COMMON /DACOM/ A(42), | | | | | |
| 1ABVAL | ,ABVALM,ABVALS,B(42) | ,C(42), | CC(205),COND(42), | | CHD20830 |
| 2CONDX | ,CONDXX,D(42) | ,DD(205),DELT(101),DGAS,DQ, | | | CHD20840 |
| 3DTAUC | ,DTAUS,DTAUX | ,DTF,DTR(3),EDFX,EDFXX,EM(42), | | | CHD20850 |
| 4ETA,ETAS,FHT(42),FHTX,FHTXX,GAGC,GAS1,GK,GX,GY,GZ, | | | | | CHD20860 |
| 5HDA(5,10) | ,IBSPM,IERR,IGC,IGL,IGLD,IGR,IGRL,IGT,IG2, | | | | CHD20870 |
| 6IHYS,INEG,IN1,IN2,I3,IPLUS,ITER,ITERT,I4,IY,IZ,J,JBE, | | | | | CHD20880 |
| 7JBEM,JRFX,JAND1,JBND2,JBS,JBSM,JASPM,JASPN,JBX,JRXX,JCEN, | | | | | CHD20890 |
| 8JCFNM,JCEN,JCNSM,JE,JE1,JE2,JHDN,JHDN1,JLSW,JSLAB,JX,JZ, | | | | | CHD20900 |
| 9K1,LAND10,LRT,MARK,NADD(42),NASW,NBNDST,NBND1(11), | | | | | CHD20910 |
| 1NBSW,NDC,NDCM,NLSW(10),NOF,NOTIME,NPBSW,NPE1N,NPS2N,NPTSW, | | | | | CHD20920 |
| 2NRID,NRIDC,NRSW(10),NRZON,NSLAB(10),NLABH(10),NSW,NXSW, | | | | | CHD20930 |
| 3NZON,NZONC,ONE,PSI,QSAVE,QTOT,QTOTAL,REFCTR,SBK,SDN, | | | | | CHD20940 |
| 4SDOTN,SNS,SRA,TAR,TAUOUT,TAUST(3),TAU1,TAU2,TAU25,TEMPA, | | | | | CHD20950 |
| 5TEMPST(3),THREE,TWO,WFP,WFX,WFXX,XI,XMCOM,XSAVE | | | | | CHD20960 |
| DIMENSION XQBold(1),XNAME(10),ISTOP(10),DAL(1) | | | | | CHD20970 |
| DIMENSION DDTAU(1),DDIV(1) | | | | | CHD20980 |
| EQUivalence (DTAU,DDTAU(1)),(DIV,DDIV(1)) | | | | | CHD20990 |

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EQUIVALENCE (XQBOLD(1),QBOLD1),(DALT(1),ALT) CHD21000
DATA XNAME(1)/6HBLOCKA/,XNAME(2)/6HBLOCKB/,XNAME(3)/6HBLOCKC/ CHD21010
DATA XNAME(4)/6HBLOCKD/,XNAME(5)/6HBLOCKE/,XNAME(6)/6HBLOCKF/ CHD21020
DATA XNAME(7)/6HBLOCKG/,XNAME(8)/5HCHCOM/ CHD21030
DATA XNAME(9),XNAME(10)/5HDACOM,6HNASCOM/ CHD21040
DATA ISTOP(1)/1865/,ISTOP(2)/4045/,ISTOP(3)/1991/,ISTOP(4)/4451/ CHD21050
DATA ISTOP(5)/311/,ISTOP(6)/2335/,ISTOP(7)/806/,ISTOP(8)/1844/ CHD21060
DATA ISTOP(9),ISTOP(10)/1080,5883/ CHD21070
DATA NPT1/200/,NPT2/100/ CHD21080
DO 400 I=1,10 CHD21090
GO TO (250,400,250,400,400,400,250,250,250),I CHD21100
250 NSTOP=ISTOP\11 CHD21110
WRITF (6,1018)XNAME(1) CHD21120
DO 390 J=1,NSTOP,8 CHD21130
KG0=J-1 CHD21140
KSTOP=J+7 CHD21150
GO TO (310,320,330,340,350,360,370,380,384,388),! CHD21160
310 WRITE (6,1019)KG0,(ABS0RP(K),K=J,KSTOP) CHD21170
GO TO 390 CHD21180
320 WRITE (6,1019)KG0,(DALT(K),K=J,KSTOP) CHD21190
GO TO 390 CHD21200
330 WRITE (6,1019)KG0,(RLPRFS(K,1),K=J,KSTOP) CHD21210
GO TO 390 CHD21220
340 WRITE (6,1019)KG0,(ALPHA(K),K=J,KSTOP) CHD21230
GO TO 390 CHD21240
350 WRITE (6,1019)KG0,(DDIV(K),K=J,KSTOP) CHD21250
GO TO 390 CHD21260
360 WRITE (6,1019)KG0,(ASTR(K),K=J,KSTOP) CHD21270
GO TO 390 CHD21280
370 WRITE (6,1019)KG0,(XQBOLD(K),K=J,KSTOP) CHD21290
GO TO 390 CHD21300
380 WRITE (6,1019)KG0,(DDTAU(K),K=J,KSTOP) CHD21310
GO TO 390 CHD21320
384 WRITE (6,1019)KG0,(A(K),K=J,KSTOP) CHD21330
GO TO 390 CHD21340
388 WRITE (6,1019)KG0,(DCHARR(K),K=J,KSTOP) CHD21350
390 CONTINUE CHD21360
400 CONTINUF CHD21370
1018 FORMAT(1H160X16HDECIMAL DUMP OF A6/) CHD21380
1019 FORMAT(1H 06,1X,8E15.7) CHD21390
CALL EXIT CHD21400
END CHD21410

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- FOR FLOWS, FLOWS
 SUBROUTINE FLOWS
 COMMON /BLOCKA/
 1APSORP(10) ,ABSC ,ACTENL ,ACTENS ,ACTENV(4,10), CHD21420
 2RSTAR ,CCPC(4) ,CCPG(4) ,CHARPT(101) ,C(C4) ,CHD21420
 3COEFT(4,10) ,COND C ,CONDV(100) ,CONST(4,10) ,COVERX(100) ,CHD21450
 4CPBAR ,CPC ,CPV(100) ,DTFREC ,UMATER(10) ,CHD21470
 5EFCOLC ,EFCOLS ,EFCOLV(4,10) ,EMTS(10) ,EMISC ,CHD21480
 6HOFM(10) ,HCOM ,HCOMG ,HSUB ,MAT(100) ,CHD21490
 7MATOMN ,MATMNF ,MN ,NN ,NNP ,CHD21500
 8NNSAVE ,NRDIV ,NPEND ,NRGO ,NST ,CHD21510
 9PARTIN(101) ,PHI ,QBYRAD ,QCOMB ,QEXTR ,CHD21520
 10GPCM ,QSUBL ,RECPRO ,REORDC ,REORDS ,CHD21530
 2REFORDV(4,10) ,RH05Z ,RH05(305) ,RHOCPX(101) ,RHOC ,CHD21540
 3RH0V(10) ,SAPL ,SABL C ,SDOT ,SDOTC ,CHD21550
 4SLOPE(10) ,TMELT(10) ,TSZ ,TS(205) ,TRCHAR ,CHD21560
 5WFZ ,WF(205) ,XCHAR ,XTINIT ,XLEFT(101) ,CHD21570
 6XMASS ,XMDOTC ,XMDOTD ,XMDOTG ,XMDOTL ,CHD21580
 7XMDOTP ,XMDOTS ,XTOTAL ,XVIRG(101) ,XZONF ,CHD21590
 COMMON/BLOCKC/
 1BLPRES(20,11) ,COMMAX ,CUTOFF ,F(20,11) ,CHD21600
 2FLOW(20,11) ,HCONV(20,11) ,IERROR ,JUNCT ,L ,CHD21620
 3N ,NOSECH ,QBACK ,QCONV(20,11) ,QGAS(20,11) ,CHD21630
 4QMISC ,TIME ,TPRINT ,TWALL(20,11) ,XIWALL(20,11) ,CHD21640
 5XIR(20,11) ,CHD21650
 COMMON /BLOCKJ/
 1FLUXI(200) ,TEDEP(200) ,XEDEP(101) ,EDEP(101) ,NTEDEP ,CHD21670
 2NXEDEP ,ITEPEP ,EDFLUX(100) ,CHD21680
 COMMON /BLOCKK/NN1,QCOND(205) ,CHD21690
 COMMON/BLOCKN/COORD ,CHD21700
 COMMON/BLOCKR/DIFC(4) ,EROC(4) ,ERODE ,CHD21710
 COMMON /CHCOM/ DTAU, IBE(10), IBS(10), IBSPN, CHD21720
 1IGTY(10), IHDN(4), IM, IZR(3), IZG(3,10), CHD21730
 2IZGT(3), JRSW, NCSN(10), NSHL(3), NSHR(3), CHD21740
 3NZFN(3), NZSN(3), RH01(305), RH02(305), RH03(410), CHD21750
 4I ,TEMPA2(205), TEMPA3(42), TEMPA4(42), TEMPA5(205), CHD21760
 5 DELX(100), DISTL(100), DUM (10), ICOM, CHD21770
 6IYS,LFT,MG,MDUM,NCEN(10),NCUT,ND(3),NLZON,SN,SN1, CHD21780
 7SCHFCK ,CHD21790
 COMMON /NUCOM/ DX(205) ,XNHD(205) ,NADA(42) ,MATA(205) ,CHD21800
 1EM(42) ,CHD21810
 COMMON /DACOM/ A(42) ,CHD21820
 1ARVAL ,ARVALM,ABVALS,B(42) ,C(42) ,CC(205) ,COND(42) ,CHD21830
 2CONDXX ,CONDXX, D(42) ,DD(205) ,DELTX(101) ,DGAS,DO, CHD21840
 3DTAUC ,DTAUS ,DTAUX ,DTF ,DTR(3) ,DFDX ,EDFXX ,EMI(42) ,CHD21850
 4ETA,ETAS,FHT(42),FHTX,FHTXX,GAGC,GAS1,GK,GX,GY,GZ, CHD21860
 5HDA(5,10) ,IBSPM ,IERR ,IGC ,IGL ,IGLD ,IGR ,IGRL ,IGT ,IG2 ,CHD21870
 6IHYS ,INEG ,IN1 ,IN2 ,IP ,IPLUS ,ITER ,ITERT ,IX ,IY ,IZ ,J ,JB ,CHD21880
 7JBEM ,JBEX ,JBND1 ,JBND2 ,JBS ,JBSM ,JBSPM ,JBSPN ,JBX ,JBXX ,JCEN ,CHD21890
 8JCENM ,JCSN ,JCSNM ,JE ,JE1 ,JE2 ,JHDN ,JHDN1 ,JLSW ,JSLAB ,JX ,JZ ,CHD21900
 9K1 ,LAND ID ,LRT ,MARK ,NADD(42) ,NASW ,NBNDST ,NBND1(11) ,CHD21910
 1NBSW ,NDC ,NDCM ,NLCW(10) ,NOF ,NOTIME ,NPBSW ,NPE1N ,NPS2N ,NPTSW ,CHD21920
 2NRID ,NR IDC ,NRSW(10) ,NRZON ,NSLAB(10) ,NSLABH(10) ,NSW ,NXSW ,CHD21930
 3NZON ,NZONC ,ONE ,PSI ,QSAVE ,QTOT ,QTOTAL ,REFCTR ,SBK ,SDN ,CHD21940
 4SDOTN ,SNS ,SRA ,TAR ,TAUOUT ,TAUST(3) ,TAU1 ,TAU2 ,TAU2S ,TEMPO ,CHD21950

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STEMPSI(3),THPFE,TWO,WFP,WFX,WFX,X1,XMCOM,XSAVE CHD21960
COMMON /NASCOM/ CHARRO,AIRM,
1CARBN1(205),CARBN5(205),SILCA1(205),SILCA5(205),PYRO(205),DEP(205)CHD21980
2,HYDI(205),AERO(205),AERN(205),BURN(205),WFD(205),WDEP(205),WSI(20)CHD21990
35),WBRN(205),EMWT(205),PRG(205) CHD22000
4,TIMEX(50),TFT(50),NPTS CHD22010
5,POR(205),PERM1(205),PERM2(205),VIS(205),GCON,RHOTS,CARTS,SILTS, CHD22020
6,PORT,PERT1,PERT2,DCOH,DCOO,DCOPY,DCODP,DCOS1,DCOCM,DCON,CFXH,CFXO,CHD22030
7,CFXPY,CFXDP,CFXS1,CFXCM,CFXN,DIFCO(205),SOX(205) CHD22040
8,ALLGAS(205),GRAF1(205),GRAF5(205),SPEED(205),DIFCH(205),DIFR(205)CHD22050
DIMENSION NRND2(10),NHDN(3) CHD22060
DIMENSION DFLTAX(I),TFPA1(1) CHD22070
EQUIVALENCE (TEMPA1(1),TS(1)),(DELTAX(1),PARTIN(1)) CHD22080
EQUIVALENCE (NBND1(2),NBND2(1)) CHD22090
EQUIVALENCE (IHDN(2),NHDN(1)) CHD22100
DO 100 IG=IGR,MG CHD22110
CALL GRIN(IG) CHD22120
IF (IG=IGR) 30,30,20 CHD22130
20 POR(JBS)=POR(JBFX) CHD22140
PFRM1(JBS)=PFRM1(JBFX) CHD22150
PERM2(JBS)=PERM2(JBFX) CHD22160
VIS(JBS)=VIS(JBFX) CHD22170
KK=JBS+1 CHD22180
GO TO 40 CHD22190
30 KK=JBS CHD22200
40 DO 50 J=KK,JBE CHD22210
CALL PORE CHD22220
50 CONTINUE CHD22230
JBFX=JBE CHD22240
100 CONTINUE CHD22250
PRFRNT=BLPRES(N,L) CHD22260
ALPHA=WF(JBE)*GCON*TEMPA1(JBE)/( EMWT(JBE)*PRFRNT*POR(JBE)+1.E-1)CHD22270
151
DO 200 IG=MG,1,-1 CHD22280
CALL GRIN(IG) CHD22290
PRG(JBE)=PRFRNT CHD22300
SFFD(JBE)=ALPHA CHD22310
GO TO (140,150,150),JPSW CHD22320
140 CONTINUE CHD22330
DO 142 J=JBEM,JBS,-1 CHD22340
SFFD(J)=0. CHD22350
142 PRG(J)=PRFRNT CHD22360
GO TO 170 CHD22380
150 DO 160 J=JBEM,JBS,-1 CHD22390
K=LLD(J) CHD22400
IF (POR(J)) 151,151,153 CHD22410
151 PRG(J)=PRG(J+1) CHD22420
SFFD(J)=0. CHD22430
GO TO 160 CHD22440
153 CONTINUE CHD22450
IF (PFRM1(J)) 151,151,155 CHD22460
155 IF (PFRM2(J)) 151,151,157 CHD22470
157 CONTINUE CHD22480
PSQ=PRG(J+1)**2+GCON*TEMPA1(J)/(EMWT(J)+1.E-10)*(VIS(J)*WF(J)/( CHD22490
1POR(J)*PERM1(J)+1.E-15)+(WF(J)/(POR(J)+1.E-15))**2/(PERM2(J)+1.E- CHD22500

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220)*DFL*TAX(K)/12.          CHD22510
PRG(J)=SORT(PSQ)             CHD22520
SPEED(J)=WF(J)*GCON*TEMPA1(J)/(   FMWT(J)*PRG(J)*POR(J)+1.E-15) CHD22530
160 CONTINUE                   CHD22540
DO 165 J=JBS,JBE             CHD22550
TEMPA=TEMPA1(J)**1.6          CHD22560
TEMPB=TEMPA1(J)**2            CHD22570
DIFR(J)=.37803E-4*TEMPA/((PRG(J)+1.E-15)*EXP(-.1257E-3*TEMPA1(J)) CHD22580
1+.6110E-8*TEMPA1(J)*POR(J) CHD22590
DIFCH(J) =.67627E-4*TEMPA/((PRG(J)+1.E-15)*EXP(-.1847E-3*TEMPA1(J)) CHD22600
1+.1319E-7*TEMPA1(J)*POR(J) CHD22610
165 CONTINUE                   CHD22620
170 CONTINUE                   CHD22630
PRFRNT=PRG(JBS)              CHD22640
ALPHA=SPEED(JBS)              CHD22650
200 CONTINUE                   CHD22660
RETURN                        CHD22670
END                          CHD22680

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- FOR FONEV,FONEV
  FUNCTION FONEV(ARG,ISAVE,XRAY,YRAY,NPTS,IDELT)           CHD22690
  DIMENSION XRAY(1),YRAY(1)                                CHD22700
C   KPATH = 0 - FIRST PASS OF SEARCH IN XRAY               CHD22710
C   KPATH = -IDELT - DECREASE ISAVE                      CHD22720
C   KPATH = IDELT - INCREASE ISAVE                      CHD22730
  KDELT=IDELT                                              CHD22740
  KPTS=NPTS                                                CHD22750
  KSAVE=ISAVE                                              CHD22760
  XARG=ARG                                                 CHD22770
  KPATH=0                                                 CHD22780
  IF(KPTS)20,20,40                                         CHD22790
20  CONTINUE
  WRITE OUTPUT TAPE 6,1000,XARG                           CHD22800
  CALL EXIT                                               CHD22810
40  CONTINUE
  IF(KSAVE)120,60,120                                     CHD22820
60  CONTINUE
  KSAVE=KDELT+1                                           CHD22830
  IF(XRAY(KSAVE)-XRAY(1))80,20,120                      CHD22840
80  CONTINUE
  KSAVE=-KSAVE                                            CHD22850
120 CONTINUF
  KSUBJ=IABS(KSAVE)                                       CHD22860
  KSUBI=KSUBJ-KDELT                                      CHD22870
  FACT=ISIGN(1,KSAVE)                                     CHD22880
  GO TO 160                                              CHD22890
140 CONTINUE
  KSURI=KSUBJ                                             CHD22900
  KSUBJ=KSUBJ+KPATH                                      CHD22910
160 CONTINUE
  X2=XRAY(KSUBJ)                                         CHD22920
  Y2=YRAY(KSUBJ)                                         CHD22930
  DX=X2-XARG                                             CHD22940
  FACTDX=FACT*DX                                         CHD22950
  IF(KPATH)220,180,260                                    CHD22960
180 CONTINUE
  IF(FACTDX)240,260,200                                  CHD22970
200 CONTINUE
  KPATH=-KDELT                                           CHD22980
  KLIMIT=KDELT+1                                         CHD22990
  GO TO 140                                              CHD23000
220 CONTINUF
  KSUR=KSURI                                             CHD23010
  IF(FACTDX)320,300,280                                  CHD23020
240 CONTINUE
  KPATH=KDELT                                           CHD23030
  KLIMIT=KDELT*(KPTS-1)+1                               CHD23040
260 CONTINUE
  KSUB=KSUBJ                                             CHD23050
  IF(FACTDX)280,300,320                                  CHD23060
280 CONTINUE
  IF(KSUB-KLIMIT)140,320,140                            CHD23070
300 CONTINUE
  FONEV=Y2                                              CHD23080

```

```
      GO TO 340          CHD23230
320  CONTINUF          CHD23240
      X1=XRAY(KSUBI)    CHD23250
      Y1=YRAY(KSUBI)    CHD23260
      DXI=X2-X1         CHD23270
      FONEV=(Y2-Y1)/DXI*DX+Y2  CHD23280
340  CONTINUE          CHD23290
      ISAVE=ISIGN(KSUB,KSAVE)  CHD23300
      RETURN             CHD23310
1000 FORMAT(1H1,22HFONEV - IND VARIABLE *,E18.7)  CHD23320
      END                CHD23330
```

```
- FOR FRFC,FREC
FUNCTION FREC(RK,RFORDC,RDUM,BDUM)
FREC=RDUM/(RDUM*BDUM+RK**(REORDC-1.)*(RK+1.))
RETURN
END
```

CHD23340
CHD23350
CHD23360
CHD23370

- FOR FRONT, FRONT
 SUBROUTINE FRONT
 C*** THE FRONT SUBROUTINE DETERMINES IF FRONT NODE IS DROPPED OR CHD23380
 C*** COMBINED CHD23390
 DIMENSION NHDN(3), RHO4(306) CHD23400
 DIMENSION DELTAX(1), TMPA1(1) CHD23410
 COMMON /BLOCKA/ CHD23420
 1ABSORP(10), ABSC, ACTENC, ACTENS, ACTENV(4,10), CHD23430
 2BSTAR, CCPC(4), CCPG(4), CHARPT(101), CKC(4), CHD23440
 3COEFT(4,10), CONDC, CONDV(100), CONST(4,10), COVERX(100), CHD23450
 4CPBAR, CPC, CPV(100), DIFREC, SUMATER(10), CHD23460
 5EFCOLC, EFCOLCS, EFCOLV(4,10), EMIS(10), EMISC, CHD23470
 6HOFM(10), HCOM, HCOMG, HSUB, MAT(100), CHD23480
 7MATOMN, MATMNE, MN, NNP, CHD23490
 8NNSAVE, NRDIV, NREND, NRGO, NST, CHD23500
 9PARTIN(101), PHI, QBYRAD, QCOMB, GEXTR, CHD23510
 10GPCOM, GSUBL, RECPRO, REORDC, REORDS, CHD23520
 2REORDV(4,10), RHO5Z, RH05(305), RHOCPX(101), RHOC, CHD23530
 3RH0V(10), SABL, SABLc, SDOT, SDOTC, CHD23540
 4SLOPE(10), TMELT(10), TSZ, TS(205), TRCHAR, CHD23550
 5WFZ, WF(205), XCHAR, XINIT, XLEFT(101), CHD23560
 6XMASS, XMDOTr, XMDOTr, XMDOTr, XMDOTr, CHD23570
 7XMDOTr, XMDOTr, XTOTAL, XVIRG(101), XZONE, CHD23580
 COMMON /BLOCKC/
 1BLPRES(20,11), COMMAX, CUTOFF, F(20,11), CHD23590
 2FLOW(20,11), HCONV(20,11), IERROR, JUNCT, L, CHD23600
 3N, NOSECH, QBACK, QCONV(20,11), QGAS(20,11), CHD23610
 4QMISC, TIME, TPRINT, TWALL(20,11), XIWALL(20,11), CHD23620
 5XIR(20,11)
 COMMON /CHCOM/ DTAU, IBE(10), IRS(10), IBSPN, CHD23630
 1IGTYP(10), IHDN(4), IM, IZB(3), IZG(3,10), CHD23640
 2IZGT(3), JRSW, NCSN(10), NSHL(3), NSHR(3), CHD23650
 3NZEN(3), NZSN(3), RH01(305), RH02(305), RH03(410), CHD23660
 4I, TEMPA2(205), TEMPA3(42), TEMPA4(42), TEMPA5(205), CHD23670
 5, DELX(100), DISTL(100), DUM(10), ICOM, CHD23680
 6IYS, LFT, MG, MDUM, NCEN(10), NCUT, ND(3), NLZON, SN, SN1, CHD23690
 7SCHECK
 EQUIVALENCE (IHDN(2), NHDN(1))
 EQUIVALENCE (RHO3(103), RHO4(1))
 EQUIVALENCE (TEMPA1(1), TS(1)), (DELTAX(), PARTIN(1))
 EQUIVALENCE (MNOD, NNP)
 IF (MAT(MNOD-2)-MAT(MNOD-1)) 310, 320, 310
 310 NCUT = NCUT+2
 320 IF (NZEN(NLZON)-NZSN(NLZON)-1) 330, 340, 330
 330 ICOM = 1
 GO TO 390
 340 IF (NLZON-1) 350, 350, 360
 350 ICOM = 4
 GO TO 390
 360 IF (NZSN(NLZON)-NZEN(NLZON-1)) 370, 380, 370
 370 ICOM = 3
 GO TO 390
 380 ICOM = 2
 390 GO TO (420, 420, 400, 430), NCUT
 400 NCUT = 1

```

IF (ICOM-2) 415,415,410          CHD23920
410 CALL SHIFT1 (NLZON,LFT,-1)    CHD23930
415 RETURN                         CHD23940
420 CONTINUE                        CHD23950
        CALL COMBIN                  CHD23960
430 NCUT = 1                         CHD23970
        GO TO (440,450,460,460),ICOM  CHD23980
440 MG = MG-1                       CHD23990
        IZGT(NLZON) = IZGT(NLZON)-1  CHD24000
        NZFN(NLZON) = NZEN(NLZON)-1  CHD24010
        GO TO 490                     CHD24020
450 NLZON = 1                        CHD24030
        MG = MG-1                     CHD24040
        GO TO 490                     CHD24050
460 IF (NCEN(MG-1)-NCSN(MG-1)-1) 470,470,480  CHD24060
470 IBS(MG-1) = IBS(MG)             CHD24070
        IBE(MG-1) = IBE(MG)           CHD24080
        IZG(NLZON,1) = MG-1          CHD24090
        NZEN(NLZON) = NZSN(NLZON)    CHD24100
        NZSN(NLZON) = NZSN(NLZON)-1  CHD24110
        MG = MG-1                     CHD24120
        GO TO 490                     CHD24130
480 NZFN(NLZON) = NZSN(NLZON)       CHD24140
        NZSN(NLZON) = NZSN(NLZON)-1  CHD24150
        NCFN(MG) = NCSN(MG)          CHD24160
        NCSN(MG) = NCSN(MG)-1        CHD24170
        NCEN(MG-1) = NCEN(MG-1)-1   CHD24180
        IBE(MG-1) = IBE(MG-1)-1    CHD24190
490 CONTINUE                         CHD24200
        ND(1) = ND(1)-1              CHD24210
        XLEFT(NN) = XLEFT(IYS)+SN1   CHD24220
        MNOD = NN                     CHD24230
        NN = NN-1                     CHD24240
        IYS = ND(1)                   CHD24250
        SCHHECK = 0.5*DELX(IYS)      CHD24260
        SN1 = XLEFT(MNOD)-XLEFT(IYS) CHD24270
        DISTL(IYS) = 0.                CHD24280
        DISTL(MNOD) = 1.              CHD24290
        DELX(IYS)=1.                 CHD24300
        RETURN                         CHD24310
        END                            CHD24320

```

```

- FOR GPCOM, GPCOM
  SUBROUTINE GPCOM
    COMMON /BLOCKA/
 1ABSORP(10) ,ABSC      ,ACTENC      ,ACTENS      ,ACTENV(4,10), CHD24330
 2BSTAR      ,CCPC(4)    ,CCPG(4)     ,CHARPT(10)  ,CKC(1..)   ,CHD24340
 3COEFT(4,10) ,CONDc    ,CONDV(100)  ,CONST(4,10) ,COVFRX(100) ,CHD24350
 4CPBAR      ,CPC       ,CPV(100)    ,DIFRFC     ,UMATER(10)  ,CHD24360
 5EFCOLC     ,EFCCLS    ,EFCOLV(4,10), FMIS(10)   ,EMISC      ,CHD24370
 6HOFM(10)   ,HCOM      ,HCOMG       ,HSUR        ,MAT(100)   ,CHD24380
 7MATOMN     ,MATMNf    ,MN          ,NN          ,NNP         ,CHD24390
 8NNSAVF     ,NRDIV     ,NREND       ,NRGO        ,NST         ,CHD24400
 9PARTIN(101) ,PHI      ,QBYRAD     ,QCOMB       ,QEXTR      ,CHD24410
10GPCOM      ,QSUBL     ,REC PRO    ,REORDC    ,REORDS    ,CHD24420
2REORDV(4,10),RHOFZ    ,RHOF(305)  ,RHOCPX(101) ,RHOC       ,CHD24430
3RHOFV(10)   ,SABL      ,SABLc       ,SDOT        ,SDOTC      ,CHD24440
4SLOPE(10)   ,TMELT(10) ,TSZ         ,TS(205)    ,TRCHAR    ,CHD24450
5WFZ         ,WF(205)   ,XCHAR       ,XINIT      ,XLEFT(101) ,CHD24460
6XMASS       ,XMDOTC   ,XMDOTD    ,XMDOTG    ,XMDOTL   ,CHD24470
7XMODTP     ,XMDOTS   ,XTOTAL     ,XVIRG(101) ,XZONE     ,CHD24480
  COMMON /BLOCKC/
1PLPRFS(20,11) ,COMMEX ,CUTOFF     ,F(20,11)   ,CHD24490
2FLOW(20,11)  ,HCONV(20,11),IFRROR ,JUNCT     ,L           ,CHD24500
3N          ,NOSECH   ,QBACK      ,QCONV(20,11),QGAS(20,11),CHD24510
4QMISC      ,TIME      ,TPRINT     ,TWALL(20,11),XIWALL(20,11),CHD24520
5XIR(20,11)
 IF (TIME-450.) 10,20,20
10 CONTINUF
  XKOE=.23144
  XMDOTO=PHI*HCONV(N,L)*XKOE
  XMDOTB=XKOE*DIFREC*XMDOTG/(BSTAR+1.E-10)
  QGPCOM=HCOMG*AMIN1(XMDOTO,XMDOTB)
  RETURN
20 CONTINUF
  QGPCOM=0.
  RETURN
END

```

```

- FOR GRIN,GRIN
  SUBROUTINE GRIN(IGI)                                     CHD24680
C***   CHARM SUBROUTINE IN CHAP --JULY 1966 VERSION      CHD24690
C   LISTING FOR GAUDFTF 8528 TAPE                         CHD24700
  COMMON /BLOCKA/
1ABSRD(10) ,ABSC ,ACTENC ,ACTENS ,ACTENV(4,10), CHD24720
2RSTAR ,CCPC(4) ,CCPG(4) ,CHARPT(101) ,CKC(4) ,CHD24730
3COEFT(4,10) ,COND C ,CONDV(100) ,CONST(4,10) ,COVERX(100) ,CHD24740
4CPBAR ,CPC ,CPV(100) ,DIFRFC ,UMATER(10) ,CHD24750
5EFCOLC ,EFCOLS ,EFCOLV(4,10),EMIS(10) ,FMISC ,CHD24760
6HGF M(10) ,HCOM ,HCOMG ,HSUB ,MAT(100) ,CHD24770
7MATMN ,MATMNF ,MN ,NN ,NNP ,CHD24780
8NNSAVE ,NRDIV ,NREND ,NRGO ,NST ,CHD24790
9PARTIN(101) ,PHI ,QBYRAD ,QCOMB ,QFXTR ,CHD24800
10GPCOM ,QSUPL ,RECPRO ,REORDC ,REORDS ,CHD24810
2REORDV(4,10) ,RH05Z ,RH05(205) ,RHOCPX(101) ,RHOC ,CHD24820
3RH0V(10) ,SABL ,SABL C ,SDOT ,SDOTC ,CHD24830
4SLOPE(10) ,TMELT(10) ,TSZ ,TS(205) ,TRCHAR ,CHD24840
5WFZ ,WF(205) ,XCHAR ,XINIT ,XLEFT(101) ,CHD24850
6XMASS ,XMDOTC ,XMDOTD ,XMDOTG ,XMDOTL ,CHD24830
7XMDOTR ,XMDOTS ,XTOTAL ,XVIRG(101) ,XZONE ,CHD24870
  COMMON /BLOCKC/
1BLPRES(20,11) ,COMM A X ,CUTOFF ,F(20,11) ,CHD24890
2FLOW(20,11) ,HCONV(20,11) ,IERROR ,JUNCT ,L ,CHD24900
3N ,NOSECH ,QBACK ,QCONV(20,11) ,QGAS(20,11) ,CHD24910
4QMISC ,TIME ,TPRINT ,TWALL(20,11) ,XIWALL(20,11) ,CHD24920
5XIR(20,11) ,CHD24930
  COMMON /BLOCKJ/
1FLUXI(200) ,TEDEP(200) ,XEDEP(101) ,EDEP(101) ,NTFDEP ,CHD24950
2NXFDEP ,ITEFPF ,EDFLUX(100) ,CHD24960
  COMMON /BLOCKK/NN1 ,QCOND(205) ,CHD24970
  COMMON /BLOCKN/COORD ,CHD24980
  COMMON /BLOCKR/DIFC(4) ,EROC(4) ,ERODE ,CHD24990
  COMMON /CHCOM/ DTAU, IBE(10), IBS(10), IBSPN, CHD25000
1IGTYP(10), IHDN(4), IM, IZB(3), IZG(3,10), CHD25010
2IZGT(3), JRSW, NCSN(10), NSHL(3), NSHR(3), CHD25020
3NZEN(7), NZSN(3), RH01(205), RH02(205), RH09(410), CHD25030
4I ,TEMPA2(205),TEMPA3(42),TEMPA4(42),TEMPA5(205), CHD25040
5 DELX(100),DISTL(100),DUM (10),ICOM, CHD25050
6IYS,LFT,MG,MDUM,NCEN(10),NCUT,ND(3),NLZON,SN,SN1, CHD25060
7SCHECK ,CHD25070
  COMMON /DACOM/ A(42),
1ABVAL ,ABVALM,ABVALS,B(42) ,C(42) ,CC(205),COND(42), CHD25090
2COND X ,CONDXX, D(42) ,DD(205),DELT X(101),DGAS,DQ, CHD25100
3DTAU ,DTAUS ,DTF,DTR(3),EDFX,FDFXX,FMI(42), CHD25110
4ETA,ETAS,FHT(42),FHTX,FHTXX,GAGC,GAS1,GK,GX,GY,GZ, CHD25120
5HDA(5,10),IBSPM,IERR,IGC,IGL,IGLD,IGR,IGRL,IGT,IG2, CHD25130
6IHYS,INEG,IN1,IN2,IP,IPLUS,ITER,ITERT,IX,IY,IZ,J,JBE, CHD25140
7JBEM,JBEX,JBD1,JBD2,JBS,JBSM,JASPM,JASPN,JBX,JRX,JCEN, CHD25150
8JCENM,JCSN,JCSNM,JE,JE1,JE2,JHDN,JHDN1,JLSW,JSLAB,JX,JZ, CHD25160
9K1,LANDID,LRT,MARK,NADD(42),NASW,NBNDST,NBND1(11), CHD25170
1NB SW,ND C,ND CM,NLSW(10),NOF,NOTIME,NPBSW,NPE1N,NPS2N,NPTSW, CHD25180
2NRID,NRIDC,NRSW(10),NRZON,NSLAB(10),NSLABH(10),NSW,NXSW, CHD25190
3NZON,NZONC,ONE,PSI,QSAVE,QTOT,QTOTAL,REFCTR,SBK,SDN, CHD25200
4SDCTN,SNS,SRA,TAR,TAUOUT,TAUST(3),TAU1,TAU2,TAU2S,TEMPA, CHD25210

```

```

51EMPST(3),THREE,TWO,WFP,WFX,WXXX,XI,XMCOM,XSAVE           CHD25220
DIMENSION NRND2(10),NHDN(3)                                CHD25230
EQUIVALENCE (NBND1(2),NBND2(1))                           CHD25240
EQUIVALENCE (IHDN(2),NHDN(1))                           CHD25250
JRS = IRS(IG)                                              CHD25260
JRSM = JRS-1                                              CHD25270
JLSW = NLSW(IG)                                             CHD25280
JRSW = NRSW(IG)                                             CHD25290
JF1 = NSLABH(IG)                                           CHD25300
JF = JE1+1                                                 CHD25310
JE2 = JE1-1                                                 CHD25320
JBND1 = NBND1(IG)-1                                       CHD25330
JBND2 = NBND2(IG)                                           CHD25340
IGL = IG-1                                                 CHD25350
JRF = IRF(IG)                                              CHD25360
JBEM = JRE-1                                              CHD25370
JCSN = NCEN(IG)                                            CHD25380
JCEN = NCEN(IG)                                            CHD25390
JCSNM=JCSN-1                                              CHD25400
JCENM = JCEN-1                                             CHD25410
IGC = IGTYP(IG)                                           CHD25420
JHDN = NHDN(IGC)                                           CHD25430
JSLAB = NSLAB(IG)                                           CHD25440
JRSPM = IRSNP+JCEN                                         CHD25450
JBSPN = JBSPM-1                                           CHD25460
RRETURN
END

```

```
- ASM INIT,INIT  
REGNAM  
*(1),INIT$ SX,1 R11,SAVEF  
M$SEA MIDOF$,+(SLJ STUFF?)  
M$SEA M$ERR$,+(J DIAG?)  
SAVE J 0  
END .
```

CHD25490
CHD25500
CHD25510
CHD25520
CHD25530
CHD25540

```

- FOR ITERS,ITER8
  SUBROUTINE ITER8(T,XI,Z,P,FCT,TOL,I)
    T1=T
    DO 4 N=1,100
      T2=FCT (T1,XI,Z ,P)
      T3=FCT (T2,XI,Z ,P)
      IF(T3)10,1,10
10  IF(ABS((T3-T2)/T3)-.0115,E,1
1  IF(T2-T1)11,2,11
11 A=(T3-T2)/(T2-T1)
12 IF(A-1.13)2,3
2  T1=T3
   GO TO 4
3  Q=A/(A-1.)
   T1=Q*T2+(1.-Q)*T3
   IF(T1)4,2,4
4  CONTINUE
   WRITE (6,1000)
1000 FORMAT(1H040X33HCONVERGENCE NOT ACHIEVED IN ITERS)
   WRITE(6,2000)T1,XI,Z,P
2000 FORMAT(1H030X4HT = E10.4,5X6HXI = E10.4,5X4HZ = E10.4,5X4HP = E10.CHD25740
14)
5  T=T3
   RETURN
   END

```

CHD25550
CHD25560
CHD25570
CHD25580
CHD25590
CHD25600
CHD25610
CHD25620
CHD25630
CHD25640
CHD25650
CHD25660
CHD25670
CHD25680
CHD25690
CHD25700
CHD25710
CHD25720
CHD25730
CHD25740
CHD25750
CHD25760
CHD25770
CHD25780

```
- FOR IWR,IWR
  SUBROUTINE IWR(Z,T,X)
  A=5400./T
  A=(2.-Z)*(2.5+A/(EXP(A)-1.))
  B=3.+106200./T
  IF(Z-1.216,6.3
  3  IF(Z-2.15,4,4
  4  ZERT=1.5*Z+(304200.*Z-424800.)/T
  GO TO 7
  5  ZERT=A+.2*B+(Z-1.21*(3.+203400./T)
  GO TO 7
  6  ZERT=A+(Z-1.)*B
  7  XI=.06855*T*(ZERT+Z)
  RETURN
END
```

CHD25790
CHD25800
CHD25810
CHD25820
CHD25830
CHD25840
CHD25850
CHD25860
CHD25870
CHD25880
CHD25890
CHD25900
CHD25910
CHD25920

```

- FOR LLD=LIC
  FUNCTION LLD(J)
    COMMON /CHCOM/ ITAL,    IBE(10),   IRS(10),   IRSPLN,
    IIGTYP(10),  IHDN(4),   IM,        IZB(3),    IZG(3,10),
    IIZGT(3),   JRSK,     NCEN(10),   NSHL(3),   NSHR(3),
    NZEN(3),   NZSN(3),   RHO1(305),  RHO2(305), RHO2(410),
    4I          ,TEMPA2(205),TEMPA3(42),TEMPA4(42),TEMPA5(205),
    5          DELX(100),DISTL(100),DUM(10),ITCM,
    6IYS,LFT,MG,MDUM,NCEN(10),NCUT,ND(3),NZON,SN,SN1,
    7SCHFCY
    IF (J=107) 5,6,6
  5 NZON=0
    LLD=J
    RETURN
  6 IF (J=187) 7,8,8
  7 NZON=1
    GO TO 9
  8 NZON=2
  9 K=J-IZB(NZON)
    KK=K/4
    LLD=NZSN(NZON) + KK
    RETURN
  END

```

```

- FOR MAIN,MAIN
  COMMON /BLOCKC/ USER(220),CC,MAX          CHD26150
  COMMON /BLOCKA/ FILL1(527),MAT(100),FILL2(3),NN,NNP,FILL3(5),PART1,CHD26153
  IN(101),FILL4(492),TS(20E)           CHD26157
  COMMON /DACOM/ UPRED(972),NASW,UPSIT(84),TAU1      CHD26160
  COMMON /TABCOM/ NDOTS(4),TIME1(100),TIME2(100),TIME3(100),
  TIME4(100),DSTEP(100),PSTEP(100),XRI(100),RH(100),OMU(100),    CHD26170
  TTT(100),PP(100),FF(100),AST(100)           CHD26180
  DIMENSION TITLE(12),NAMF(2)                 CHD26190
  TPRINT=0.                                     CHD26195
  NTART=0.                                     CHD26200
  TFND=1.F6                                    CHD26210
  TAU1=0.                                      CHD26220
  MTO=0.                                       CHD25230
  READ (5,990) TITLE                         CHD26233
  WRITE (6,992) TITLE                         CHD26235
  3 CONTINUF                                    CHD26238
  READ (5,1000) NTAB,NTYP                     CHD26240
  NTABT=NTABT+1                               CHD26250
  I=1                                         CHD26260
  INFRST=1                                    CHD26270
  5 CONTINUE                                    CHD26280
  GO TO (10,20,30,40),NTAB                     CHD26290
  10 CONTINUE                                   CHD26310
  READ (5,1010) TIME1(I)+DSTEP(I)            CHD26320
  TIMEZ = TIME1(I)                           CHD26330
  GO TO 50                                     CHD26340
  20 CONTINUF                                  CHD26350
  READ (5,1010) TIME2(I)+PSTEP(I)            CHD26360
  TIMEZ = TIME2(I)                           CHD26370
  GO TO 50                                     CHD26380
  30 CONTINUE                                   CHD26390
  GO TO (33,36),NTYP                         CHD26400
  33 READ (5,1010) TIME3(I),XRI(I),RH(I),OMU(I)
  GO TO 37                                     CHD26410
  36 READ (5,1010) TIME3(I),TT(I),RH(I)        CHD26420
  37 TIMEZ=TIME3(I)                           CHD26440
  NASW=NTYP                                    CHD26450
  GO TO 50                                     CHD26460
  40 CONTINUE                                   CHD26470
  READ (5,1010) TIME4(I),PP(I),FF(I),AST(I)
  TIMEZ=TIME4(I)                           CHD26480
  50 CONTINUE                                   CHD26490
  GO TO (62,60),INFRST                      CHD26500
  60 IF (TIMEZ-TIMEY) 70,70,65               CHD26510
  62 INFRST=2                                 CHD26520
  65 CONTINUF                                 CHD26530
  I=I+1                                       CHD26540
  TIMEY=TIMEZ                                CHD26550
  GO TO 5                                     CHD26560
  70 NDOTS(NTAR)=I-1                          CHD26580
  TEND=AMIN1(TEND,TIMFY)                    CHD26590
  IF (NTABT-4; 3,80,80)                      CHD26600
  80 CONTINUE                                 CHD26610
  NDOTSX=NDOTS(1)                           CHD26620

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```

        WRITE (6,1020) (TIME1(I),DSTEP(I),I=1,NDOTSX)           CHD26630
        NDOTSX=NDOTS(2)
        WRITE (6,1021) (TIME2(I),PSTEP(I),I=1,NDOTSX)           CHD26640
        NDOTSX=NDOTS(3)
        GO TO (90,95),NASW
90 CONTINUF
        WRITE (6,1024) (TIME3(I),XRI(I),RH(I),OMU(I),I=1,NDOTSX) CHD26650
        NDOTSX=NDOTS(4)
        GO TO 98
95 CONTINUF
        WRITE (6,1026) (TIME3(I),TT(I),RH(I),I=1,NDOTSX)          CHD26660
        NDOTSX=NDOTS(4)
98 CONTINUE
        WRITE (6,1028) (TIME4(I),PP(I),FF(I),AST(I),I=1,NDOTSX) CHD26670
        COMMAG=1.E-6
        WRITE (6,1030)
        NNP=0
99 CONTINUE
        NN=NNP
        READ (5,1031) MNO,NAME,WIDE,NUMERO
        IF (MNO) 112,112,110
110 NNP=NNP+NUMERO
        NN=NN+1
        WRITE (6,1C33) MNO,NAME,WIDE,NUMERO
        DWIDE=WIDE/FLOAT(NUMERO)
        MTO=MAX0(MTO,MNO)
        DO 111 J=NN,NNP
        MAT(J)=MNO
        PARTIN(J)=DWIDE
111 CONTINUF
        GO TO 99
112 NN=NNP
        NNP=NN+1
        READ (5,1032) TS(1)
        DO 113 J=1,100
113 TS(J)=TS(1)
        CALL OUTPUT (MTO)
        GO TO 109
100 IF (1.00001*TAU1-TPRINT) 104,102,102
102 CALL WRITE
        DPRINT=TBSTEP(TPRINT,TIME2,PSTEP,NDOTS(2))
        TPRINT=TPRINT+DPRINT
104 CONTINUE
        IF (TEND-1.00001*TAU1) 106,106,108
106 CALL EXIT
108 CONTINUE
        DPRINT=PRINT-TAU1
        DTEND=TEND-TAU1
        COMMAG=TBSTEP(TAU1,TIME1,DSTEP,NDOTS(1))
        COMMAG=AMIN1(COMMAG,DPRINT+DTEND)
        SET=1.E-6*TAU1
        COMMAG=AMAX1(COMMAG,SET)
109 CONTINUF
        CALL CHARM
        GO TO 100

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| 990 FORMAT (12A6) | CHD26913 |
| 992 FORMAT (4X12H TITLE---- 12A6//) | CHD26917 |
| 1000 FORMAT (2I10) | CHD26920 |
| 1010 FORMAT (4F10.0) | CHD26930 |
| 1020 FORMAT (1H09X35HCALCULATION TIME STEP CONTROL TABLE/19X4HTIME7X, 19HTIME STEP/19X5H(SEC)8X5H(SEC)/(F25.2,F13.4)) | CHD26940 |
| 1022 FORMAT (1H09X29HPRINT TIME STEP CONTROL TABLE/19X4HTIME7X, 19HTIME STEP/19X5H(SEC)8X5H(SEC)/(F25.2,F13.4)) | CHD26950 |
| 1024 FORMAT (1H0.9X23HSURFACE HEAT FLUX TABLE/ 119X4HTIME8X8HRECCOVRY3X1CHHEAT TRANSFER3X9HMISC HEAT/ 231X8HENTHALPY5X9HPARAMETER5X1H TO SURFACE/19X5H(SEC)6X9H(BTU/LBM)) | CHD26960 |
| 33X13H(LBM/FT2-SEC)3X9H(BTU/SEC)/(F25.2,F13.2,F13.5,F15.3)) | CHD26977 |
| 1026 FORMAT (1H0.9X25HSURFACE TEMPERATURE TABLE/19X4HTIME6X11HTEMPERATUHD26980 1RE2X13HHEAT TRANSFER/44X9HPARAMETER/19X5H(SEC)7X7H(DEG R14X13H(LBMCHD26981 2/FT2-SEC)/(F25.2,F13.2,F13.5)) | CHD26987 |
| 1028 FORMAT (1H0.9X44HLOCAL STATIC PRESSURE AND FLOW CONTROL TABLE/ 119X4HTIME6X9HLOC PRESS4X4HFLOW4X12HLOCAL STRESS/19X5H(SEC)15X9H(LBFCHD26991 2/FT2)4X4H(--15X9H(LBF/IN2)/(F25.2,F13.4,F8.0,F13.4)) | CHD26992 |
| 1030 FORMAT (1H19X9HMATERIALS//15X36HMATERIAL NAME THICKNESS NUMBERCHD26993 1 OF/33X4H(IN)17X5HNODES) | CHD26996 |
| 1031 FORMAT (I10.2A6,F18.4,I10) | CHD26997 |
| 1032 FORMAT (F10.4) | CHD26998 |
| 1033 FORMAT (13X,1H(I1,1H)2A6,F10.4,I9) END | CHD27000 |
| | CHD27010 |

- FOR MOLWT,MOLWT
 SUBROUTINE MOLWT
 COMMON /BLOCKA/
 1ABSORP(10) ,ABSC ,ACTENC ,ACTFNS ,ACTENV(4,10) ,CHD27020
 2BSTAR ,CCPC(4) ,CCPG(4) ,CHARPT(101) ,CKC(4) ,CHD27030
 3COEFT(4,10) ,CONDc ,CONDV(100) ,CONST(4,10) ,COVERX(100) ,CHD27060
 4CPRAA ,CPC ,CPV(100) ,DIFREC ,SUMATFR(10) ,CHD27070
 5EFCOLC ,EFCOLS ,EFCOLV(4,10) ,EMIS(10) ,EMISC ,CHD27080
 6HOFM(10) ,HCOM ,HCOMG ,HSUB ,MAT(100) ,CHD27090
 7MATOMN ,MATMNF ,MN ,MN ,NNP ,CHD27100
 8NNSAVE ,NRDIV ,NREND ,NRGO ,NST ,CHD27110
 9PARTIN(101) ,PHI ,OBYRAD ,OCOMB ,OEXTR ,CHD27120
 10PCOM ,QSURL ,RFCPRO ,RFORDC ,PFORDS ,CHD27130
 2RECORDV(4,10) ,RH052 ,RH05(205) ,RH0CPX(101) ,RHOC ,CHD27140
 3PHOV(10) ,SABL ,SABLc ,SDOT ,SDOTC ,CHD27150
 4SLOPE(10) ,TMELT(10) ,TSZ ,TS(205) ,TRCHAR ,CHD27160
 5WFZ ,WF(205) ,XCHAR ,XINIT ,XLFFT(101) ,CHD27170
 6XMASS ,XMDOTC ,XMDOTD ,XMDOTG ,XMDOTL ,CHD27180
 7XMDOTR ,XMDOTS ,XTOTAL ,XVIRG(101) ,XZONF ,CHD27190
 COMMON/BLOCKC/
 1BLPRES(20,11) ,COMMAX ,CUTOFF ,F(20,11) ,CHD27200
 2FLOW(20,11) ,HCONV(20,11) ,IERROR ,JUNCT ,L ,CHD27210
 3N ,NOSFCH ,OBACK ,QCONV(20,11) ,QGAS(20,11) ,CHD27220
 40MISC ,TIME ,TPRINT ,TWALL(20,11) ,XIWALL(20,11) ,CHD27240
 5>IR(20,11) ,CHD27250
 COMMON /BLOCKJ/
 1FLUXI(200) ,TEDEP(200) ,XFDEP(101) ,EDEP(101) ,NTFDEP ,CHD27260
 2NXFDEP ,ITFPFP ,FDFLUX(100) ,CHD27280
 COMMON /BLOCKK/NN1,QCOND(205) ,CHD27290
 COMMON/BLOCKN/COORD ,CHD27300
 COMMON/BLOCKR/DIFC(4) ,FROC(4) ,ERODF ,CHD27310
 COMMON /CHCOM/ DTAU, IBE(101), IRS(101), IRSPLN, CHD27320
 1IGTYP(10), IHDN(4), IM, IZB(31), IZG(3,10), CHD27330
 2IZGT(3), JRSW, NCSN(10), NSHL(31), NSHP(3), CHD27340
 3NZEN(3), NZSN(3), RH01(305), RH02(305), RH03(410), CHD27350
 4I ,TEMPA2(205), TEMPA3(42), TEMPA4(42), TEMPA5(205), CHD27360
 5 DELX(100) ,DISTL(100), DUM (10), ICOM, CHD27370
 6IYS,LFT, MG, MDUM, NCEN(10), NCUT, ND(3), NLZON, SN, SN1, CHD27380
 7SCHECK ,CHD27390
 COMMON/NUCOM/ NADA, CHD27400
 1EM(42) ,CHD27410
 COMMON /DACOM/ A(42),
 1ABVAL ,ABVALM, ABVALS,B(42) ,C(42) ,CC(205),COND(42), CHD27420
 2CONDx ,CONDxx, D(42) ,DD(205) ,DELFX(101),DGAS,DQ, CHD27430
 3DTAUC ,DTAUS ,DTF,DTR(3),EDFX,EDFXX,EMI(42), CHD27440
 4ETA,ETAS,FHT(42),FHTX,FHTXX,GAGC,GAS1,GK,GX,GY,GZ, CHD27450
 5HDA(5,10),IBSPM,IERR,IGC,IGL,IGLD,IGR,IGRL,IGT,IG2, CHD27460
 6IHYS,INEG,IN1,IN2,IP,IPLUS,ITER,ITERT,IX,IY,IZ,J,JBE, CHD27470
 7JBEM,JBEX,JBND1,JBND2,JBS,JBSM,JBSPLN,JRX,JRX,JCFN, CHD27480
 8JCENM,JCSN,JCSNM,JE,JE1,JE2,JHDN,JHDN1,JLSW,JSLAR,JX,JZ, CHD27490
 9K1,LANDID,LRT,MARK,NADD(42),NASW,NBNDST,NBND1(11), CHD27500
 1NBSW,NDC,NDCM,NLSW(10),NOF,NOTIME,NPBSW,NPE1N,NPS2N,NPTSW, CHD27510
 2NRID,NRIDC,NRSW(10),NRZON,NSLAB(10),NSLABH(10),NSW,NXSW, CHD27520
 3NZON,NZONC,ONE,PSI,QSAVE,QTOT,QTOTAL,REFCTR,SBK,SDN, CHD27530
 4SDOTN,SNS,SRA,TAR,TAUOUT,TAUST(3),TAU1,TAU2,TAU2S,TEMPO, CHD27540
 CHD27550

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STEMPSI(3),THREE,TWO,WFP,WFX,WXXX,XI,XMCOM,XSAVE CHD27560
COMMON /NASCOM/ CHAPRO,AIRM,
1CARBN1(205),CARBN5(205),SILCA1(205),SILCA5(205),PYRO(205),DEP(205)CHD27580
2,HYD(205),AERO(205),AERN(205),BURN(205),WFD(205), WDFP(205),WSI(205)CHD27590
351,WBRN(205),EMWT(205),PRG(205) CHD27600
4,TIMFX(50),TFT(50),NPTS CHD27610
5,POR(205),PERM1(205),PERM2(205),VISC(205),CCON,RHOTS,CART,,SILTS, CHD27620
6PORT,PERT1,PERT2,DCOH,DCOO,DCOPY,DCODP,DCOSI,DCOCM,DCON,CFXH,CFXO,CHD27630
7CFXPY,CFXDP,CFXSI,CFXCM,CFXN,DIFCO(205),SOX(205) CHD27640
8,ALLGAS(205),GRAF1(205),GRAF5(205),SPEED(205),DIFCH(205),DIFR(205)CHD27650
9,VISCO,VISCON,AF,BF,SILICA,REQ,PMW,DMW,HMW,AOMW,ANMW,SMW,BMW,CX(6)CHD27660
DIMENSION NBND1(10),NBND2(10),NHDN(3) CHD27670
EQUIVALENCE (NBND1(2),NBND2(1)) CHD27680
EQUIVALENCE (IHDN(2),NHDN(1)) CHD27690
EQUIVALENCE (TEMPA1(1),TS(1)),(DELTAX(1),PARTIN(1)) CHD27700
DIMENSION DELTAX(1),TEMPA1(1) CHD27710
DO 100 IG=IGR,MG CHD27720
CALL GRIN(IG) CHD27730
IF (IG-IGR) 30,30,20 CHD27740
20 CONTINUE CHD27750
ALLGAS(JBS)=ALLGAS(JBEX) CHD27760
EMWT(JBS)=EMWT(JBEX) CHD27770
KK=JBS+1 CHD27780
GO TO 40 CHD27790
30 KK=JBS CHD27800
40 DO 50 J=KK,JBF CHD27810
ALLGAS(J)=PYRO(J)+DEP(J)+HYD(J)+AERO(J)+AERN(J)+SOX(J)+BURN(J) CHD27820
1+1.E-20 CHD27830
EMWT(J)=ALLGAS(J)/(PYRO(J)/PMW+DEP(J)/DMW+HYD(J)/HMW+AERO(J)/AOMW CHD27840
1+AERN(J)/ANMW+SOX(J)/SMW+BURN(J)/BMW+5.F-22) CHD27850
50 CONTINUE CHD27860
JBEX=JBE CHD27870
100 CONTINUE CHD27880
IF (IGR-1) 205,205,210 CHD27890
205 IGRL=1 CHD27900
GO TO 215 CHD27910
210 IGRL=IGR-1 CHD27920
215 CONTINUE CHD27930
JBEX=JBS(IGR) CHD27940
DO 250 IG=1,IGRL CHD27950
CALL GRIN(IG) CHD27960
DO 230 J=JBS,JBE CHD27970
EMWT(J)=FMWT(JBEX) CHD27980
230 ALLGAS(J)=ALLGAS(JBEX) CHD27990
250 CONTINUE CHD28000
RETURN CHD28010
END CHD28020

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- FOR PCAPF,PCAPP
FUNCTION PCAPF(K)                                              CHD28030
C*** THE PCAPF SUBROUTINE CALCULATES THE DENSITY-SPECIFIC HEAT PRODUC HD28040
DIMENSION NHDN(31), RH04(106)                                     CHD28050
DIMENSION DFLTAX(11), TEMPA1(11)                                    CHD28060
COMMON /RLOCKA/
1ABSORP(10) ,ABSC      ,ACTENC      ,ACTENS      ,ACTENV(4,10), CHD28080
2BSTAR   ,CCPC(4)     ,CCPG(4)     ,CHARPT(101) ,CKC(4)      ,CHD28090
3COEFT(4,10) ,COND C ,CONDV(100) ,CONST(4,10) ,COVERX(100) ,CHD28100
4CPBAR    ,CPC        ,CDUMI(100) ,DIFREC      ,UMATER(10) ,CHD28110
5EFCOLC   ,EFCOLS    ,EFCOLV(4,10) ,EMIS(10)  ,EMISC      ,CHD28120
6HOFM(10) ,HCOM       ,HCOMG       ,HSUB        ,MAT(100)  ,CHD28130
7MATOMN   ,MATMN F   ,MN          ,NN          ,NNP         ,CHD28140
8NNSAVF   ,NRDIV     ,NREND       ,NRGO        ,NST         ,CHD28150
9PARTIN(101) ,PHI     ,QBYRAD     ,QCUMB      ,QEXTR      ,CHD28160
10GPCOM   ,QSUBL     ,RECPRO      ,PEORDC     ,REORDS    ,CHD28170
2REORDV(4,10) ,RH052  ,RH05(305) ,RHOGPX(101) ,RHOC       ,CHD28180
3RH0V(10) ,SABL      ,SABLC       ,SDOT        ,SDOTC     ,CHD28190
4SLOPE(10) ,TMELT(10) ,TSZ         ,TS(205)    ,TRCHAR    ,CHD28200
5WFZ      ,WF(205)   ,XCHAR       ,XINIT      ,XLEFT(101) ,CHD28210
6XMASS    ,XMDOTC   ,XMDOTD    ,XMDOTG    ,XMDOTL   ,CHD28220
7XMDOTR   ,XMDOTS   ,XTOTAL      ,XVIRG(101) ,XZONE    ,CHD28230
COMMON/BLOCKC/
1BLPRES(20,11) ,COMM AX ,CUTOFF     ,F(20,11)  ,      CHD28240
2FLOW(20,11) ,HCONV(20,11) ,IERROR    ,JUNCT     ,L          CHD28250
3N        ,NOSECH   ,QBACK      ,QCONV(20,11) ,QGAS(20,11) ,CHD28260
4QMISC   ,TIME      ,TPRINT     ,TWALL(20,11) ,XIWALL(20,11) ,CHD28270
5XIR(20,11)
COMMON /FCOM/ DTAU, IBE(10), IBS(10), IBSPN, CHD28300
1IGTYP(10), IHDN(4), IM, IZB(2), IZG(2,10), CHD28310
2IZGT(3), JRSW, NCSN(12), NSHL(3), NSHR(3), CHD28320
3NZEN(3), NZSN(3), RH01(305), RH02(305), RH03(410), CHD28330
4I        ,TEMPA2(205), TEMPA3(42), TEMPA4(42), TEMPA5(205), CHD28340
5       ,DELX(100), DISTL(100), DUM(10), ICOM, CHD28350
6IYS,LFT,MG,MDUM,NCEN(10),NCUT,ND(3),NLZON,SN,SN1, CHD28360
7SCHFCK
COMMON /DACOM/ A(42),
1ABVAL ,ABVALM,ABVALS,B(42),C(42), CC(205),COND(42), CHD28380
2COND X,CONDXX, D(42),DD(205),DELTX(101),DGAS,DQ, CHD28390
3DTAUC ,DTAUS ,DTF,DTR(3),EDFX,EDFXX,EMI(42), CHD28400
4ETA,ETAS,FHT(42),FHTX,FHTXX,GAGC,GAS1,GK,GX,GY,GZ, CHD28410
5HDA(5,10),IBSPM,IERR,IGC,IGL,IGLD,IGR,IGRL,IGT,IG2, CHD28420
6IHYS,INEG,IN1,IN2,IP,IPLUS,ITER,ITERT,IX,IY,IZ,J,JBE, CHD28430
7JBEM,JBEX,JBND,JBND2,JBSM,JBSPM,JBSPN,JBX,JBXX,JCEN, CHD28440
8JCENM,JCSNM,JCSNM,JE,JE1,JE2,JHDN,JHDN1,JLSW,JSLAB,JX,JZ, CHD28450
9K1,LANDID,LRT,MARK,NADD(42),NASW,NB,DST,NBND1(11), CHD28460
1NB SW,NDC,NDCM,NL SW(10),NOF,NOTIME,NPBSW,NPE1N,NPS2N,NF,SW, CHD28470
2NRID,NRIDC,NRSW(10),NRZON,NSLAB(10),NSLABH(10),NSW,NXSW, CHD28480
3NZON,NZONC,ONE,PSI,QSAVE,QTOT,QTOTAL,REFCTR,SBK,SDN, CHD28490
4SDOTN,SNS,SRA,TAR,TAUOUT,TAUST(3),TAU1,TAU2,TAU2S,TEMPA, CHD28500
5TEM,ST(3),THREE,TWO,WFP,WFX,WFX,XI,XMCOM,XSAVE CHD28510
COMMON /NASCOM/ CHARR,AIRM,
1CARBN1(205),CARBN5(205),SILCA1(205),SILCA5(205),PYRO(205),DEP(205)CHD28540
2,HYD(205),AERO(205),AERN(205),BURN(205),WFD(205), WDEP(205),WSI(20)CHD28550
3,WPBN(205),EMWT(205),PRG(205) CHD28560

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4,TIMEX(50),TFT(50)+NPTS CHD28570
5,POR(205),PERM1(205),PERM2(205),VISC(205),GCON,RHOTS,CARTS,SILTS, CHD28580
6,PORT,PERT1,PERT2,DCOH,DCOQ,DCOPY,DCODP,DCOSI,DCOCM,DCON,CFXH,CFXO,CHD28590
7,CFXPY,CFXDP,CFXS,CFXCM,CFIN,DFC0(205),SOX(205) CHD28600
8,ALLGAS(205),GRA 2051 CHD28610
EQUIVALENCE (IHD ),NHDN(1) CHD28620
EQUIVALENCE (RH03(103),RH04(1)) CHD28630
EQUIVALENCE (TEMPA1(1),TS(1)),(DELTAX(1),PARTIN(1)) CHD28640
EQUIVALENCE (MNOD,NNP) CHD28650
DIMENSION AREA(42),AREAV(42) CHD28660
EQUIVALENCE (RHOCPX(44),AREA11),AREAV(43)) CHD28670
KL=JBSM+K CHD28680
GO TO (13,7,7),JRSW CHD28690
7 CPC = CCPC(1)+TEMPA3(K)*(CCPC(2)+TEMPA3(K)*(CCPC(3)
1+TEMPA3(K)*CCPC(4))) CHD28700
1 CPC=CPC*(CARBN1(KL)+GRAF1(KL)+SILCA1(KL))/RHOC CHD28710
13 CPV = COEFT(1,I)+TEMPA3(K)*(COEFT(2,I)+TEMPA3(K)*
1(COEFT(3,I)+TEMPA3(K)*COEFT(4,I))) CHD28730
CPV=CPV+RH03(K)/RH0V(I) CHD28740
GO TO (15,17,17),JRSW CHD28750
15 PCAPF = CPV CHD28760
GO TO 18 CHD28770
17 PCAPF=CPV+CPC CHD28780
18 PCAPF=PCAPF+DELTAX(IM)*AREAV(K)/DTAU+1.E-20) CHD28790
RETURN CHD28800
END CHD28810
CHD28620

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- ASM PICKUP,PICKUP
 PICKUP S AO,WORK
 L AO,1,R11
 S,HI AO,PICK1
 L AO,*0,R11
 S,HL AO,PICK2
 PIC1 L AO,\$-\$
 PICK1 S AO,\$-\$
 L AO,WORK
 J 2,R11
 WORK RFS 1
 JFACTO
 REGNAM
 END .

SAVE AO
 SET ADDR TO FILL
 PICK UP LOC TO PICKUP
 • SET ADDR TO PICKUP
 PICKUP CONTENTS
 MOVE
 RESTORE AO
 RETURN

CHD28830
 CHD28840
 CHD28850
 CHD28860
 CHD28870
 CHD28880
 CHD28890
 CHD28900
 CHD28910
 CHD28920
 CHD28930
 CHD28940
 CHD28950

- FOR PORE, PORE

| | | | | |
|--|---------------|-----------------------------|----------------|------------|
| SURROUNING PORE | | | | CHD28960 |
| COMMON /BLOCKA/ | | | | CHD28970 |
| 1ABSORP(10), ABSC | ,ACTENC | ,ACTENS | ,ACTENV(4,10), | CHD28980 |
| 2BSTAR ,CCPC(4) | ,CCPG(4) | ,CHARPT(101) | ,CKC(4) | , CHD28990 |
| 3COEFF(4,10) ,COND C | ,CONDV(100) | ,CONST(4,10) | ,COVERX(100) | , CHD29000 |
| 4CPBAR ,CPC | ,CPV(100) | ,DIFREC | ,UMATER(10) | , CHD29010 |
| 5EFCOLC ,EFCOLS | ,EFCOLV(4,10) | ,EMIS(10) | ,EMISC | , CHD29020 |
| 6HOFM(10) ,HCOM | ,HCOMG | ,HSUR | ,MAT(100) | , CHD29030 |
| 7MATOMN ,MATMNE | ,MN | ,NN | ,NNP | , CHD29040 |
| 8NNSAVE ,NRDIV | ,NPEND | ,NRGO | ,NST | , CHD29050 |
| 9PARTIN(101) ,PHI | ,QBYRAD | ,QCOMR | ,QEXTP | , CHD29060 |
| 10GPCOM ,QSUBL | ,RECPRO | ,REORDC | ,REORDS | , CHD29070 |
| 2REORDV(4,10) ,RHOFZ | ,RHOF(305) | ,PHOCPX(101) | ,RHQC | , CHD29080 |
| 3RHOV(10) ,SABL | ,SABLC | ,SDOT | ,SDOTC | , CHD29090 |
| 4SLOPE(10) ,TMELT(10) | ,TSZ | ,TS(205) | ,TRCHAR | , CHD29100 |
| 5WFZ ,WF(205) | ,XCHAR | ,XTINIT | ,XLEFT(101) | , CHD29110 |
| 6XMASS ,XMDOTC | ,XMDOTD | ,XMDOTG | ,XMDOTL | , CHD29120 |
| 7XMDOTR ,XMDOTS | ,XTOTAL | ,XVIRG(101) | ,XZONF | CHD29130 |
| COMMON/BLOCKC/ | | | | CHD29140 |
| 1BLPRES(20,11) | ,COMMEX | ,CUTOFF | ,F(20,11) | , CHD29150 |
| 2FLOW(20,11) ,HCONV(20,11),IEROR | | ,JUNCT | ,L | , CHD29160 |
| 3N ,NOSECH | ,QBACK | ,QCONV(20,11),QGAS(20,11) | , CHD29170 | |
| 4QMISC ,TIME | ,TPRINT | ,TWALL(20,11),XIWALL(20,11) | , CHD29180 | |
| 5XIR(20,11) | | | | CHD29190 |
| COMMON /BLOCKJ/ | | | | CHD29200 |
| 1FLUXI(200),TEDEP(200),XEDEP(101),EDEP(101),NTFDFP, | | | | CHD29210 |
| 2NXEDEP,ITEPEP,EDFLUX(100) | | | | CHD29220 |
| COMMON /BLOCKK/NN1,QCOND(205) | | | | CHD29230 |
| COMMON/BLOCKN/CCORD | | | | CHD29240 |
| COMMON/BLOCKR/DIFC(4),EROC(4),ERODE | | | | CHD29250 |
| COMMON /CHCOM/ DTAU, IBE(10), TBS(10), IBSPN, | | | | CHD29260 |
| 1IGTYP(10), IHDN(4), IM, IZB(3), IZG(3,10), | | | | CHD29270 |
| 2IZGT(3), JRSW, NCSN(10), NSHL(3), NSHR(3), | | | | CHD29280 |
| 3NZEN(3), NZSN(3), RH01(305), RH02(305), RH03(410), | | | | CHD29290 |
| 4I ,TEMPA2(205),TEMPA3(42),TEMPA4(42),TEMPS(205), | | | | CHD29300 |
| 5 DELX(100),DISTL(100),DUM(10),ICOM, | | | | CHD29310 |
| 6IYS,LFT,MG,MDUM,NCEN(10),NCUT,ND(3),NLZON,SN,SN1, | | | | CHD29320 |
| 7SCHECK | | | | CHD29330 |
| COMMON /NUCOM/ DX(205),XNHD(205),NADA(42),MATA(205), | | | | CHD29340 |
| 1EM(42) | | | | CHD29350 |
| COMMON /DACOM/ A(42), | | | | CHD29360 |
| 1ABVAL ,ABVALM,ABVALS,B(42),C(42), CC(205),COND(42), | | | | CHD29370 |
| 2CONDX ,CONDXX, D(42), DD(205),DELTX(101),DGAS,DO, | | | | CHD29380 |
| 3DTAUC ,DTAUS ,DTAUX ,DTF,DTR(3),EDFX,EDFXX,EMI(42), | | | | CHD29390 |
| 4ETA,ETAS,FHT(42),FHTX,FHTXX,GAGC,GAS1,GK,GX,GY,GZ, | | | | CHD29400 |
| 5HDA(5,10),IBSPM,IERR,IGC,IGL,IGLD,IGR,IGRL,IGT,IG2, | | | | CHD29410 |
| 6IHYS,INEG,IN1,IN2,IP,IPLUS,ITER,ITERT,IX,IY,IZ,J,JBE, | | | | CHD29420 |
| 7JBEM,JBEX,JBND1,JBND2,JBS,JBSM,JRSPX,JRSPN,JBX,JRXX,JCEN, | | | | CHD29430 |
| 8JCENM,JCSN,JCSNM,JE,JE1,JE2,JHDN,JHDN1,JLSW,JSLAB,JX,JZ, | | | | CHD29440 |
| 9K1,LANDID,LRT,MARK,NADD(42),NASW,NBNDST,NBND1(11), | | | | CHD29450 |
| 1NBSW,NDC,NDCM,NLSW(10),NOF,NOTIME,NPSW,NPE1N,NPS2N,NPTSW, | | | | CHD29460 |
| 2NRID,NRIDC,NRSW(10),NRZON,NSLAB(10),NSLABH(10),NSW,NXSW, | | | | CHD29470 |
| 3NZON,NZONC,ONE,PSI,QSAVE,QTOT,QTOTAL,REFCTR,SBK,SDN, | | | | CHD29480 |
| 4SDOTN,SNS,SRA,TAR,TAUOUT,TAUST(3),TAU1,TAU2,TAU2S,TEMPA, | | | | CHD29490 |

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5 STEMPSI(2),THREE,TWS,WFP,WFX,WFXX,XI,XMCOM,XSAVF          CHD29500
COMMON /NASCOM/ CHAR0,AIRN,                                     CHD29510
1 CARBN1(205),CARBN5(205),SILCA1(205),SILCA5(205),PYRO(205),DEP(205)CHD29520
2 HYD(205),AFRO(205),AERN(205),BURN(205),WFD(205),WDFP(205),WSI(205)CHD29530
15 ,WBRN(205),FMWT(205),PRG(205)                                CHD29540
4,TIMFX(50),TET(50),NPTC                                         CHD29550
5,POR(205),PERM1(205),PERM2(205),VISCI(205),GC0N,RHOTS,CARTS,SILTS,CHD29560
6,PORT,PERT1,PERT2,DCOH,DCOG,DCOPY,DCODR,DCOSI,DCOCM,DCON,CFXH,CFXO,CHD29570
7,CFXPY,CFXDP,CFXS1,CFXCM,CFXN,DIFCO(205),SOX(205)           CHD29580
8,ALLGAS(205),GRAF1(205),GRAFS(205),SPEID(205),DIFCH(205),DIFR(205)CHD29590
9,VISCO,VISCON,AF,BF,SILICA,REC,PMW,DMW,HMW,AOMW,ANMW,SMW,RMW,CX(6)CHD29600
DIMENSION NHND(11),NHDN(3)                                       CHD29610
EQUIVALENCE (NHND(11),NHDN(1))                                     CHD29620
EQUIVALENCE (NHDN(2),NHDN(1))                                     CHD29630
DIMENSION TFMPA1(11)                                              CHD29640
EQUIVALENCE (TFMPA1(11),TS(1))                                     CHD29650
GO TO (10,20,101),JRSW                                         CHD29660
10 POR(J)=1.-(RH01(J)+RH0C)/RHOTS                               CHD29670
GO TO 30
20 POR(J)=1.-(SILCA1(J)/SILTS-(CARBN1(J)+GRAF1(J))/CARTS)    CHD29680
30 HOLD=POR(J)/PORT                                           CHD29700
SAVF=(1.-PORT)/(1.-POR(J))                                      CHD29710
PERM2(J)=HOLD*SAVF                                           CHD29720
ERM1(J)=PERM2(J)**2*HOLD*PERT1*(1.+.31A*TFMPA1(J)**1.4/(PRG(J)+1.)CHD29730
1E-15))                                                 CHD29740
PERM2(J)=PERM2(J)*HOLD*PERT2                                 CHD29750
C INSERT VISCOSITY DETERMINATION                               CHD29760
VISCI(J)=VISCO*(TFMPA1(J)/VISCON)**.7                         CHD29770
RETURN                                                       CHD29780
END

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- ECR RECFFD,RECFFD
  SUBROUTINE RECFFD(TEMPS)
  COMMON /BLOCKA/
  1ABSORP(10) ,ABSC      ,ACTENC      ,ACTENS      ,ACTENV(4,10) ,CHD29800
  2BSTAR      ,CCPC(4)   ,CCPG(4)    ,(HARPT(10)) ,CKC(4)      ,CHD29810
  3COEFT(4,10) ,COND C   ,CONDV(100) ,CONST(4,10) ,COVERX(100) ,CHD29840
  4CPBAR      ,CPC       ,CPV(100)   ,DIFREC      ,IJMATER(10) ,CHD29850
  5EFCOL C   ,EFCOLS    ,EFCOLV(4,10),FMIS(10) ,FMISC      ,CHD29860
  6HOFM(10)   ,HCOM      ,HCOMG      ,HSUB        ,MAT(10)    ,CHD29870
  7MATOMN    ,MATMNF    ,MN         ,NN          ,NNP        ,CHD29880
  8NNSAVE     ,NRDIV     ,NREND      ,NRGO        ,NST        ,CHD29890
  9PARTIN(10) ,PHT       ,OBYRAD    ,OCOMB      ,OEXTR      ,CHD29900
  10GPCOM    ,OSUBL     ,RECPR0    ,PEOPDC    ,RFORDS    ,CHD29910
  2REORDV(4,10),RH05Z   ,RH05(305) ,RHOCPX(101) ,PHOC      ,CHD29920
  3RHOV(10)   ,SABL      ,SABLC     ,SDOT        ,SDOTC    ,CHD29930
  4SLCPE(10)  ,TMELT(10) ,TSZ        ,TS(205)   ,TRCHAR    ,CHD29940
  5WFZ        ,WF(205)   ,XCHAR     ,XINIT      ,XLEFT(101) ,CHD29950
  6XMASS      ,XMDOTC   ,XMDOTD   ,XMDOTG    ,XMDOTL    ,CHD29960
  7XMODTR    ,XMDOTS   ,XTOTAL    ,XVIRG(101) ,XZONE     ,CHD29970
  COMMON /BLOCKC/
  1BLPRES(20,11) ,COMMEX   ,CUTOFF    ,F(20,11)  ,CHD29990
  2FLOW(20,11)  ,HCONV(20,11),IERROR   ,JUNCT     ,L          ,CHD30000
  3N           ,NOSECH   ,QBACK     ,QCONV(20,11),QGAS(20,11) ,CHD30010
  4QMISC      ,TIME      ,TPRINT    ,TWALL(20,11),XIWALL(20,11),CHD30020
  5XIR(20,11)  ,          ,          ,          ,          ,CHD30030
  COMMON/BLOCKR/DIFC(4),EROC(4),FRODF
C
C
C XMDOTR IS SPELLED XMODTR IN COMMON. WATCH THIS WHEN
C EXAMINING DUMPS AND WHFN CODING.
C
C
C EXTERNAL FRFC
  IF(XMDOTG>2,4
  2 XMDOTG=0.
  3 DIFREC=0.
  GO TO 6
  4 OMG=ALOG(XMDOTG*TWALL(N,L)**.5*(.12*(1.E4/TWALL(N,L)))
  1/(BLPRES(N,L)/2116.2))/2.3026
  DIFREC=DIFC(1)+OMG*(DIFC(2)+OMG*(DIFC(3)+OMG*DIFC(4)))
  6 XMDUM=BSTAR*HCONV(N,L)
  XMDOTD=XMDUM-XMDOTG*DIFREC
  IF(XMDOTD<-1.E-6)10,10,20
  10 XMDOTL=0.
  GO TO 30
  20 DR=EFCOL C*(BLPRES(N,L)/10077.)*REORDC
  XMDOTR=DR*EXP(-ACTENC/TEMPS)
  XMDOTR=XMDOTR
  IF(XMDOTR<-1.E-6)10,10,25
  25 RDUM=XMDOTD*BSTAR**REORDC/XMDOTR
  RDUM=(PHI*HCONV(N,L)+XMDOTG)/XMDOTD
  RK=1./BDUM
  CALL ITER8(RK,REORDC,RDUM,BDUM,FREC+1.E-3,11)
  XMDOTL=XMDOTD*(1.-BDUM*RK)/(1.+RK)
  30 DS=EFCOLS*XMDUM*(BLPRES(N,L)/2116.2)**(-REORDS)

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```
XMDOTS=DS*EXP1-ACTFNS/TEMPA)
IF(XMDOTS-1.E-6)40,40,50
40 XMDOTS=0.
50 XMDOTC=XMDOTL+XMDOTS
RETURN
END
```

CHD30340
CHD30350
CHD30360
CHD30370
CHD30380
CHD30390

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- FOR RHOSR,RHOSR
  SUBROUTINE RHOSR (K,KL)                               CHD30400
C**** THE RHOSR SUBROUTINE FINDS DATA NEEDED FOR DENSITY CALCULATIONS CHD30410
  DIMENSION DELTAX(1), TEMPA1(1)                      CHD30420
  DIMENSION AREAC(1),EMBM(1),PC(1),RATE(1),RH04(1),WFD(1)   CHD30430
  COMMON /BLOCKA/
 1ABSORP(10) ,ABSC      ,ACTENC      ,ACTENS      ,ACTENV(4,10), CHD30440
 2BSTAR    ,CCPC(4)     ,CCPG(4)      ,CHARPT(101) ,CKC(4)      , CHD30450
 3COEFT(4,10) ,CONDc    ,CONDV(100)   ,CONST(4,10) ,COVERX(100) , CHD30460
 4CPRAR    ,CPC        ,CPV(100)     ,CIEFEC      ,CUMATER(10) , CHD30470
 5EFCOLC   ,EFCOLS     ,EFCOLV(4,10) ,EMIS(10)   ,FMISC       , CHD30480
 6HOFM(10) ,HCOM       ,HCOMG       ,HSUP        ,MAT(100)   , CHD30490
 7MATOWN   ,MATMNf     ,MN          ,NN          ,NNND       , CHD30500
 8NNSAVE   ,NRDIV      ,NREND       ,NRGO        ,NST         , CHD30520
 9PARTIN(101) ,PHI      ,OBYRAD      ,OCOMR       ,OEXTR      , CHD30530
 10GPCOM   ,QSUBL      ,RFCPRO      ,REOPDC      ,REORDS     , CHD30540
 2REORD(1,101),RH05Z   ,RH05(305)   ,RH0CPX(101) ,RHOC       , CHD30550
 3RH0V(101) ,SABL      ,SABLc       ,SDOT        ,SDOTC      , CHD30560
 4SLOPE(10) ,TMELT(10) ,TSZ         ,TS(2-5)    ,TRCHAR     , CHD30570
 5WFZ      ,WF(205)    ,XCHAR       ,XINIT       ,XLEFT(101) , CHD30580
 6XMASS    ,XMDOTC     ,XMDOTD     ,XMDOTG     ,XMDOTL     , CHD30590
 7XMDOTR   ,XMDOTS     ,XTOTAL      ,XVIRG(101) ,XZONE      , CHD30600
  COMMON /CHCOM/ DTAU, IBE(10), IBS(10), IBSPN,      CHD30610
 1IGTYP(10), IHDN(4), IM, IZB(3), IZG(3,10),      CHD30620
 2IZGT(3), JRSW, NCSN(10), NSHL(3), NSHR(3),      CHD30630
 3NZEN(3), NZSN(3), RH01(305), RH02(305), RH03(410), CHD30640
 4I      ,TEMPA2(205), TEMPA3(42), TEMPA4(42), TEMPA5(205), CHD30650
 5      ,DELX(100), DISTL(100), DUM(10), ICOM,      CHD30660
 6IYS,LFT,MS,MDUM,NCEN(10),NCUT,ND(3),NLZON,SN,SN1, CHD30670
 7SCHECK
  EQUIVALENCE (TEMPA1(1),TS(1)),(DELTAX(1),PARTIN(1)) CHD30680
  EQUIVALENCE (EMBM(1),PC(1))                         CHD30690
  EQUIVALENCE (RH03(103),RH04(1))                      CHD30700
  EQUIVALENCE (WF(1),WFD(1),RATE(1))                  CHD30710
  EQUIVALENCE (RH03(307), PC(1)), (RH03(350),ARFAC(1)) CHD30720
  ONF = (3.3RH01(KL)+RH05(KL))/4.                      CHD30730
  ARFAC(K)=0.                                         CHD30740
  THREE=0.                                           CHD30750
  IF (ONE-1.E-10) 2727,2727,2720                     CHD30760
2720 CONTINUE                                         CHD30770
  DO 2725 J=1,2                                     CHD30780
  TWO = -EFCOLV(J,1)*EXP(-ACTENV(J,1)/TEMPA3(K))    CHD30790
  ARFAC(K) = TWO*RHO1(KL)**REORDV(J,1)+ARFAC(K)      CHD30800
  THREE=TWO*REORDV(J,1)*ONE**((REORDV(J,1)-1.1)+THREE) CHD30810
2725 CONTINUE                                         CHD30820
2727 CONTINUF                                         CHD30830
  EMBM(K) = 1.-THREE*DTAU/2.                          CHD30840
  IF (KL-205) 2730,2740,2740                        CHD30850
2730 RATE(KL)=THREE                                  CHD30860
2740 CONTINUE                                         CHD30870
  RETURN                                              CHD30880
  END                                                 CHD30890

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- FOR SHIFT1, SHIFT1
 SUBROUTINE SHIFT1 (NZON, NLR, INCOM) CHD30910
 **** THE SHIFT1 SURROUNTING INTERPOLATES NEW VALUES NEEDED FOR NODE CHD30920
 **** ADDITION TO A ZONE CHD30930
 DIMENSION NHDN(3), RH04(106) CHD30940
 DIMENSION DELTAX(11), TEMPAT(11) CHD30950
 COMMON /BLOCKA/
 1ABSORP(10) ,ABSC ,ACTENC ,ACTENS ,ACTENV(4,10); CHD30960
 2BSTAR ,CCPC(4) ,CCPG(4) ,CHARPT(10) ,CKC(4) ,CHD30980
 3COEFT(4,10) ,CONDc ,CONDV(100) ,CONST(4,10) ,COVEPX(100) ,CHD30990
 4CPBAR ,CPc ,CPV(100) ,DFRfc ,UMATER(10) ,CHD31000
 5EFCOLC ,EFCOLS ,EFCOLV(4,10) ,EMIS(10) ,EMISC ,CHD31010
 6HOFM(10) ,HCOM ,HCOMG ,HSUB ,MAT(100) ,CHD31020
 7MATOMN ,MATMNf ,MN ,NN ,NNP ,CHD31030
 8NNSAVE ,NRDIV ,NREND ,NRGO ,NST ,CHD31040
 9PARTIN(101) ,PHI ,QBYRAD ,QCOMP ,QEXTR ,CHD31050
 10GPCOM ,QSUBL ,RECPCRO ,RFORDC ,RFORDS ,CHD31060
 2REORDV(4,10),RH05Z ,RH05(305) ,RH05P(101) ,RHOC ,CHD31070
 3RH0V(10) ,SABL ,SABLc ,SDOT ,SDOTC ,CHD31080
 4SLOPE(10) ,TMELT(10) ,TSZ ,TS12051 ,TRCHAR ,CHD31090
 5WFZ ,WF(205) ,XCHAR ,XINIT ,XLEFT(101) ,CHD31100
 6XMASS ,XMDOTC ,XMDOTD ,XMDOTG ,XMDOTL ,CHD31110
 7XMDOTR ,XMDOTS ,XTOTAL ,XVIRG(101) ,XZONE ,CHD31120
 COMMON/BLOCKC/
 1BLPRES(20,11) ,COMMAX ,CUTOFF ,F(20,11) ,CHD31130
 2FLOW(20,11) ,HCONV(20,11),IERROR ,JUNCT ,L ,CHD31140
 3N ,NOSECH ,QBACK ,QLONV(20,11),QGAS(20,11) ,CHD31150
 40M!SC ,TIME ,TPRINT ,TWALL(20,11),XIWALL(20,11) ,CHD31160
 5XIR(20,11) ,
 COMMON /CHCOM/ DTAU, IBE(10), IRS(10), IRSPPN, CHD31170
 11GTYP(10), IHDN(4), IM, IZB(3), IZG(3,10), CHD31180
 212GT(3), JRSW, NCSN(10), NSHL(3), NSHR(3), CHD31190
 3NZen(3), NZSN(3), RH01(305), RH02(305), RH03(410), CHD31200
 4I ,TEMPA2(205),TEMPA3(42),TEMPA4(42),TEMPA5(205), CHD31210
 5 DELX(100),DISTL(100),DUM (10),ICOM, CHD31220
 6IYS,LFT,MG,MDUM,NCEN(10),NCUT,ND(3),NLZON,SN,SN1, CHD31230
 7SCHECK ,
 COMMON /NASCOM/ CHARRO,AIRM, CHD31240
 1CARBN(205),CARBN5(205),SILCA1(205),SILCA5(205),PYRO(205),DEP(205) CHD31250
 2+HYD(205),AERO(205),AERN(205),BURN(205),WFD(205), WDEP(205),WSI(20 CHD31260
 35),WBRN(205),EMWT(205),PRG(205) CHD31270
 4,TIMEX(50),TFT(50),NPTS CHD31280
 5,POR(205),PERM1(205),PERM2(205),VIS(205),GCON,RHOTS,CARTS,SILTS, CHD31290
 6PORT,PERT1,PERT2,DCOH,DC00,DCOPY,DCODP,DCOS1,DCOCM,DCON,CFXH,CFXO,CHD31300
 7CFXPY,CFXDP,CFXSI,(FXCM,CFXN,DFC0(205),SOX(205) CHD31310
 8,ALLGAS(205),GRAF1(205) CHD31320
 EQUIVALENCE (IHDN(2),NHDN(1)) CHD31330
 EQUIVALENCE (RH03(103),RH04(1)) CHD31340
 EQUIVALENCE (TEMPA1(1),TS(1)),(DELTAX(1),PARTIN(1)) CHD31350
 EQUIVALENCE (MNOD,NNP) CHD31360
 REAL MARY CHD31370
 NONF = INCOM CHD31380
 JHDN = NHDN(NZON) CHD31390
 GO TO (20,10),NLR CHD31400
 10 NSHR(NZON) = NONE CHD31410
 CHD31420
 CHD31430

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IU = IZGT(NZON) CHD31440
IG = IZG(NZON,IU) CHD31450
IGX = IG+1 CHD31460
GO TO 22 CHD31470
20 NSHL(NZON) = NONE CHD31480
IG = IZG(NZON,1) CHD31490
NONE = -NONE / CHD31500
IGX = IG-1 CHD31510
22 IF (NONE) 80,80,25 CHD31520
25 NZONX = IGTYP(IGX) CHD31530
30 KHDN = NHDN(NZONX) CHD31540
35 NTWO = VONE*JHDN CHD31550
GO TO (40,NLR) CHD31560
40 IX = IBF(IG)+NTWO CHD31570
IY = IBS(IGX)+NONE*KHDN CHD31580
IZ = IBSPN+NCSN(IGX)+NONE CHD31590
WFD(IX)=WFD(IY) CHD31600
WDFP(IX)=WDFP(IY) CHD31610
WSI(IX)=WSI(IY) CHD31620
WBRN(IX)=WBRN(IY) CHD31630
EMWT(IX)=EMWT(IY) CHD31640
WF(IX)=WF(IY) CHD31650
GRAF1(IX)=GRAF1(IY) CHD31660
TEMPA1(IX) = TEMPA1(IY) CHD31670
TEMPA2(IX) = TEMPA2(IY) CHD31680
TEMPA5(IX) = TEMPA5(IY) CHD31690
SILCA1(IX)=SILCA1(IY) CHD31700
CARBN1(IX)=CARBN1(IY) CHD31710
GO TO 60 CHD31720
50 IX = IRS(IG)
IY = IBF(IGX)
IZ = IBSPN+NCSN(IG)
60 IF (JHDN-KHDN) 65,65,70 CHD31730
65 NTHREE = KHDN/JHDN CHD31740
DO 67 J=1,NTWO CHD31750
IX = IX-1 CHD31760
CHD31770
IY = IY-NTHREE CHD31780
WFD(IX)=WFD(IY) CHD31790
WDFP(IX)=WDFP(IY) CHD31800
WSI(IX)=WSI(IY) CHD31810
WBRN(IX)=WBRN(IY) CHD31820
EMWT(IX)=EMWT(IY) CHD31830
WF(IX)=WF(IY) CHD31840
GRAF1(IX)=GRAF1(IY) CHD31850
RHO1(IX) = RHO1(IY) CHD31860
RHO2(IX) = RHO2(IY) CHD31870
SILCA1(IX)=SILCA1(IY) CHD31880
CARBN1(IX)=CARBN1(IY) CHD31890
TEMPA1(IX) = TEMPA1(IY) CHD31900
TEMPA2(IX) = TEMPA2(IY) CHD31910
TEMPA5(IX) = TEMPA5(IY) CHD31920
67 TEMPA5(IX) = TEMPA5(IY) CHD31930
GO TO 80 CHD31940
70 NTHREF = JHDN/KHDN CHD31950
FIVF = 1./FLOAT(NTHREF) CHD31960
KNT1 = 0 CHD31970
CHD31980

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71 KNT = 0 CHD31990
72 ONE = (TEMPA1(IY)-TEMPA2(IY-1))*FIVE CHD32000
    TWO = (TEMPA2(IY)-TEMPA2(IY-1))*FIVE CHD32010
    HOLD=(SILCA1(IY)-SILCA1(IY-1))*FIVE CHD32020
    SAVE=(CARBN1(IY)-CARBN1(IY-1))*FIVE CHD32030
    GARY=(WFD(IY)-WFD(IY-1))*FIVE CHD32040
    HECT=(WDFF(IY)-WDEP(IY-1))*FIVE CHD32050
    MARY=(WSI(IY)-WST(IY-1))*FIVE CHD32060
    CRUZ=(WARN(IY)-WPRN(IY-1))*FIVE CHD32070
    CAJA=(EMWT(IY)-FMWT(IY-1))*FIVE CHD32080
    TIENDA=(WF(IY)-WF(IY-1))*FIVE CHD32090
    CINE=(GRAF1(IY)-GRAF1(IY-1))*FIVE CHD32100
    IF (KNT) 73,73,74 CHD32110
73 JX = IZ CHD32120
GO TO 75 CHD32130
74 JX = IY CHD32140
75 JY = IY CHD32150
    THREE = (RHO1(JX)-RHO1(IY-1))*FIVE CHD32160
    FOUR = (RHO2(JX)-RHO2(IY-1))*FIVE CHD32170
    DO 76 J=1,NTHREF CHD32180
    IX = IX-1 CHD32190
    RHO1(IX) = RHO1(JX)-THRFF CHD32200
    RHO2(IX) = RHO2(JX)-FOUR CHD32210
    SILCA1(IX)=SILCA1(JY)-HOLD CHD32220
    CARBN1(IX)=CARBN1(JY)-SAVE CHD32230
    TEMPAA1(IX) = TEMPAA1(JY)-ONE CHD32240
    TEMPAA2(IX) = TEMPAA2(JY)-TWO CHD32250
    TEMPAA3(IX) = TEMPAA2(IX) CHD32260
    WFD(IX)=WFD(IY)-GABY CHD32270
    WDEP(IX)=WDEP(IY)-HECT CHD32280
    WSI(IX)=WSI(IY)-MARY CHD32290
    WPRN(IX)=WPRN(IY)-CRUZ CHD32300
    EMWT(IX)=EMWT(IY)-CAJA CHD32310
    WF(IX)=WF(IY)-TIENDA CHD32320
    GRAF1(IX)=GRAF1(IY)-CINE CHD32330
    JX = IX CHD32340
76 JY = JX CHD32350
    KNT = KNT+1 CHD32360
    IY = IY-1 CHD32370
    IF (KNT-KHDN1) 72,78,78 CHD32380
78 IZ = IZ-1 CHD32390
    KNT1 = KNT1+1 CHD32400
    IF (KNT1-NONE) 71,80,80 CHD32410
80 RETURN CHD32420
END CHD32430

```

- FOR SHIFT2,SHIFT3
 SUBROUTINE SHIFT2
 C**** THE SHIFT2 SUBROUTINE DOES SHIFT OF VALUES IN ZONES CHD32440
 DIMENSION NHDN(3), RH04(306) CHD32450
 DIMENSION DFLTAX(1), TEMPA1(1) CHD32460
 COMMON /BLOCKA/
 TABSORP(10), ABSC, ACTFNC, ACTENV, ACTENV(4,10), CHD32470
 PRESTAR, CCPCL(4), CCPG(4), CHAPPT(101), CKC(4), CHD32480
 BCOEFF(4,10), CONDC, CONDV(100), CONST(4,10), CRX(100), CHD32490
 ACPBAR, CPC, CPV(100), DIFREC, DMATER(10), FMISC, CHD32500
 SEFCOLC, EFCOLS, EFCOLV(4,10), EMIS(10), FMISC, CHD32510
 6HDFM(10), HCOM, HCOMG, HCP, MAT(100), CHD32520
 7MATMN, MATMN, MN, MN, MN, CHD32530
 BNNSAVE, NRDTIV, NPFND, NPFN, NST, CHD32540
 PARTIN(101), PH1, RBYRAD, RMR, NFT, CHD32550
 10GPCOM, QSUBL, RECPR0, RDRC, REORDS, CHD32560
 2REORDV(4,10), RH05Z, RH05(205), RCPX(101), RHOC, CHD32570
 3RH0V(101), SABL, SABL, DOT, SDOTC, CHD32580
 4SLOPE(101), TMELT(10), TSZ, S1205, RCHAR, CHD32590
 5WFZ, WF(205), XCHAR, XEFT, LFT(101), CHD32600
 6XMASS, XMDOTC, XMDOTD, XMDOTG, XMDOTL, CHD32610
 7XMDDTP, XMDDOTS, XTOTAL, YVIRG(101), ZONE, CHD32620
 COMMON /BLOCKC/
 1RLPRES(20,11), COMMAX, CUTOFF, F(20,11), CHD32630
 2FLOW(20,11), HCONV(20,11), IERROR, JUNCT, L, CHD32640
 3N, NOSECH, QBACK, QCONV(20,11), QGAS(20,11), CHD32650
 40MISC, TIME, TPRINT, TWALL(20,11), XIWALL(20,11), CHD32660
 5XIR(20,11)
 COMMON /HCOM/ DTAU, IBE(10), IRS(10), IRSPI, CHD32670
 1IGTYP(10), IHDN(4), IM, IZB(1), IZG(1,10), CHD32680
 2IZGT(3), JRSW, NCSN(10), NSHL(3), NSHR(3), CHD32690
 3NZEN(3), NZSN(3), RH01(205), RH02(205), RH03(410), CHD32700
 4I, TEMPA2(205), TEMPA3(42), TEMPA4(42), TEMPA5(205), CHD32710
 5, DELX(100), DISTL(100), DUM(10), ICOM, CHD32720
 6IYS, LFT, MG, MDUM, NCEN(10), NCUT, ND(3), NLZON, SN, SN1, CHD32730
 7SCHECK
 COMMON /NASCOM/ CHARRO, AIRM, CHD32740
 1CARBN1(205), CARBN5(205), SILCA1(205), SILCA5(205), PYFO(205), DEP(205), CHD32750
 2, HYD(205), AERO(205), AERN(205), BURN(205), WFD(205), WDFP(205), WSI(205), CHD32760
 3, WBRN(205), EMWT(205), PRG(205), CHD32770
 4, TIMFX(50), TFT(50), NPTS, CHD32780
 5, POR(205), PERM1(205), PERM2(205), VISC(205), GCON, RHOTS, CARTS, SILTS, CHD32790
 6, PORT, PERT1, PERT2, DCOH, DC00, DCOPY, DCODP, DCOST, DCOCM, DCON, CFXH, CFZO, CHD32800
 7, CFXPY, CFXDP, CFXSI, CFXCM, CFXN, DIFCO(205), S0X(205), CHD32810
 8, ALLGAS(205), GRAF1(205), CHD32820
 EQUIVALFNCE (IHDN(2), NHDN(1)) CHD32830
 EQUIVALFNCE (RH03(103), RH04(11)) CHD32840
 EQUIVALENCE (TEMPA1(1), TS(1)), (DFLTAX(1), PARTIN(1)) CHD32850
 EQUIVALENCE (MNOD, NNP) CHD32860
 DO 70 NZON=1,3
 IF (NSHL(NZON)) 10,60,10
 10 JHDN = NHDN(NZON)
 NONF = NSHL(NZON)*JHDN
 JRS = IZRINZON)+NONF
 IG = IZG(NZON,1) CHD32870

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IU = IZGT(NZON)          CHD32980
IGX = IZG(NZON,IU)        CHD32990
JBE = IBE(IGX)+NSHR(NZON)*JHON
IF (NSHL(NZON)) 20,20,30
20 JX = JBF
J = -1
GO TO 40
30 JX = JBS
J = 1
40 IY = JX-J
IX = IY-NCNF
DO 50 K=JBS,JBE
IX = IX+J
IY = IY+J
TEMPA1(IX) = TEMPAL(IY)
TEMPA2(IX) = TEMPAL(IY)
TFMPA5(IX) = TFMPA5(IY)
SILCA1(IX)=SILCA1(IY)
CARRN1(IX)=CARBN1(IY)
WFD (IX)=WFD (IY)
WDEP(IX)=WDEP(IY)
WSI (IX)=WSI (IY)
WBRN(IX)=WBRN(IY)
FMWT(IX)=FMWT(IY)
WF (IX)=WF(IY)
GRAF1(IX)=GRAF1(IY)
RHO1(IX) = RHO1(IY)
50 RHO2(IX) = RHO2(IY)
NZSN(NZON) = NZSN(NZON)+NSHL(NZON)
NSHL(NZON) =0
60 NZEN(NZON) = NZEN(NZON)+NSHR(NZON)
70 NSHR(NZON) = 0
RETURN
END

```

```

- FOR SIC,SIC
  SUBROUTINE SIC (K,KL,TEMPA,DELT)
C
C****  S102-CARBON REACTION
C
  COMMON /BLOCKKA/
    1ABSORP(10)  ,ABSC      ,ACTENC     ,ACTENS      ,ACTENV(4,10), CHD93320
    2BSTAR       ,CCPC(4)   ,CCPG(4)    ,CHARPT(10)  ,CKC(4)      , CHD93330
    3COEFT(4,10) ,CONDc    ,CONDV(100)  ,CONST(4,10) ,COVERX(100) , CHD93340
    4CPBAR       ,CPC       ,CPV(100)   ,DIFFFC     ,UMATER(10) , CHD93350
    5EFCOLC     ,EFCOLS    ,EFCOLV(4,10),EM15(10) ,EMISC      , CHD93360
    6HOFM(10)   ,HCOM      ,HOMG       ,HSUR        ,MAT(100)   , CHD93370
    7MATOMN     ,MATMNF    ,MN         ,NN          ,NMF        , CHD93380
    8NNSAVE      ,NRDIV     ,NREND      ,NRGO        ,NST        , CHD93390
    9PARTIN(10)  ,PHI       ,QYRAD      ,QCOMR      ,QFXTR      , CHD93400
   10GPCOM      ,QSUBL     ,RECPRO     ,REORDC    ,REORDS    , CHD93410
   2REORDV(4,10),RH05Z    ,RH05(305)  ,RHOCPX(101),RHOC      , CHD93420
   3PHOV(10)   ,SABL      ,SABLc      ,SDOT        ,SDOTC     , CHD93430
   4SLOPE(10)  ,SMELT(10) ,TSZ        ,TS(205)    ,TRCHAR    , CHD93440
   5WFZ         ,WF(205)   ,XCHAP     ,XINIT      ,XLFFT(101) , CHD93450
   6XMASS       ,XMDOTC   ,XMDOTD   ,XMDOTG   ,XMDCTL   , CHD93460
   7XMDOTR     ,XMDOTS   ,XTOTAL    ,XVIRG(101) ,XZONE     , CHD93470
  COMMON/BLOCKC/
   1BLPRES(20,11) ,COMMEX   ,CUTOFF     ,F(20,11)  , CHD93480
   2FLOW(20,11)  ,HCONV(20,11),ERROR     ,JUNCT     ,L          , CHD93490
   3N          ,NOSECH   ,QBACK      ,QCONV(20,11),QGAS(20,11), CHD93500
   4QMISC      ,TIME      ,TPRINT    ,TWALL(20,11),XTWALL(20,11), CHD93510
   5XIP(20,11)  ,           ,           ,           ,           , CHD93520
  COMMON /BLOCKJ/
   1FLUXI(200),TEDEP(200),XEDEP(101),EDEP(101),NTEDEP, CHD93530
   2NXFDEP,ITEPEP,EDFLUX(100) ,           ,           , CHD93540
  COMMON /BLOCKK/NN1,QCOND(205) ,           ,           , CHD93550
  COMMON/BLOCKN/COORD
  COMMON/BLOCKR/DIFC(4),FROC(4),FRODF
  COMMON /CHCOM/ DTAU,    IBE(10),   IB5(10),   IBSPN, CHD93560
   1IGTYP(10),  IDHN(4),   IM,        IZB(3),    IZG(3,10), CHD93570
   2IZGT(3),    JRSW,     NCSN(10),  NSHL(3),  NSHR(3),  CHD93580
   3NZEN(3),    NZSN(3),  RH01(205), RH02(205), RH03(410), CHD93590
   4I          ,TEMPA2(205),TEMPA3(42),TEMPA4(42),TEMPS(205), CHD93600
   5          ,DELX(100),  DISTL(100),DUN(10),  ICOM,  CHD93610
   6IYS,LFT,MG,MDUM,NCEN(10),NCUT,ND(3),NLZON,SN,SN1, CHD93620
   7SCHECK
C****  DIMENSION STATEMENTS
C
  DIMENSION DELTAX(1),TEMPA1(1) ,           ,           , CHD93630
  EQUIVALENCE (TEMPA1(1),TS(1)),(DELTAX(1),PARTIN(1)) ,           , CHD93640
  COMMON /NASCOM/ CHARRO,ATRM,               ,           , CHD93650
   1CARBN1(205),CARBN5(205),SILCA1(205),PYRO(205),DEP(205) , CHD93660
   2HYD(205),AERO(205),AERN(205),BURN(205),WFD(205), WDEP(205),WSI(20) , CHD93670
   35),WBRN(205),EMWT(205),PRG(205) ,           ,           , CHD93680
   4,TIMFX(50),TFT(50),NPTS ,           ,           , CHD93690
   5,POR(205),PERM1(205),PERM2(205),VIS(205),GCON,RHOTS,CARTS,SILTS, CHD93700
   6PORT,PERT1,PERT2,DCOH,DCOO,DCOPY,DCODP,DCOSI,DCOCM,DCON,CFX4,CFXO,CHD93710
   7CFXPY,CFXDP,CFXS1,CFXCM,CFXN,DIFCO(205),SOX(205) ,           , CHD93720
   8,ALLGAS(205),GRAF1(205),GRAF5(205),SPEED(205),DIFCH(205),DIFR(205) , CHD93730

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9,VISCO,VISCON,AF,BF,SILICA,RFO,PMW,DMW,HMW,AOMW,ANMW,SMW,BMW,CX(6)CHD33860
C CHD33870
WSI02=AF*EXP(-BF/TFMPA)*(SILCA1(KL)/SILICA)**RFO CHD33880
SILCA1(KL)=SILCA1(KL)-WSI02*DTAU CHD33890
IF (SILCA5(KL)) .5,.6,.6 CHD33900
5 SILCA5(KL)=0. CHD33910
WSI02=(SILCA1(KL)-SILCA5(KL))/DTAU CHD33920
6 CONTINUF CHD33930
CARBNS(KL)=CARBN1(KL)-WSI02*DTAU*.2 CHD33940
WSI(KL)=WSI02*(DELTAX(K)+DEL)*.05 CHD33950
RETURN CHD33960
END CHD33970

- AGM STUFF2, STUFF3
REGNAME

| | | |
|-------------|------------|----------|
| STUFF2* NOP | | |
| S | A0, STUFF3 | CHD33980 |
| L | A0, C127 | CHD33990 |
| AN, 14 | A0, 2 | CHD34000 |
| S | A0, C127 | CHD34010 |
| L | A0, STUFF3 | CHD34020 |
| J | DIAG6 | CHD34030 |
| STUFF3 +0 | | CHD34040 |
| FND | . | CHD34050 |
| | | CHD34060 |
| | | CHD34070 |

```
- FOR SURZ,SURZ
  SUBROUTINE SURZ(Z,T,P)
    XLN=ALOG(P/2116.21/2.3026
    THETA=T*(.555556-.069444*XLN)
    IF (THETA>2000.) 1• 1• 2
1 Z = 1.
  GO TO 3
2 Z = 2.5+.1*TANH(THETA/500.-7.)+.4*TANH(THETA/1000.-7.)+TANH(THETA)CHD34140
  1/2500.-5.8)
3 RETURN
  END
```

- FOR WRITE,WRITE

SUBROUTINE WRITE

COMMON /PLOCKA/

| | | | | | |
|---------------|------------|---------------|--------------|---------------|-----------|
| 1ABSORP(10) | ,ABSC | ,ACTENC | ,ACTENS | ,ACTENV(4,10) | ,CHD34220 |
| 2B5T4R | ,CCPC(4) | ,UCPG(4) | ,CHARPT(10) | ,CKC(4) | ,CHD34230 |
| 3C0EFT(4,10) | ,COND | ,CONDV(100) | ,CONST(4,10) | ,COVFRX(100) | ,CHD34250 |
| 4CPBAR | ,CPC | ,CPVI(100) | ,DIFRFC | ,UMATFR(10) | ,CHD34270 |
| 5EFCOLC | ,EFCOLS | ,EFCOLV(4,10) | ,EMIS(10) | ,EMISC | ,CHD34280 |
| 6HOFM(10) | ,HCOM | ,HCOMG | ,HSUR | ,UMAT(100) | ,CHD34290 |
| 7MATMN | ,MATMNF | ,MN | ,NN | ,NNP | ,CHD34300 |
| 9NNSAVE | ,NRDIV | ,NRFIND | ,NRGO | ,NST | ,CHD34310 |
| 9PARTIN(10) | ,PHI | ,OBYPAD | ,QCOMB | ,QEXTR | ,CHD34320 |
| 10GPCom | ,OSUBL | ,RECPRO | ,REFRDC | ,REFORDS | ,CHD34330 |
| 2REORDV(4,10) | ,RH05Z | ,PH05(10) | ,RH0CPX(10) | ,RHCC | ,CHD34340 |
| 3PHOV(10) | ,SABL | ,SABL | ,SDOT | ,SDOTC | ,CHD34350 |
| 4SLOPE(10) | ,TMELT(10) | ,TS(205) | ,TS(205) | ,TRCHAR | ,CHD34360 |
| 5WFZ | ,WF(205) | ,XCHAR | ,XINIT | ,XLEFT(10) | ,CHD34370 |
| 6XMASS | ,XMDO TC | ,XMDO TD | ,XMDO TG | ,XMDO TL | ,CHD34380 |
| 7XMODTR | ,XMDO TS | ,XTOTAL | ,XVIRG(10) | ,XZONE | ,CHD34390 |

COMMON/BLOCKB/

| | | | | | |
|----------------|----------------|---------------|----------------|---------------|-----------|
| 1ALT | ,UFA | ,AOFACH | ,BETA(20) | ,BLCOM(20,11) | ,CHD34400 |
| 2BLDEN(20,11) | ,ENT(0,11) | ,BLTEM(20,11) | ,BLVEL(20,11) | ,BLRN(20,11) | ,CHD34410 |
| 3BMULT | ,DIST(20,11) | ,FSOM | ,FSGAM | ,LFNGTH(21) | ,CHD34420 |
| 4NCIM | ,NTEMP | ,NTHETA | ,NTIMF | ,PAMB | ,CHD34430 |
| 5P-2 | ,PTOTAL | ,QAMB | ,QSHOUL | , | ,CHD34440 |
| 6P(20,11) | ,REFCOM(20,11) | | ,REFDEN(20,11) | | ,CHD34450 |
| 7REFENT(20,11) | | ,REFRN(20,11) | ,REFTEM(20,11) | | ,CHD34460 |
| 8REFVIS(20,11) | | ,RH0A | ,RH0VIS | ,RNPERF | ,CHD34470 |
| 9PTRAN | ,SOFS | ,SWEEP | ,THETA(11) | ,THETSH | ,CHD34480 |
| 1TTOTAL | ,UAMB | ,VISCOS | ,X(20,11) | ,XE0(20,11) | ,CHD34490 |
| 2XIAMB | ,XISP | ,XLTRAN | ,XMACH | ,XY | ,CHD34500 |
| 3ATEMP | ,BLVIS(20,11) | ,ZWALL | ,REFPR(20,11) | ,HMAX | ,CHD34510 |

COMMON /PLOCKC/

| | | | | | |
|--------------|---------------|---------|---------------|----------------|-----------|
| 1BI | ,ES(20,11) | ,COMMAY | ,CUTOFF | ,F(20,11) | ,CHD34520 |
| 2FL_w(20,11) | ,HCCNV(20,11) | ,IER OR | ,JUNCT | ,L | ,CHD34530 |
| 3N | ,NOSECH | ,QBACK | ,QCONV(20,11) | ,QGAS(20,11) | ,CHD34540 |
| 4QMISC | ,TIME | ,TPRINT | ,TWALL(20,11) | ,XIWALL(20,11) | ,CHD34550 |
| 5XIR(20,11) | | | | | ,CHD34560 |

COMMON /RLOCKD/

| | | | | | |
|-------------|------------|------------|----------------|--------------|-----------|
| 1ALPHA(200) | ,AMB(200) | ,AMRT(200) | ,AMULT(200) | ,AXLD(200) | ,CHD34570 |
| 2BWTEST | ,IATMOS | ,IPR | ,IPRINT(20,10) | | ,CHD34580 |
| 3IG | ,IX | ,KK | ,MELTN | ,MELTL | ,CHD34590 |
| 4 | MVTEST | ,NKK | ,NCHARM | ,NMATLU | ,CHD34600 |
| 5NMATL | ,NMATLD | ,NSTRES | ,NTBW | ,NTIME1 | ,CHD34610 |
| 6NTIME2 | ,PRINT | ,PUT(20) | ,QBAC(200) | ,QINC(20) | ,CHD34620 |
| 7QINCR | ,QM(200) | ,QTIME(20) | ,QTABL(6,200) | | ,CHD34630 |
| 8RPRINC | ,RQINC | ,PXINC | ,T(200) | ,TRW(200) | ,CHD34640 |
| 9TEMP(7) | | | ,TNT(20) | ,TORIBW(200) | ,CHD34650 |
| 1TSIN(10) | ,TT(200) | ,VI(200) | ,XINC(20) | | ,CHD34660 |
| 2XINCP | ,XTIME(20) | ,Z(200) | ,ZZ(200) | | ,CHD34670 |

COMMON /FLOCKF/

| | | | | | |
|---------------|---------------|--------------|---------------|-------------|-----------|
| 1ASTR(205) | ,AXLDEQ | ,CCOMSC(4) | ,CCUMSV(4,10) | ,CEMODC(4) | ,CHD34720 |
| 2CEMODV(4,10) | ,CEXP(4) | ,CEXPV(4,10) | ,CLCOEF | ,CMWGAS(4) | ,CHD34730 |
| 3CNUC(4) | ,CNLV(4,10) | ,CSHRSC(4) | ,CSHRSV(4,10) | ,CSTRO(205) | ,CHD34740 |
| 4CTENSC(4) | ,CTENSV(4,10) | ,GP(205) | ,PERMC | ,PIN | ,CHD34750 |

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      P0R0SC      ,P0R0SV(101) ,P1TR1(205) ,PSTR2(205) ,PSTR3(205) , CHD34760
      ERIN      ,RSTRO(205) ,SHRSTR(205) ,SSMAX(205) ,RAD(205)   CHD34770
      7,NGLART
      COMMON/BLOCKG/
      1CBOLD      ,QBWTOT      ,QCLD(20,10) ,QCOLD      ,QCONVT(20,10),CHD34800
      2QGAST(20,10),QGLD(20,10) ,QGOLD      ,QMTSCT      ,QMOLD      CHD34810
      COMMON /BLOCKR/NCND(205)
      COMMON/BLOCKR/DIFC(4),PROC(4),FRDF
      COMMON /PACOM/ UPFED(897),ITERT,MAS(74),NASW,UPSIT(84),TAU1
      COMMON /NASCOM/ CHARRO,AIRM,
      1CARBN1(205),CARBN(205),SILCA1(205),SILCA5(205),PYRO(205),DEP(205)CHD34860
      2,HYD(205),AERO(205),AERN(205),BURN(205),WFD(205),WDFP(205),WSI(20CHD34870
      35),WBRN(205),EMWT(205),PRG(205)
      4,TIMEX(50),ZFT(50),NPTS
      5,POR(205),PERM1(205),PERM2(205),VISC(205),GCON,RHOTS,CARTS,SILTS, CHD34900
      6PORT,PERT1,PERT2,DCOH,DC00,DCOPY,DCODP,DCOS1,DCOCM,DCON,CFXH,CFXO,CHD34910
      7CFXPY,CFXDP,CFXS1,CFXCM,CFXN,DIFC0(205),SOX(205)           CHD34920
      8,ALLGAS(205),GRAF1(205),GRAF5(205),SPEED(205)
      DIMENSION RHOR(1),XR(1),PRHOA(1),RHOU(1)
      EQUIVALENCE (RH05(119),RHOR(1)),(CHARPT(2),XR(1))
      1      ,(RHOU(1),RH05(205)),(PRHOA(1),XVIRG(1))           CHD34950
      DATA HLAM1/6H LAMIN/,HLAM2/2HAR/,HTURB1/6HTURBUL/,HTURB2/3HENT/ CHD34960
      C
      C          PRINT TEMPERATURE, DENSITY, AND GAS PRESSURE DISTRIBUTIONCHD35000
      C          FOR DETAILED DESIGN
      WRITE (6,1000) TAU1,ITERT
      390 WRITE (6,1015)
      ISPY=1
      392 CONTINUE
      DO 470 I=NNP,1,-1
      IPLUS=I+203
      IF (I-NRFND) 403,403,400
      400 IF (I-NNP) 460,401,401
      401 JSUB=192
      GO TO 410
      403 IF (I-NRG0) 460,460,404
      404 JSUB=NRD1V*(I-NRG0)+120
      410 FNRDIV=NRDIV
      DX=(XLFFT(I)-XLFFT(I-1))/FNRDIV
      XDUM=XLFFT(I)-XLFFT(1)+DX
      DO 450 J=1,NRDIV
      XDUM=XDUM-DX
      LT=JSUB-J
      TDUM=TS(LT)-459.69
      IF (J-1)420,420,430
      420 RHO=RHO5(IPLUS)
      M=I
      GO TO 444
      430 RHO=RHO5(LT)
      M=I-1
      444 GO TO (445,446),ISPY
      445 CONTINUE
      RHODE=RHO-CARBN1(LT)-SILCA1(LT)-GRAF1(LT)
      WRITE (6,1016, M,XDUM,TDUM,QCOND(LT),RHO,RHODE,CARBN1(LT),GRAF1(LT)CHD35300

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1)•SILCA1(LT),PRG(I),FMWT(LT),SPEED(LT) CHD35210
GO TO 450 CHD35320
446 CONTINUE CHD35330
    WRITE (6,1022) M,WF(LT),WFD(LT),WDFP(LT),WSI(LT),WBRN(LT),AERO(LT) CHD35340
    I+AERN(LT),HYD(LT),PYRO(LT),DEP(LT),SOX(LT),BURN(LT),ALLGAS(LT) CHD35350
450 CONTINUE CHD35360
    GO TO 470 CHD35370
460 TDUM=TS(I)-4E9.60 CHD35380
    XDUM=XLEFT(I)-XLEFT(1) CHD35390
    GO TO (461,462),ISPY CHD35400
461 CONTINUE CHD35410
    RHO=RHO5(IPLUS) CHD35420
    RHODE=RHO5(IPLUS)-CARBN1(I)-SILCA1(I)-GRAF1(I) CHD35430
    WRITE (6,1016) I,XDUM,TDUM,QCOND(I),RHO,RHODE,CARBN1(I),GRAF1(I), CHD35440
    1)SILCA1(I),PRG(I),FMWT(I),SPEED(I) CHD35450
    GO TO 463 CHD35460
462 CONTINUE CHD35470
    WRITE (6,1022) I,WF(I),WFD(I),WDFP(I),WSI(I),WBRN(I),AERO(I), CHD35480
    1)AERN(I),HYD(I),PYRO(I),DEP(I),SOX(I),BURN(I),ALLGAS(I) CHD35490
463 CONTINUE CHD35500
470 CONTINUE CHD35510
    GO TO (471,472),ISPY CHD35520
471 ISPY=2 CHD35530
    WRITE (6,1021) CHD35540
    GO TO 392 CHD35550
472 CONTINUE CHD35560
1000 FORMAT (1H1,6H TIME=F8.2,5X17HTOTAL ITERATIONS=16//) CHD35570
1015 FORMAT(1H0,7X8HDISTANCE14X9HCONDUCTED7X18H----- CHD35580
    1)5H-DFNSITIFS (LBM/FT3)-----2X BHINTERNAL/PH NODE FR CHD35590
    230HOM BACK TEMP HEAT FLUX7X28HTOTAL DECOMP CARBONCHD35600
    34X 17HGRAPHITE SILICA 6X20HPRESSURE MOL WT VFLOCITY/9X CHD35610
    4 6H(IN16X22H(DEG F) (BTU/FT2-SEC)159X 9H(LBF/FT2)14XAH(FT/SEC)/) CHD35620
1016 FORMAT (1H ,13,F10.4,F12.2,F15.4,2X,5F11.4,F12.5,F9.3,E13.5) CHD35630
1021 FORMAT(1H0,6X=3HGAS FLOW,3X,32H-----SOURCES AND SINKS----- 5XCHD35640
    174H-----CONCENTRATIONS-----CHD35650
    2----- /15H NODE RATE(LBM/,12X14H(LBM/NODE-SEC),49X14H(LBM/FT3)CHD35660
    3 VOID)/7X53HFT2-SEC) PYRO DEPO ST-C INT COMB OXYGEN CHD35670
    43X27H NITROGEN HYDROGEN PYRO,6X,4HDFP0,6X3HS107X4HBURN6X5HTOTACHD35680
    5L/1 CHD35690
1022 FORMAT(I4,E11.4,1X,4E9.2,RE10.3) CHD35700
    END CHD35710

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```
- FOR TBSTEP,TBSTEP
  FUNCTION TBSTEP (TAU1,TIMF1,DSTEP,NPTS)
  DIMENSION TIMF1(1),DSTEP(1)
  I=2
  3 IF (I-NPTS) 5,5,4
  4 TBSTEP=DSTEP(I-1)
  RETURN
  5 IF (TAU1-TIMF1(I)) 7,6,6
  6 I=I+1
  GO TO 3
  7 CONTINUE
  TBSTEP=TIME1(1)-TAU1
  TBSTEP=GAMIN1(TBSTEP,DSTEP(I-1))
  RETURN
  END
```

CHD35720
CHD35730
CHD35740
CHD35750
CHD35760
CHD35770
CHD35780
CHD35790
CHD35800
CHD35810
CHD35820
CHD35830
CHD35840
CHD35850
CHD35860

```

- FOR OUTPUT,OUTPUT
  SUBROUTINE OUTPUT (MTO)                                CHD35870
  COMMON /BLOCKA/
  1ABSORP(10)  ABSC      ACTENC   ACTENS   ACTENV(4+10), CHD35880
  2BSTAR       CCPC(4)   CCPG(4)  CHARPT(10) CKC(4)   CHD35890
  3COEFT(4+10) CONDC    CONDV(100) CONST(4+10) COVERX(100) CHD35910
  4CPBAR       CPC       CPV(100)  DIFREC   SUMATER(10)  CHD35920
  5EFCOLC     EFCOLS    EFCOLV(4+10) EMIS(10)  EMISC    CHD35930
  6HOFM(10)   HCOM      HCOMG    HSUB     MAT(100)  CHD35940
  7MATMNE     MATMNE    MN        NN       NNP      CHD35950
  8NNSAVE     NRDIV    NREND    NRGO    NST      CHD35960
  9PARTIN(10) PHI       QBYRAD   QCOMB   QEXTRA  CHD35970
  10GPCOM    QSUBL     RECPRO   REORDC  REORDS  CHD35980
  2REORDV(4+10) RHO5Z   RH05(305) RHOCPX(101) RHOC    CHD35990
  3RH0V(10)   SABL     SABLc    SDOT    SDOTC   CHD36000
  4SLOPE(10) TMELT(10) TSZ      TS(205)  TCHAR   CHD36010
  5WFZ        WF(205)  XCHAR    XINIT   XLEFT(101) CHD36020
  6XMASS     XMDOTC   XMDOTD  XMDOTG  XMDOTL  CHD36030
  7XMDOTR   XMDOTS   XTOTAL   XVIRG(101) XZONE   CHD36040
  COMMON/BLOCKC/
  1BLPRES(20+11) COMMAX   CUTOFF   F(20+11)  CHD36060
  2FLOW(20+11) HCUNV(20+11),IERROR JUNCT    L       CHD36070
  3N        NOSECH   QBACK    QCONV(20+11),QGAS(20+11) CHD36080
  4QMISC    TIME      IPRINT   TWALL(20+11),XIWALL(20+11) CHD36090
  5XIR(20+11)
  COMMON/BLOCKR/DIFC(4),EROC(4),ERODE
  COMMON /NASCOM/ CHACRO,AIRM,                                     CHD36110
  1CARBN1(205),CARBN5(205),SILCA1(205),SILCA5(205),PYRO(205),DEP(205) CHD36130
  2HYD(205),AERO(205),AERN(205),BURN(205),WFD(205),WDEP(205),WSI(20) CHD36140
  35,WBRN(204),EMWT(205),PRG(205)                                     CHD36150
  4,TIMEX(50),TFT(50),NPTS                                         CHD36160
  5,POR(205),PERM1(205),PERM2(205),VIS(205),GCON,RHOTS,CARTS,SILTS, CHD36170
  6PORT,PERT1,PERT2,DCOH,DCOO,DCOPY,DCODP,DCOSI,DCOCM,DCON,CFXH,CFXO,CHD36180
  7CFXPY,CFXDP,CFXS1,CFXCM,CFXN,DIFC(205),SOX(205)                   CHD36190
  8,ALLGAS(205),GRAF1(205),GRAF5(205),SPEED(205),DIFCH(205),DIFR(205) CHD36200
  9,VISCO,VISCON,AF,BF,SILICA,REO,PMW,DMW,HMW,AOMW,ANMW,SMW,BMW,CX(6) CHD36210
  1,QSI,QBRN,QDEP                                         CHD36220
  WRITE (6,1049)                                         CHD36230
  DO 10 I = 1,MTO                                         CHD36240
  WRITE (6,1050) I                                         CHD36250
  WRITE (6,1051)                                         CHD36260
  WRITE (6,1052) ACTENV(1,1),ACTENV(1,2),EFCOLV(1,1),EFCOLV(1,2), CHD36270
  1RECRDV(1,1),REORDV(1,2)                                         CHD36280
  WRITE (6,1053) HOFM(1)                                         CHD36290
  WRITE(6,1054) (COEFT(I,J),J=1,4),(CONST(I,J),J=1,4) CHD36300
  WRITE(6,1055) EMIS(1),ABSORP(1),RH0V(1),SLOPE(1) CHD36310
  10 CONTINUE
  WRITE (6,1056)                                         CHD36320
  WRITE (6,1057)                                         CNP36330
  WRITE (6,1052) ACTENC,ACTENS,EFCOLC,EFCOLS,REORDC,REORDS CHD36350
  WRITE (6,1058) HCOM                                         CHD36360
  WRITE (6,1060) HSUB                                         CHD36370
  WRITE (6,1061) EMISC,ABSC,RHOC,TCHAR CHD36380
  WRITE (6,1062) CHARRC                                         CHD36390
  WRITE (6,1063)                                         CHD36400

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      WRITE (6,1064) (CCPG(J),J=1,4)                                CHD36410
      WRITE(6,1065) H*OMG                                         CHD36420
      WRITE (6,1066)                                         CHD36430
      WRITE(6,1067) CARTS,RHOTS,S*LTS                           CHD36440
      WRITE (6,1068) PORT,PERT1,PERT2                         CHD36450
      WRITE (6,1069) VISCO,VISCON                            CHD36460
      WRITE (6,1070) DCOCH,DCODP,DCON,DCOO,DCOPY,DCOSI    CHD36470
      WRITE (6,1071) BSTAR,(DIFC(J),J=1,4)                   CHD36480
      WRITF (6,1072) QSI,QDFF                               CHD36490
      WRITE (6,1073) BF,AF,REO                             CHD36500
      WRITE (6,1074) SILICA                                CHD36510
      WRITE (6,1075) (X(1),CX(4),CX(2),CX(5),CX(3),CX(6))   CHD36520
1049 FORMAT (1H0,10X,39HMATERIAL PROPERTIES OF VIRGIN MATERIALS) CHD36530
1050 FORMAT (1H0,14X,1)HMATERIAL (,I2,1H1)                  CHD36540
1051 FORMAT (1H0,59X10HFIRST REAC,6X11HSECOND REAC)        CHD36550
1052 FORMAT (1H ,24X,28HACTIVATION TEMPERATURE,DEG R ,6X,F10.1,6X,F10.1) CHD36560
      1          /25X,25HCOLLISION FREQUENCY,1/SEC      ,9X,E14.6,E16.6  CHD36570
      2/25X,14HREACTION ORDER,20X,F10.4,6X,F10.1)           CHD36580
1053 FORMAT (1H0,24X,29HHEAT OF DECOMPOSITION,BTU/LBM,5X,F10.2) CHD36590
1054 FORMAT (1H0,24X,27HSPECIFIC HEAT,BTU/LBM-DEG R ,7X,1H(E10.4,3H)+CHD36600
      1,(E10.4,4H)T+(,E10.4,7H)T**2+1,E10.4,5H)T**3/25X,34HCONDUCTIVITY,BCHD36610
      2TU-IN/FT2-SEC-DEG R ,1H(E10.4,3H)+1,E10.4,4H)T+(,E10.4,7H)T**2+(, CHD36620
      3E10.4,5H)T**3)                                     CHD36630
1055 FORMAT (1H0,24X,10HEMISSIVITY,26X,F10.4/25X12HABSORPTIVITY,22X, CHD36640
      1F10.4/25X15HDENSITY,LBM/FT3,19X,F10.2/25X34HTRANSPIRATION FACTOR (CHD36650
      2ABL GASES),,F10.4)                                 CHD36660
1056 FORMAT (1H0/10X31HMATERIAL PROPERTIES OF THE CHAR)     CHD36690
1057 FORMAT (1H0,53X,19HCOMBUSTION REACTION,3X,16HCHAR SUBLIMATION) CHD36700
1058 FORMAT (1H0,24X,26HHEAT OF COMBUSTION,BTU/LBM,8X,F10.2) CHD36710
1060 FORMAT (1H ,24X,27HHEAT OF SUBLIMATION,BTU/LBM,7X,F10.2) CHD36720
1061 FORMAT (1H0,24X,10HEMISSIVITY,24X,F10.4/25X12HABSORPTIVITY,22X, CHD36730
      1F10.4/25X15HDENSITY,LBM/FT3,19X,F10.2/25X34HTRANSPIRATION FACTOR (CHD36740
      2CHAR GASES),,F10.4)                                CHD36750
1062 FORMAT (1H0,24X,38HDENSITY OF THE CARBON IN CHAR,LBM/FT3 ,F7.2) CHD36760
1063 FORMAT (1H0/10X23HABLATION GAS PROPERTIES)             CHD36770
1064 FORMAT (1HC,24X,27HSPECIFIC HEAT,BTU/LBM-DEG R ,7X,1H(E10.4,3H)+CHD36780
      1,(E10.4,4H)T+(,E10.4,7H)T**2+1,E10.4,5H)T**3) CHD36790
1065 FORMAT (1H ,24X,30HHEAT O" GAS COMBUSTION,BTU/LBM,4X,F10.2) CHD36800
1065 FORMAT (1H0/10X15HOTHER CONSTANTS)                      CHD36810
1067 FORMAT (1H0,24X34HTHEORETICAL CARBON DENSITY,LBM/FT3,F10.2/
      125X,34HTHEORETICAL VIRGIN DENSITY,LBM/FT3,F10.2/ CHD36830
      225X,34HTHEORETICAL SILICA DENSITY,LBM/FT3,F10.2) CHD36840
1068 FORMAT (1H0,24X,18HREFERENCE POROSITY,16X,F10.4/ CHD36850
      125X,34HREFERENCE VISCOS PERMEABILITY,FT2,E14.6/ CHD36860
      225X,35HREFERENCE INERTIAL PERMEABILITY,FT ,E13.6) CHD36870
1069 FORMAT (1H0,24X,30HREFERENCE VISCOSITY,LBM/FT-SEC,E14.6/ CHD36880
      125X,34HREFERENCE TEMPERATURE FOR VISC.,R ,F10.2) CHD36890
1070 FORMAT (1H0,14X,34HSURFACE DIFFUSION CONSTANT,FT2/SEC/
      125X,15HCARBON MONOXIDE,19X,E14.6/ CHD36900
      225X,32HDEPOSITION GAS (EXCEPT HYDROGEN),2X,E14.6/ CHD36910
      325X,8HNITROGEN,26X,E14.6/ CHD36920
      425X,8HOXYGEN ,26X,E14.6/ CHD36930
      525X,7HMETHANE,27X,E14.6/ CHD36940
      625X,16HSILICON MONOXIDE,18X,E14.6) CHD36950
1071 FORMAT (1H0/25X, 17HBLLOWING PARAMETER,17XF10.4/25X, CHD36960
                                         CHD36970

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129HDIFFUSION REDUCTION PARAMETER,5X1H(E10.4,3H)+1,E10.4,6H)ETA+1, CHD36980
2F10.4,9H)ETA##2+(,F10.4,7H)FTA##3)
1072 FORMAT (25X,32HHEAT OF REACTION, S1O2-C,BTU/LBM,2XF10.2/
125X,39HHEAT OF REACTION, C DEPOSITION, BTU/LBM,F8.2)
1073 FORMAT (1H0,14X,32HSILICA-CARBON REACTION CONSTANTS/
1 25X,28HACTIVATION TEMPERATURE,DEG R ,6X,F10.1/
2 25X,25HCOLLISION FREQUENCY,1/SEC ,9X,E14.6
3/25X,14HREACTION ORDER,20X,F10.4)
1074 FORMAT (1H0,24X,38HSILICA DENSIT: IN INITIAL CHAR,LBM/FT3, F8.2)
1075 FORMAT (1H0,14X,36HCARBON DEPOSITION REACTION CONSTANTS/
11H0,58X, 12HLOW HYDROGEN,6X,13HHIGH HYDROGFN/
225X,1HX,33X, E14.6,E16.6/25X,1HY,33X,E14.5,E16.6/25X,1HZ,33X,E14.6CHD37090
3,E16.6)
RETURN
END

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REFERENCES

1. Caudette, R.S.; del Casal, E.P.; and Crowder, P.A.: Charring Ablation Performance in Turbulent Flow. Volume I, "Analytical and Experimental Data". Prepared under NASA Contract No. NAS 9-6288, Boeing Document D2-114031-1, September 1966.
2. Hillberg, L.H.: The Convective Heating and Ablation Program (CHAP). Boeing Document D2-36402-1, May 1966.
3. Wells, P.B.: A Method for Predicting the Thermal Response of Charring Ablation Materials. Boeing Document D2-23256-1, June 1964.
4. Scala, S.M.: The Ablation of Graphite in Dissociated Air, Part I, "Theory". Institute of the Aeronautical Sciences Paper 62-154, June 1962.
5. Bartlett, E.P.: Analytical and Graphical Prediction of Graphite Ablation Rates and Surface Temperatures During Re-Entry at 25,000 to 45,000 Feet per Second. Air Force Flight Test Center Report, TDR-63-40, March 1964.
6. Nelson, B.F.: A Model for Phenolic Nylon Diffusion Controlled Char Combustion Rates. Boeing Coordination Sheet 2-5521-2-15CS, July 1965.
7. Scala, S.M.; and Gilbert, L.M.: Aerothermochemical Behavior of Graphite at Elevated Temperatures. General Electric Report R63SD89, November 1963.
8. Crank, J.; and Nicolson, P.: "A Practical Method for Numerical Evaluations of Solutions of Partial Differential Equations of the Heat-Conduction Type". Proceedings of the Cambridge Philosophical Society, Vol. 43, 1967, pp. 50-67.